

AFWL-TR-79-193

AD-E200607

① LEVEL III

AFWL-TR-  
79-193

AD A092379



DDC FILE COPY

## QUANTA - USERS MANUAL

1st Lt M. E. Badessa

July 1980

Final Report

Approved for public release; distribution unlimited.

DTIC  
ELECTE  
DEC 3 1980  
S B D

THIS DOCUMENT IS UNCLASSIFIED.  
THE COPY IS NOT TO BE REPRODUCED OR  
SIGNIFICANTLY MODIFIED OR USED FOR  
REPRODUCTION PURPOSES.

AIR FORCE WEAPONS LABORATORY  
Air Force Systems Command  
Kirtland Air Force Base, NM 87117

80 12 02 007

This final report was prepared by the Air Force Weapons Laboratory, Kirtland Air Force Base, New Mexico, under Job Order 88092220. First Lieutenant Maria Badessa (NTYV) was the Laboratory Project Officer-in-Charge.

When US Government drawings, specifications, or other data are used for any purpose other than a definitely related Government procurement operation, the Government thereby incurs no responsibility nor any obligation whatsoever, and the fact that the Government may have formulated, furnished, or in any way supplied the said drawings, specifications, or other data, is not to be regarded by implication or otherwise, as in any manner licensing the holder or any other person or corporation, or conveying any rights or permission to manufacture, use, or sell any patented invention that may in any way be related thereto.

This report has been authored by an employee of the United States Government. Accordingly, the United States Government retains a nonexclusive, royalty-free license to publish or reproduce the material contained herein, or allow others to do so, for the United States Government purposes.

This report has been reviewed by the Public Affairs Office and is releasable to the National Technical Information Service (NTIS). At NTIS, it will be available to the general public, including foreign nations.

This technical report has been reviewed and is approved for publication.



MARIA E. BADESSA  
1st Lt, USAF  
Project Officer

FOR THE DIRECTOR



TERRY A. SCHMIDT  
Major, USAF  
Chief, Environment & Effects Branch



THOMAS W. CIAMBRONE  
Colonel, USAF  
Chief, Applied Physics Division

DO NOT RETURN THIS COPY. RETAIN OR DESTROY.

## **DISCLAIMER NOTICE**

**THIS DOCUMENT IS BEST QUALITY  
PRACTICABLE. THE COPY FURNISHED  
TO DTIC CONTAINED A SIGNIFICANT  
NUMBER OF PAGES WHICH DO NOT  
REPRODUCE LEGIBLY.**

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER AFWL-TR-79-193	2. GOVT ACCESSION NO. AD-A092 379	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) QUANTA - USERS MANUAL		5. TYPE OF REPORT & PERIOD COVERED Final Report
		6. PERFORMING ORG. REPORT NUMBER
7. AUTHOR(s) 1st Lt Maria E. Badessa		8. CONTRACT OR GRANT NUMBER(s)
9. PERFORMING ORGANIZATION NAME AND ADDRESS Air Force Weapons Laboratory (NTYV) Kirtland Air Force Base, NM 87117		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS 62601F/88092220
11. CONTROLLING OFFICE NAME AND ADDRESS Air Force Weapons Laboratory (NTYV) Kirtland Air Force Base, NM 87117		12. REPORT DATE July 1980
		13. NUMBER OF PAGES 178
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)		15. SECURITY CLASS. (of this report) Unclassified
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report)  Approved for public release; distribution unlimited.		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Survivability                      Optimization Base Escape                        Nuclear Weapon Allocation Flush		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This report provides instructions for using the QUANTA computer code, a code developed within the Applied Physics Division of the Air Force Weapons Laboratory to study the survivability of a flushing aircraft force from a nuclear attack of sea launched ballistic missiles. Included topics are structure of the input deck, description of the restart capabilities, details of array sizes, and a list of the error messages that might be encountered. The most current version of the QUANTA code is attached as Appendix A.		

DD FORM 1473  
1 JAN 73

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

## SUMMARY

The basic purpose of this report is to assist the QUANTA user in running the code efficiently. Included topics are structure of the input deck, description of the restart capabilities, details of array sizes, and a list of the error messages that may be encountered. It should be expected that occasional problems with the program will occur as the user attempts runs with new combinations of parameter values. If a problem is detected which cannot be solved through this documentation, notify the author or the Air Force Weapons Laboratory. Appendix A is a listing of the current version of QUANTA and Appendix B is the output of a run using the sample input data described in the text.

Accession For	
NTIS	<input checked="checked" type="checkbox"/>
DTIC TAB	<input type="checkbox"/>
Unannounced	<input type="checkbox"/>
Justification	
By	
Distribution/	
Availability Codes	
Dist	Avail and/or Special
A	23 CW

CONTENTS

INTRODUCTION	5
INPUT DATA	6
SAMPLE INPUT DATA	12
RESTART OPTION IN QUANTA	17
ARRAY DIMENSIONS	21
ERROR MESSAGES	24
APPENDIX A - QUANTA LISTING	29
APPENDIX B - QUANTA OUTPUT	162

## INTRODUCTION

QUANTA is a computer model developed at the Air Force Weapons Laboratory (AFWL) to study the effects of a sea-launched ballistic missile (SLBM) nuclear attack on targets consisting of a flushing aircraft force. The program QUANTO (Ref. 1) was used as a basis for its mathematical development. Using the technique of Lagrangian multiplier optimization, a near-optimal allocation of SLBMs to targets is calculated. There are three main differences between these two codes. The first and most dramatic difference is that QUANTA simulates the base escape survivability in greater detail. QUANTO essentially attacks the circle about the turn point (not brake release point) where dispersed aircraft may possibly be at the time of weapon arrival. If aircraft are still on the runway or sitting at the brake release point, they still are considered to be evenly distributed within this circle. However, QUANTA attacks the target in two distinct positions: the runway and the circle centered at the turn point, thus giving a more accurate description of the probability of survival for flushing aircraft. The second difference is that QUANTA allows the attacker the option to allocate weapons to the nonalert aircraft at a base by assigning a value to that target. The third is that QUANTA does not allocate weapons which do not attain a certain value of aircraft killed. This value is user specified and will be discussed later in greater detail in the description of input.

This document contains the information needed to construct the input data for QUANTA and make a successful run. In addition, procedures for running with a restart capability are discussed. Notes on array dimensions and problem sizes are also included.

- 
1. QUANTO--A CODE TO OPTIMIZE WEAPON ALLOCATIONS, AFWL-TR-73-242, Kirtland Air Force Base, New Mex., 1974.

## INPUT DATA

The input is read by the subroutines STARTR, READER, PROCES, MARVIN, and ALOCIN in that order. A brief description of the variables that are read and their format will follow. The structure of the data deck is divided into the following categories:

- Initial data card
- Beddown data
- Aircraft parameters
- Submarine data
- Missile parameters and profile
- Aircraft profile
- Cutoff values
- Convergence parameters
- Initial allocation

STARTR will read the initial data card. Variables which determine the sizes of the arrays in QUANTA are on this card.

- Initial data card

Format: 815

Variables:

- NTGTS - number of targets/air bases
- NSUBS - number of submarine locations
- NTYPES - number of types of aircraft
- MXRWAY - maximum number of runways found on a given base
- MTYPES - number of types of missiles
- IOUT - If it equals 1, standard printout. Additional reallocation information will be printed, if it equals 2.
- NACTT - total number of aircraft in scenario
- NMARV - number of cutoff values. If all weapons in the scenario are to be allocated, NMARV must equal 0.

READER will read the beddown data, aircraft parameters, submarine data, and missile parameters and profile. The aircraft beddown data is input as a set of cards for each base. The first card(s) of the set identifies the base, with the number of alert aircraft at that target and is followed by a takeoff sequence list for the alert aircraft. The number of these sets must equal the value of



NTGTS, read by STARTR. The aircraft parameters such as hardness and brake release time will be read from one card per aircraft type. However, one parameter, the distance to the turn point, will be input for all aircraft types preceding aircraft data. The time intervals for takeoff sequences consist of a set of cards containing NTYPES variables. Submarine data will be read from one card per submarine location. The total number of cards must equal NSUBS (which was read from initial data card). The missile parameters and profile is input as a set of cards for each missile type. On the first card of the set will be the missile parameters such as yield and reliability. Following this card will be the missile profile.

- Beddown data

Format: 3F10.4, I5, 5X, 3F10.4/(7F10.4)

Variables:

TGTLAT - target latitude in decimal degrees

TGTLNG - target longitude in degrees

BASVAL - value of the base which also could include a value for nonalert aircraft

NRWAYS - number of runways on base

VALj - number of aircraft of type j on base, j=1 to NTYPES

Format: 7011

Variables:

ISEQ - takeoff sequence of aircraft identified by type number

- Aircraft parameters

Format: 7F10.6

Variables:

DTCENTj - the minimum distance from brake release (start of takeoff roll) to the turn point of aircraft type j, j=1 to NTYPES.

Format: 4F10.4

Variables:

RELVAL - relative value of aircraft

BRTIME - the time, in minutes, between launch of the first SLBMs and the start of takeoff roll of the aircraft. (Assume it is the first to take off.)

PSI - overpressure hardness in lb/in<sup>2</sup>

CAL - vulnerability level to free-field thermal energy in cal/cm<sup>2</sup>

Format: 7F10.4

Variables:

DELTA<sub>i,j,k</sub> - takeoff time intervals in minutes between each ordered pair of aircraft. Type k will follow type j. After all possible combinations are read for single runways, then input dual, triple, etc. i=1 to MXRWAY, j=1 to NTYPES, k=1 to NTYPES. The last integer increments most often; e.g., (1,1,1), (1,1,2), ..., (1,1,NTYPES), (1,2,1), ..., (1,2,NTYPES), etc.

- Submarine data

Format: 2F10.4, 3I5

Variables:

SUBLAT - submarine latitude in degrees

SUBLNG - submarine longitude in degrees

ISUBS - number of submarines at this location

NMPS - number of missiles per submarine. (This number will automatically be the same for each sub at this location.)

MTYPE - missile type by number

- Missile parameters and profile

Format: 7F10.4

Variables:

DELT<sub>M</sub> - launch interval between salvos in minutes

REL - overall reliability of the missile. This includes launch, in-flight, and detonation.

RNGMIN - minimum range in nautical miles

RNGMAX - maximum range in nautical miles

YIELD - warhead yield in kilotons

BURST - height of burst in feet aboveground

RVS - number of reentry vehicles per missile

Format: I5, 5X, 6F10.4/(6F10.4)

Variables:

M<sub>PROF</sub> - number of data points in missile profile

F<sub>TIME</sub>, F<sub>M<sub>RNG</sub></sub> - time in minutes, distance in nautical miles of missile trajectory

PROCES will read the aircraft profile. A set of cards for each aircraft type consists of the following:

- Altitude
- Count

- Flight profile data - measured relative to the brake release for a nonturning aircraft.
- Additional parameters - needed to construct an extended flight profile in ground range and time.
- Environments - must be the same for all types of aircraft.
- Aircraft profile
  - Altitude
    - Format: F10.8
    - Variables:
      - AZ - final level-off altitude in feet above the ground. It must be less than or equal to the maximum (last) altitude in the flight profile.
  - Count
    - Format: I5
    - Variables:
      - NDATA - number of data points in aircraft profile
  - Flight profile data
    - Format: 3F15.8, 2F10.6
    - Variables:
      - F - ground range in feet
      - G - time in seconds
      - A - altitude in feet which is nondecreasing
      - VEL - Mach number describing ground speed
      - ACCEL - level-off acceleration in feet per second squared if the aircraft were to level-off at the altitude specified on this card.

NOTE: Accurate values for distance, time and altitude are important because of the method QUANTA uses to compute kill regions for an aircraft. At the time of weapon arrival, the altitude and distance from brake release of the aircraft are used to calculate the probability of kill. However, the values for VEL and ACCEL are used to accelerate the aircraft from its velocity at level-off altitude to its final escape velocity. The standard equations of motion use these parameters associated with level-off only to determine time-distance pairs for the flight profile. Therefore, it would suffice if every number in VEL and ACCEL arrays were equal to the velocity and acceleration of the aircraft at level-off altitude.

- Additional parameters
  - Format: 3F15.8, F10.6
  - Variables:
    - ALTFM - minimum altitude in feet at which the aircraft attains final Mach

FMACH - final (maximum) Mach number

TINT - time interval, in seconds, used to extend the profile after the aircraft has reached its final escape velocity (60 s is presently used).

XATI - number of data points (in time and distance) that are calculated for the flight profile from the level-off velocity to final escape velocity (10 is presently used).

NOTE: The aircraft is assumed to follow the input flight profile until the level-off altitude is reached. QUANTA then accelerates the aircraft to its final escape velocity which is assumed to be the maximum velocity and is specified as FMACH. However, this cannot occur if XATI is equal to zero or if ALTFM is less than the level-off altitude. If XATI equals zero (i.e., there are no data points between level-off and escape velocity), no acceleration takes place after level-off and the velocity at level-off will define the final escape velocity. If ALTFM is less than the level-off altitude, then there is no acceleration since the aircraft should have reached its final mach in the input profile. After the aircraft has reached final escape, TINT and FMACH are used to determine time-distance pairs. The total number of data points in the extended profile is NXAP.

- Environments

Format: 4F10.8

Variables:

HTE - terrain height

RHO - the albedo factor, which is the fraction (between 0.0 and 1.0) of incident thermal energy which reflects off the ground. For a SAC normal day, the albedo is 0.3. A worst case abnormal day has a higher albedo.

VIS - the visibility in miles; 10 for a SAC normal day

PZ - the water vapor in the air, in millimeters; 5 for a SAC normal day

MARVIN will read the cutoff values. SLBMs which arrive at a target sufficiently late may not produce adequate kill to justify allocation. These SLBMs may be the last (or next to the last) weapons launched. This is a result of the aircraft having enough time to disperse into a larger area. The program will check if a weapon can attain a kill at least as large as the cutoff value. If it does not, that weapon will not be allocated to any real targets but to a dummy target. After an optimum allocation has been reached using this cutoff value, the program will use it as an initial allocation for the next run with a different cutoff value. For this reason, the cutoff values should be in descending order; i.e., highest value read first. This enables the program to be run more efficiently saving the user cost and time. If the cutoff is as low as 0.1,

almost all weapons will be allocated. If it is near 10.0, as little as one-tenth of the weapons will be allocated depending on the scenario.

- Cutoff values

Format: 7F10.5

Variables:

CUT<sub>i</sub> - the slope of the curve defining the relationship between the number of weapons allocated and the probability of kill,  $i=1$  to NMARV.

ALOCIN will read the convergence parameters and the initial allocation. There are three methods by which the iteration process will stop: (1) if the increase in kill becomes insignificant, (2) if the limit for the total number of iterations has been reached, or (3) if the difference in the Lagrangian multipliers becomes relatively small. These criteria are user specified. The initial allocation of missiles to targets is input submarine by submarine. The subs are in the order of the submarine locations with all subs at one location preceding the first sub at the next location.

- Convergence parameters

Format: F10.4, 2I5, F10.4

Variables:

CHGKIL - the value of aircraft killed used as a measure for a significant increase in kill in ITCUT2 iterations, i.e., if in the last ITCUT2 iterations the value killed has not increased by at least CHGKIL, the iterative process will stop.

ITCUT1 - the total number of ITCUT2 iterations in the optimization process, i.e., QUANTA, if not stopped by some other means, will continue through ITCUT1 x ITCUT2 number of iterations.

ITCUT2 - after this number of iterations, QUANTA checks for a significant increase in value killed.

EPSCUT - for an optimum, the Lagrangian multipliers must all be equal. Since this is impossible, a test for convergence is if they are within a tolerance of EPSCUT.

- Initial allocation

Format: 14I5

Variables:

ITGINO - the target number to which the SLBM is allocated. The SLBMs from a submarine will appear in ascending order by salvo. If there are more than 14 salvos on a sub, then continue the allocation on the next card. Begin reading the allocation of the next sub with a new card. If the cutoff value is large, the initial allocation should read - 1 which represents the dummy target.

## SAMPLE INPUT DATA

To assist the reader in developing an input deck, the following pages detail an example of the input data for QUANTA. The first row of numbers on each page of Table 1 are to aid the reader in locating the columns for the variables, while the first number on every line indicates the card number. The first card of input tells that there are four targets, three sub locations, two aircraft types, a maximum of two runways, two missile types, standard printout, 20 aircraft, and one marval run.

The next eight cards identify the four targets. The first base, located somewhere in the Pacific, has a value of 15 for either its importance as a target or for nonalert aircraft. This is to insure that weapons will be drawn down. Aircraft type one precedes aircraft type two in the takeoff sequence on every base. The only target that has two runways is target three.

The following cards describe the two aircraft types. According to the tenth card, the first aircraft has the capability to make its flyout turn 3.5 nmi from brake release. The following two cards identify the aircraft types with their relative value, brake-release time, and overpressure and thermal hardnesses. According to cards 13 and 14, aircraft type one following type one has a take-off interval of 0.25 min. If dual runways exist, the time interval is cut in half.

The following group of nine cards describes submarine and missile parameters. Cards 15 through 17 state the three submarine locations along with the number of missiles on each sub at that location. There are three subs at location two, while locations one and three have only two subs. These cards also show a total of 36 missiles of type one and 56 missiles of type two in this scenario. However, there are 40 weapon groups (NWPNS described later). A weapon group consists of weapons that have the same characteristics, i.e., they are launched at the same time, from the same location, and have the same parameters. The next six cards identify missile types one and two with weapon reliability, yield, height-of-burst and number of RVs. A total of four data points are used to describe the trajectory for each missile.

The next group of 20 cards details the flight profile for aircraft type one. Card number 24 says that this aircraft reaches level-off altitude of 10,000 ft., but the flight profile indicates that it reaches a maximum Mach of 0.9 at a

TABLE 1. SAMPLE DATA DECK

	1	2	3	4	5	6	7	8	9	0	1	2	3	4	5	6	7	8	9	0
1.		4	3	2	2	2	1	20	1											
2.		13.5833	144.9167			15.0		1		2.0		1.0								
3.	112																			
4.		44.8	68.8333			2.0		1		1.0		3.0								
5.	1222																			
6.		33.9167	84.5167					2		4.0		5.0								
7.	111122222																			
8.		33.4333	112.1667			10.0		1		4.0										
9.	1111																			
10.		3.5	5.5																	
11.		2.5	3.5			1.0		96.0												
12.		1.0	4.2			1.5		120.0												
13.		0.25	0.5			0.5		0.5		0.125		0.25						0.25		
14.		0.25																		
15.		36.75	74.0			2	18	1												
16.		28.05	93.45			3	12	2												
17.		45.65	126.05			2	10	2												
18.		0.2	0.9			250.0		2250.0		1000.0		7000.0						2.0		
19.		4	3.5			250.0		5.5		950.0		7.5		1600.0						
20.		9.5	2250.0																	
21.		0.25	0.85			650.0		2000.0		800.0		6000.0		3.0						
22.		4	5.0			650.0		7.5		1100.0		10.0		1550.0						
23.		12.5	2000.0																	
24.	10000.0																			
25.	16		PROFILE 1																	
26.			0.0			0.0				0.0		0.0								
27.			1500.0			7.5				5.0		0.13								
28.			3700.0			19.0				7.0		0.17								
29.			5700.0			30.0				16.0		0.20								
30.			9000.0			48.0				75.0		0.25								
31.			13000.0			63.0				230.0		0.34								
32.			20000.0			79.5				250.0		0.45								
33.			33000.0			105.0				500.0		0.60								

TABLE 1. CONTINUED.

123456789012345678901234567890123456789012345678901234567890														
34.	50000.0				130.0			1250.0			0.75			
35.	63000.0				150.0			2300.0			0.80			
36.	72000.0				160.0			2800.0			0.90			
37.	90000.0				180.0			4500.0			0.90			
38.	98000.0				195.0			5800.0			0.90			
39.	105000.0				200.0			7000.0			0.90			
40.	110000.0				205.0			9200.0			0.90			
41.	115000.0				210.0			10000.0			0.90			
42.	2800.0	0.9			60.0									
43.	0.0	0.3			10.0			5.0						
44.	5000.0													
45.	11	PROFILE 2												
46.	0.0				0.0			0.0			6.2			
47.	2000.0				20.0			9.0			0.14		6.2	
48.	3900.0				30.0			30.0			0.14		6.2	
49.	6200.0				40.0			92.0			0.19		6.2	
50.	9500.0				50.0			360.0			0.25		6.2	
51.	13400.0				60.0			500.0			0.31		6.2	
52.	15600.0				66.0			500.01			0.35		6.2	
53.	55900.0				125.0			500.11			0.68		6.2	
54.	61000.0				132.0			1425.0			0.70		6.2	
55.	68000.0				140.0			3950.0			0.72		6.2	
56.	75500.0				148.0			5000.0			0.73		6.2	
57.	7600.0	0.849			60.0			10.0						
58.	0.0	0.3			10.0			5.0						
59.	0.5													
60.	0.1	10			100			0.01						
61.	1	2	3	4	1	2	3	-1	-1	-1	-1	-1	-1	-1
62.	-1	-1	-1	-1										
63.	1	2	3	4	4	2	3	1	-1	-1	-1	-1	-1	-1
64.	-1	-1	-1	-1										
65.	1	1	1	2	2	2	3	3	3	4	4	4		
66.	1	1	1	2	2	3	2	3	3	4	4	4		



AFWL-TR-79-193

TABLE 1. CONCLUDED.

	<u>1</u>	<u>2</u>	<u>3</u>	<u>4</u>	<u>5</u>	<u>6</u>	<u>7</u>	<u>8</u>	<u>9</u>	<u>0</u>	<u>1</u>	<u>2</u>	<u>3</u>	<u>4</u>	<u>5</u>	<u>6</u>	<u>7</u>	<u>8</u>	<u>9</u>	<u>0</u>	<u>1</u>	<u>2</u>	<u>3</u>	<u>4</u>	<u>5</u>	<u>6</u>	<u>7</u>	<u>8</u>	<u>9</u>	<u>0</u>	
67.		4	4	4	3	3	3	2	2	2	1	1	1																		
68.		1	0	2	0	3	0	4	0	-1	-1																				
69.		1	0	2	0	3	0	4	0	-1	-1																				

lower altitude of 2,800 ft. This is stated on cards 36 and 42. For this reason, the acceleration is zero on all profile cards and on card 42 XATI is also zero. QUANTA will simply extend the profile using FMACH and TINT (card 42) to find time-distance pairs. Cards 44 through 58 describe the flight profile for aircraft type two. The first card of this group shows a level-off altitude of 5,000 ft. After it reaches this altitude it will accelerate at  $6.2 \text{ ft/s}^2$  (card number 56) until it reaches a final mach of 0.849 at an altitude of 7,600 ft (card number 57). A total of 10 data points will identify this interval in the flight profile (XATI on card 57). At 60 s intervals, distance will be computed by QUANTA to complete the profile. Please note that cards 43 and 58 have the same values for the environments.

For this one marval run, the cutoff value on card 59 is 0.5. The next card, which is the convergence parameters card, states the three conditions which may terminate the iterative process: (1) after every 100 iterations, QUANTA will check for an increase of kill of at least 0.1 value points, (2) there will be no more than 1,000 iterations, and (3) if the difference between the largest and smallest Lagrangian multiplier is less than 0.01, an optimum solution has been reached.

The last group of cards which describes the initial allocation matrix consists of a total of nine cards. The first seven missiles from each sub at location one will be allocated to real targets (cards 61 and 63). The rest of the weapons will go to the dummy target since the user feels they will not attain enough kill. All of the missiles at sub location two will be allocated while some at the third sub location will not. This is shown by the zeros appearing on the last two cards. This is a mathematical representation of missiles being used for other time urgent targets such as communications.

## RESTART OPTION IN QUANTA

The restart option, pertinent for CDC systems, permits the QUANTA user to resume calculations for a particular scenario without the loss of an excessive amount of time. For example, if the computer should crash after the program has been executing for 20 minutes, all is not lost. With a restart tape, the user can recover the computations close to the point of interruption.

There are three methods by which QUANTA writes a restart tape. First, if sense switch one is turned on (controlled by the operator), the program will write the essential variables onto the restart file. In the example mentioned above, the operator would turn the switch on before the computer crashed, thereby enabling QUANTA to write the tape and stop execution gracefully. The second method will also terminate the problem for insufficient time. After ITCUT2 iterations have been completed in the optimization process, QUANTA verifies that there is ample time for another ITCUT2 iteration. Third, during each run, the restart file will be automatically written after every fifth ITCUT1 iteration (i.e., 5 x ITCUT2, 10 x ITCUT2, etc.). This is to insure that the user can still obtain a tape even if something disastrous should happen. If there is any doubt the program will not be completed in the time allotted, the user should save the restart tape.

If the user chooses to save the file, it must be specified in the control language during the initial run. The local file name of the tape is TAPE13 and should be referenced as such throughout the initial run and all subsequent runs. The QUANTA user has the option of storing the restart file on magnetic tape or disk. When starting with a restart tape that is on permanent file, sense switch two must be turned on. If the sense switch is on and the file does not exist, QUANTA will abort. A sequence of commands appearing in the control cards for obtaining a permanent file on an initial run is:

```
REQUEST (TAPE13, *PF)
COPY (ZILCH, TAPE13)
FTN (I = COMPILE, S, S = PFMTEXT, . . .)
.
.
.
CATALOG (TAPE13, FILENAME, ID = . . .)
```

and for that restart run,

```
ATTACH (TAPE13, FILENAME, ID = . . .)
SWITCH(2)
FTN (I = COMPILE, S, S = PFMTEXT, . . .)
.
.
.
CATALOG (TAPE13, FILENAME, ID = . . .)
```

The first two cards in the above restart run replace the first two cards of the initial run. During all QUANTA runs, the FTN card requires the S, S = PFMTEXT parameters for compilation. The user may choose to catalogue TAPE13 on all subsequent runs.

At this point it becomes very apparent that the restart capability in QUANTA is machine dependent in its language. In particular, the ALTER and EXTEND routines are in job control language for the CDC computers. Before attempting to use the program on a computer other than the CDC, consult computer manuals for equivalent commands.

On a restart run, data are read just as in the initial run. QUANTA will use these data in the beginning of the program to set up arrays and compute the survivability matrix which for storage purposes is too large to be put onto the tape. When QUANTA begins the reallocation process (for finding the optimal laydown), it will check a restart file, if one exists. The information from that file will be used as a closer approximation to the optimal solution. Figure 1 demonstrates the above procedures.

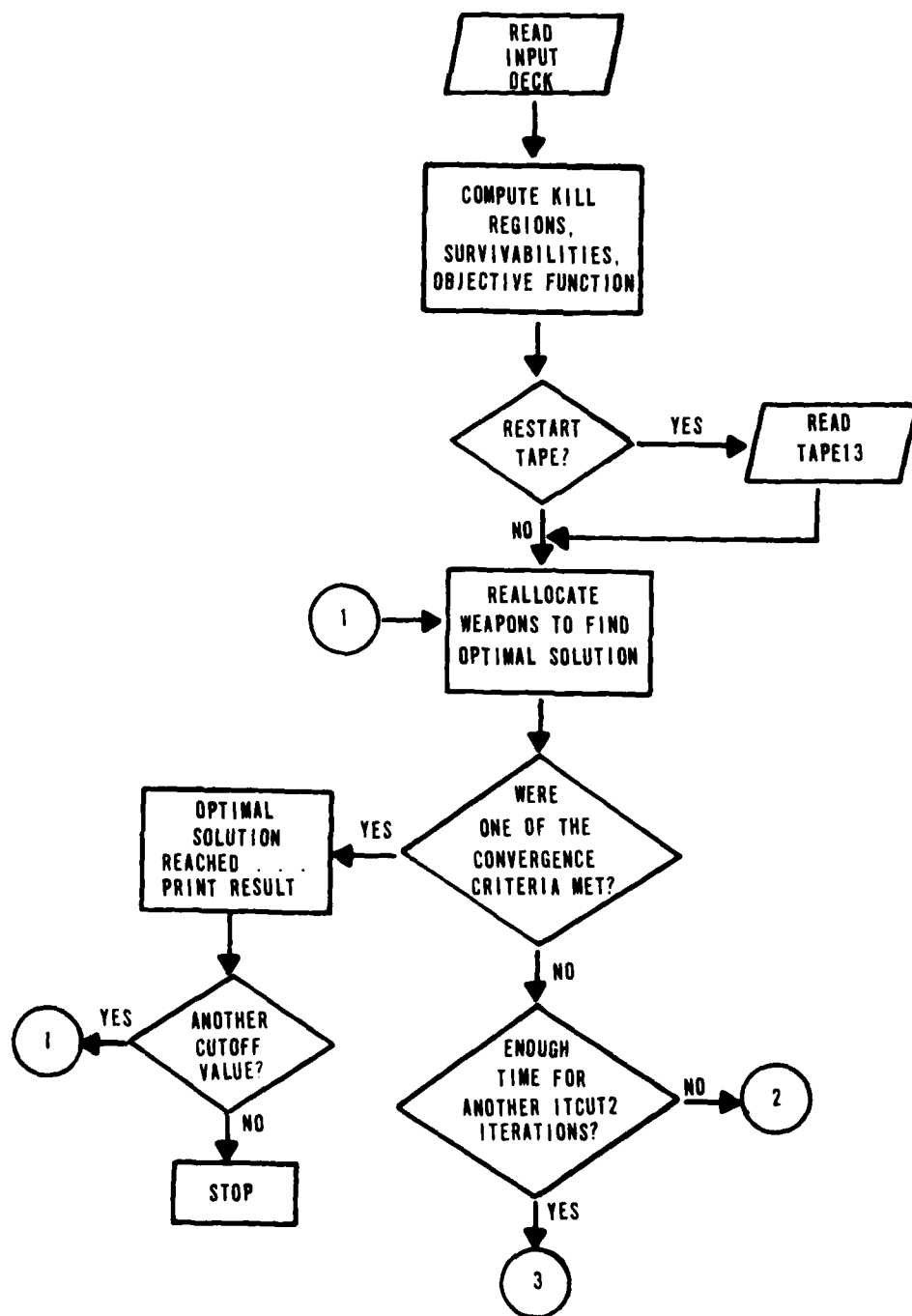


Figure 1. Flow chart.

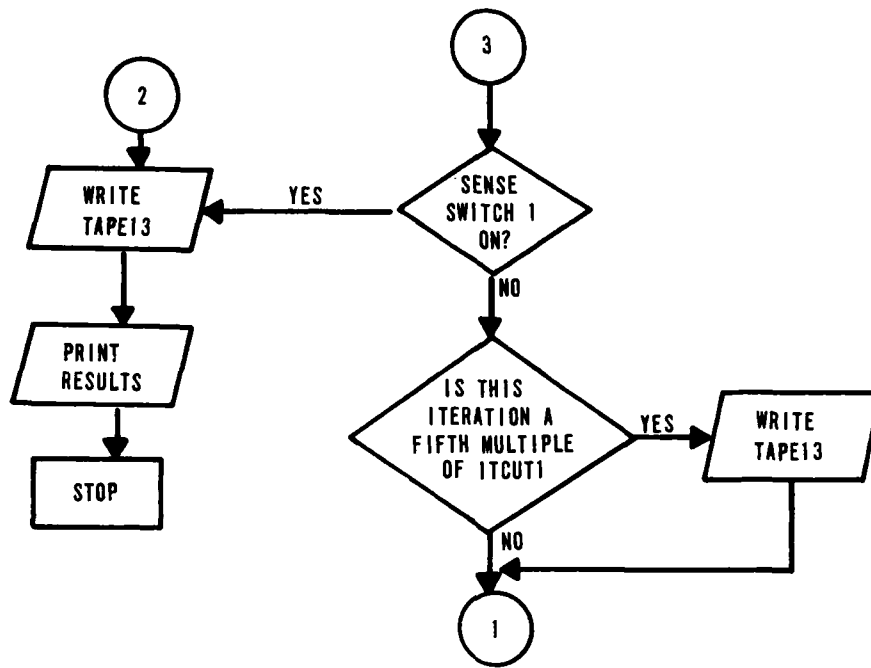


Figure 1. Concluded.

## ARRAY DIMENSIONS

This section is to give the reader a better understanding of the program itself and to delineate the variables within the code that must be changed with problem size. Internally, QUANTA sets up four large arrays. In the main routine, they are named WORK1, WORK2, ALOC, and FLAMB.

The WORK1 array comprises a number of small arrays which have been read from input and will be utilized throughout the execution of the program. One example is the array containing the relative value of the aircraft. This variable is essential in the calculation of the total probability of kill which is continuously recomputed during the iterative process.\* There are 12 such arrays in the WORK1 array and its size is determined by the subroutines WORK1 and REMW1. The formula for the size is given below.

After QUANTA reads and verifies all the input, it begins calculations for the survivability of aircraft at a target against all weapons. Since the size of this matrix can become extremely large, these computations are stored onto tape (TAPE4) for mass storage (machine dependent). After this is completed, most of the variables, such as target and submarine locations, needed for these calculations are no longer required. Therefore, in order to save core, the WORK2 array, originally storing such variables, is then used for computations which define the objective function. For this reason, two messages are printed onto output for the required WORK2 array size. The first message tells how much storage is needed for the input variables, while the second tells the amount of core needed to compute the probability of kill. The subroutines WORK2, REMW2, and SECW2 calculate the size and the formulas for both which are given below. The user should make the size of the WORK2 array at least as large as the maximum of the two.

The size is the same for both the ALOC and FLAMB arrays. The ALOC array stores the allocation matrix and the FLAMB array is used for the Lagrangian multiplier matrix. Their dimension should be set to  $3 \times \text{NWPNS} \times \text{NTGTS}$ , where NTGTS is the number of targets and NWPNS is the number of weapon groups, not total number of weapons. To compute NWPNS add the number of missiles (described as NMPS in input) at each submarine location (not each sub at the location).

---

\*Through this reallocation process, QUANTA finds an optimal missile laydown by moving weapons from target to target.

If the user has not provided adequate core for all these arrays, an error message will be printed and execution stopped. The program does this check by comparing the values of NLCM1, NLCM2, and NLCM3, with the required dimension sizes. A data statement in the main program defining NLCM1, NLCM2, and NLCM3 should be set to the number of words in WORK1, WORK2, and ALOC, respectively. Stated below are the variables which determine the dimensions of the arrays. Most of them are read from the initial card of input.

NLCM1 = NTGTS (number of targets)  
 + (NTGTS + 1) x NTYPES (types of aircraft)  
 + 3 x NSUBS (number of sub locations)  
 + MTYPES (types of missiles)  
 + NACT (number of aircraft)  
 + NMARV (number of marval runs)  
 + NWPNS (total number of weapon groups)  
 + 2 x NWPNS x MXNAPB (maximum number of aircraft found  
 at a given target)

NLCM2 = 3 x NTGTS  
 + 5 x NTYPES  
 + NTYPES x NTYPES x MXRWAY (maximum runways on a given  
 target)  
 + 63 x NTYPES x MTYPES  
 + 7 x MTYPES  
 + 2 x NSUBS (number of sub locations)  
 + 2 x NTYPES x NXAP (number of data points in the extended  
 aircraft profile)  
 + 6 x NTYPES x NPAP (maximum of data points in the aircraft  
 profile)  
 + 2 x MTYPES x MXMPR (maximum points in missile trajectory)  
 + 2 x MXNAPB  
 + MXNMPS (maximum of the number of missiles per sub - NMPS)  
 + 30

NLCM2\* = NACT  
 + 2 x NTGTS  
 + 3 x NTYPES  
 + MTYPES  
 + 4 x MXNAPB

---

\*The value defined in the program should be the maximum of the two NLCM2 formulas.



$$NLCM3 = 3 \times NTGTS \times NWPNS$$

There is a data statement in the main routine which may affect the size of WORK2. The variables NPAP, NXAP, and MXMPR are in the equation for the first NLCM2 above. NPAP is the maximum of the number of data points (described in input as NDATA) of all the aircraft profiles. NXAP is the desired number of time-distance pairs in the extended profile for all aircraft types. MXMPR is the maximum of the number of pairs (MPROF in input) in the missile trajectories. These values should be appropriately defined in the DATA statement.

There is another array in the main program that must change with problem size. INDX sets up the index for reading and writing the large survivability matrix on mass storage. Its dimension must be at least  $2 \times NTGTS + 1$ . A data statement defining NDX must also be set to this value. As with the WORK arrays, if the size is incorrect, an error message will be printed indicating the problem.

Outside of the main program, in particular in four subroutines, there are arrays which must be dimensioned properly to insure complete execution. In subroutines SETS, OUTRNG, and ZERO an array BASENO must be the size of NTGTS. The data statement which checks its correct size is in subroutine ZERO. In subroutine BOSS arrays FN, ST, and STT must be at least as large as NMARV (the number of marval runs). The data statement initializing these arrays must also be changed.

With each new problem, the user must insure that the dimensions of all these arrays are adequate for storage. With each array there is an integer that must equal the value of its dimension. The purpose is to allow QUANTA's built-in check system to verify sufficient core for problem size.

## ERROR MESSAGES

In order to minimize the number of errors that could occur in such a large code as QUANTA, a series of checks were developed for the input data. However, these checks do not enable the program to sense when a typographical error has been made by the user. For example, it cannot determine that the aircraft overpressure hardness was meant to read 1.0 when in actuality it reads 10. For this reason, the program will print the variables as they are read so that the user may verify the quantities. QUANTA also checks the variables when read but in a general sense. For example, it can detect if the aircraft vulnerability levels and weapon yields are positive values.

Table 2 lists all the error messages QUANTA could issue and the remedies for these errors. When an error is detected, the program will stop execution immediately following a message printed in the day file and at the end of output. The latter message will identify the subroutine along with an error number and a brief description of the problem.

TABLE 2. ERROR DESCRIPTION

<u>Subroutine/Error No.</u>	<u>Message</u>	<u>What To Do</u>
REMW1		
1	Size of WORK1 array exceeds dimension.	The dimension of the WORK1 array is too small for your problem size. Change its dimension to what the required size reads. Also change NLCM1 in the data statement.
SECW2		
1	Size of WORK2 array exceeds dimension.	The dimension of the WORK2 array is too small for your problem size. Change its dimension to what the required size reads. Also change NLCM2 in the data statement.
REMW2		
1	Size of WORK2 array exceeds dimension.	Same as SECW2-1.
STARTR		
1-5	Variable read must be greater than 0.	Change the first card of input to read nonnegative numbers.
6	IOUT must be either 1 or 2.	Change the sixth variable on the first card of input to comply with message.
7-8	Variable read must be greater than 0.	Change NACT or NMARV to comply.
READER		
1	Total number of aircraft is greater than original input.	The number of aircraft that was read in is less than the total number added from each base. Check the number of aircraft at each base. If that is correct, then change the first card (NACT). Otherwise, change the number at the base which is incorrect.

TABLE 2. CONTINUED.

Subroutine/Error No.	Message	What To Do
READER (cont.)		
2	Base latitude and longitude must be greater than 0.	Change the variables so that they are positive.
3	Number of runways on a base must be greater than 0 and not greater than the maximum number of runways.	Check to make sure that all bases have the correct number of runways. If it is not right, change that particular card. Otherwise, change the first card of input (MXRWAY) to reflect the maximum of the number of runways on a base.
4	Number of aircraft of a given type cannot be less than 0.	Change the variable VAL so that it is nonnegative.
5	An aircraft type on a base must be greater than 0 and not greater than the number of types.	Change the takeoff sequence ISEQ so that the values read will be from 1 to NTYPES (which is read on the first card).
6-13	Variables read must be greater than 0.	Change the variables so that they are positive.
14	The type of sub must be greater than 0 and not greater than the total.	Change the missile type of a sub location so that its value is between 1 and MTYPES (which is read on the first card of input); or, change MTYPES to comply.
15	The number of time/distance pairs cannot be greater than MXMPR.	MXMPR is a data statement in the main program which is the maximum of the number of pairs in the missile profile. Check that number against the profiles of each type. Change the appropriate value.
16	The time interval between salvo launches must be greater than 0.	Change DELTM so that it is positive.

TABLE 2. CONTINUED.

<u>Subroutine/Error No.</u>		<u>Message</u>	<u>What To Do</u>
READER (cont.)			
17		The reliability of a missile must be greater than 0 and less than 1.	Change the value of REL to comply with message.
18		The maximum range of the missile must be greater than its minimum range.	Change the maximum range RNGMAX or the minimum range RNGMIN to comply.
19-23		The variables read must be greater than 0.	Change the variables to comply with messages.
PROCES			
1		The level-off altitude of the aircraft must be greater than 0.	Change AZ to a positive value.
2		The number of data points in aircraft profile is larger than NPAP.	NPAP is in a data statement in the main program. It is the maximum of the number of points in the aircraft profile. Check it against all aircraft types. Change the appropriate value.
3-5		Variables read cannot be less than 0.	Change the first card in the profile so that the variables are nonnegative.
6-7		The ground range and time must be strictly increasing.	Check that each variable read on consecutive cards is increasing in value. Change those that are not.
8-11		Variables read must be positive.	Change the additional parameters card so that the variables comply with messages.
12-15		Variables read must be positive.	Change the variables on the environments card so that they meet the requirements specified in the error message.

TABLE 2. CONCLUDED.

<u>Subroutine/Error No.</u>	<u>Message</u>	<u>What To Do</u>
PROCES (cont.)		
16	Mach at level-off cannot be greater than final Mach.	Check the Mach at the level-off altitude and FMACH to insure that the values comply with error message.
MARVIN		
1	CUT cannot be less than 0.	Change the variable so that it is positive.
ALOCIN		
1-4	Variables read must be greater than 0.	Change the convergence parameters card so that the variables are positive.
5	The target number receiving this weapon must be between -1 and NTGTS.	Change the variables to comply with error message.
DTLINE		
1-8	Root cannot be found.	Check the vulnerability levels for the aircraft and weapon yield for validity.

AFWL-TR-79-193

APPENDIX A  
QUANTA LISTING

```

1  PROGRAM WUWU1A,IPUT,OUTPUT,TAPES,TAPES=INPUT,TAPES=INPUT,TAPES=INPUT
2  COMMON/LC/LC(806)
3  COMMON/LMC/LMC(656)
4  COMMON/LMC3/LC(408)
5  COMMON/LMC4/LC(408)
6  COMMON/IMP/IMP(100)
7  COMMON/IR/IR(100)
8  COMMON/IR/IR(100)
9  COMMON/IR/IR(100)
10 COMMON/IR/IR(100)
11 COMMON/IR/IR(100)
12 COMMON/IR/IR(100)
13 COMMON/IR/IR(100)
14 COMMON/IR/IR(100)
15 COMMON/IR/IR(100)
16 COMMON/IR/IR(100)
17 COMMON/IR/IR(100)
18 COMMON/IR/IR(100)
19 COMMON/IR/IR(100)
20 COMMON/IR/IR(100)
21 COMMON/IR/IR(100)
22 COMMON/IR/IR(100)
23 COMMON/IR/IR(100)
24 COMMON/IR/IR(100)
25 COMMON/IR/IR(100)
26 COMMON/IR/IR(100)
27 COMMON/IR/IR(100)
28 COMMON/IR/IR(100)
29 COMMON/IR/IR(100)
30 COMMON/IR/IR(100)
31 COMMON/IR/IR(100)
32 COMMON/IR/IR(100)
33 COMMON/IR/IR(100)
34 COMMON/IR/IR(100)
35 COMMON/IR/IR(100)
36 COMMON/IR/IR(100)
37 COMMON/IR/IR(100)
38 COMMON/IR/IR(100)
39 COMMON/IR/IR(100)
40 COMMON/IR/IR(100)
41 COMMON/IR/IR(100)
42 COMMON/IR/IR(100)
43 COMMON/IR/IR(100)
44 COMMON/IR/IR(100)
45 COMMON/IR/IR(100)
46 COMMON/IR/IR(100)
47 COMMON/IR/IR(100)
48 COMMON/IR/IR(100)
49 COMMON/IR/IR(100)
50 COMMON/IR/IR(100)
51 COMMON/IR/IR(100)
52 COMMON/IR/IR(100)
53 COMMON/IR/IR(100)
54 COMMON/IR/IR(100)
55 COMMON/IR/IR(100)
56 COMMON/IR/IR(100)
57 COMMON/IR/IR(100)
58 COMMON/IR/IR(100)
59 COMMON/IR/IR(100)
60 COMMON/IR/IR(100)
61 COMMON/IR/IR(100)
62 COMMON/IR/IR(100)
63 COMMON/IR/IR(100)
64 COMMON/IR/IR(100)
65 COMMON/IR/IR(100)
66 COMMON/IR/IR(100)
67 COMMON/IR/IR(100)
68 COMMON/IR/IR(100)
69 COMMON/IR/IR(100)
70 COMMON/IR/IR(100)
71 COMMON/IR/IR(100)
72 COMMON/IR/IR(100)
73 COMMON/IR/IR(100)
74 COMMON/IR/IR(100)
75 COMMON/IR/IR(100)
76 COMMON/IR/IR(100)
77 COMMON/IR/IR(100)
78 COMMON/IR/IR(100)
79 COMMON/IR/IR(100)
80 COMMON/IR/IR(100)
81 COMMON/IR/IR(100)
82 COMMON/IR/IR(100)
83 COMMON/IR/IR(100)
84 COMMON/IR/IR(100)
85 COMMON/IR/IR(100)
86 COMMON/IR/IR(100)
87 COMMON/IR/IR(100)
88 COMMON/IR/IR(100)
89 COMMON/IR/IR(100)
90 COMMON/IR/IR(100)
91 COMMON/IR/IR(100)
92 COMMON/IR/IR(100)
93 COMMON/IR/IR(100)
94 COMMON/IR/IR(100)
95 COMMON/IR/IR(100)
96 COMMON/IR/IR(100)
97 COMMON/IR/IR(100)
98 COMMON/IR/IR(100)
99 COMMON/IR/IR(100)
100 COMMON/IR/IR(100)

```



```

51 * #WKRZ(INFISA),#WKRZ(NFLMT),#WKRZ(NBUNUS))
52 CALL MARKV, (MARKV,WKRZ(NCUT),IMARV)
53 CALL ALLOC (INTGTS,NSUBS,NMPS,MANAP,ALOC,WKRZ(NALUCU),
54 * WKRZ(INISUBS),WKRZ(NMPS),WKRZ(NFLMT),#WKRZ(NALUCU))
55 CALL LETHAL(WKRZ(NMPS),#WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),
56 * WKRZ(NS),#WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
57 * WKRZ(NS),#WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
58 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
59 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
60 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
61 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
62 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
63 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
64 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
65 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
66 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
67 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
68 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
69 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
70 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
71 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
72 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
73 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
74 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
75 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
76 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
77 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
78 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
79 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
80 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
81 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
82 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
83 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
84 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
85 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
86 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
87 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
88 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
89 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
90 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
91 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
92 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
93 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
94 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
95 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
96 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
97 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
98 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
99 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))
100 * WKRZ(NFLMT),#WKRZ(NALUCU),#WKRZ(NMPS),#WKRZ(NALUCU))

```

IF (IQUIT.EQ.1) UM, ISSW,CG,] CALL TERM (IQUIT,ISSW)

PAGE 3

```
101 C
102 IF (IMARKV.LL.IMARKV .AND. .IMARKV.GT.0) GO TO 80
103 STOP
104 802 FORMAT(IX,' THE REQUIRED SIZE FOR THE ALUC AND FLAMB ARRAYS IS ',
105 ' 17,75 THE SIZE YOU HAVE DESIGNATED IS 9,17)
106 801 FORMAT (IX,' THE REQUIRED SIZE FOR THE INDX ARRAY IS 9,17)
107 ' ' THE SIZE YOU HAVE DESIGNATED IS 9,17)
108 END
109
```

QUANTA  
QUANTA  
QUANTA  
QUANTA  
QUANTA  
QUANTA  
QUANTA

102  
103  
104  
105  
106  
107  
108  
109

```

109 SUBROUTINE WUKK1(N1GTS,N1TYPES,N5SUBS,NVAL,NKEL,NVAR,N1SUBS,N1NMP5,
110 *N1TYPE,NWUK1,NLUM),N1SUBNACT,NKEL,N1TYPES,NBASVA)
111
112 SUBROUTINE WUKK1 CALCULATES SUBARRAY STARTING
113 ADDRESSES IN THE WUKK1 ARRAY
114
115 NVAL=1
116 NKELJA=NVAL*N1GTS*N1TYPES
117 N1SUBS=NKELJA*N1TYPES
118 N1NMP5=N1SUBS*N5SUBS
119 N1TYPE=N1NMP5*N1SUBS
120 NKEL=NKEL*N1TYPES
121 N1SUBNACT=N1SUBS*NACT
122 N1NMP5=N1SUBS*N1GTS
123 IF ((NWUK1-1)*G1,NLUM),N1GTS,1) NWUK1,NLUM)
124 RETURN
125
126 DOUO PUMAT1/30M SUBROUTINE WUKK1 HAS DETECTED IMAT1/3
127 * 30M THE REQUIRED WUKK1 ARRAY SIZE IS AT LEAST 110,/,
128 * 30M THE PROVIDED WUKK1 ARRAY SIZE IS 110,/.
129 * 30M HENCE AN ERROR WILL BE DETECTED LATER IF WE DOUO BOMB FIRST)
130
131 END

```

PAGE 5

```
129 SUBROUTINE REMM1(NBARR1,NBARR2,NSURV,NALUO,NCL,NLUM1,NBARR3,MANAPB) 130
130 * NSURV) 131
131 SUBROUTINE REMM1 CALCULATES THE REMAINING SUBARRAY 132
132 STARTING ADDRESSES IN THE SUBARRAY 133
133 DATA NMEME/5NMEME/ 134
134 NSURV=NBARR1 135
135 NSURV=NBARR2 136
136 NALUO=NSURV+NBARR3+MANAPB 137
137 NCL=NALUO+NMEME 138
138 NBARR1=NCL+NBARR2-1 139
139 WRITE (6,6000)NBARR1,NLUM1 140
140 IF (NBARR1.GT.NLUM1) CALL ABORT('MEME+1"SIZE OF SUBARR1 ARRAY EXCEED 141
141 IS DIMENSION") 142
142 RETURN 143
143 6000 FORMAT(14H THE REQUIRED SUBARR1 ARRAY SIZE IS *110*% 144
144 * 34H THE PROVIDED SUBARR1 ARRAY SIZE IS *110) 145
145 END 146
```

```

146 SUPROUTINE SECURENTGTS,NTYPES,NUMCZ,PRODSUM,AVALL,SIZEOF,AN,INACT
147 • ISUM,NSUM,NUMCZ,NSUM,INACT,AVALL,NUMCZ,PRODSUM,NTYPES
148
149 SUBROUTINE SECURE CALCULATES SUMMARY STATISTICS
150
151 DATA WHERE/DBSECZ/
152
153
154 CALCULATE STARTING ADDRESSES
155
156
157
158
159
160
161
162
163
164
165
166
167
168
169
170
171

```

[illegible]

220	SUBROUTINE REMK2(NWORK,MANAP,MANAP,NDI,NIN,INCL,MAN)	QUANTA	221
221	SUBROUTINE REMK2 CALCULATES THE STARTING ADDRESSES OF	QUANTA	222
222	THE REMAINING SUBARRAYS IN THE WORK2 ARRAY	QUANTA	223
223	DATA WHERE/5NREM2/	QUANTA	224
224	I=0;I=IWORK	QUANTA	225
225	NINCL=NDI+MANAP	QUANTA	226
226	NMAN=NINCL+MANAP	QUANTA	227
227	NWORK=NMAN+MANAP-1	QUANTA	228
228	WRITE(6,5000)NWORK,INCL	QUANTA	229
229	IF (NWORK.GT.INCL) CALL ADUMI(WHERE,1,SIZE OF WORK2 ARRAY EXCEED	QUANTA	230
230	IS DIMENSION")	QUANTA	231
231	RETURN	QUANTA	232
232	FORMAT(1,34) THE REQUIRED WORK2 ARRAY SIZE IS *110*.	QUANTA	233
233	* 34* THE PROVIDED WORK2 ARRAY SIZE IS *110)	QUANTA	234
234	END	QUANTA	235

235	1	SUBROUTINE ABOUT (WHERE,NUM,MSG)	QUANTA	235
236	0	DIMENSION MSG(12)	QUANTA	237
237	0		QUANTA	238
238	0	WRITE (6,3) NUM,WHERE	QUANTA	239
239	0	DO 1 L=1,12	QUANTA	240
240	0	IF (MSG(L).E9.0) GO TO 2	QUANTA	241
241	0	1 CONTINUE	QUANTA	242
242	0	L=13	QUANTA	243
243	0		QUANTA	244
244	0	2 L=L-1	QUANTA	245
245	0	IF (L.GT.0) WRITE (6,4) (MSG(I),I=1,L)	QUANTA	246
246	0		QUANTA	247
247	0	STOP "PROGRAM ABOUT "	QUANTA	248
248	0		QUANTA	249
249	0	3 FORMAT (1X,12I10,10X,12A10)	QUANTA	250
250	0	4 FORMAT (1X,5H-----,5A,12A10)	QUANTA	251
251	0	END	QUANTA	252
252	0		QUANTA	253



```

253 SUBROUTINE STARTK(NTUTS,NSUBS,NTYPES,MAXWAY,NTYPE,LOUT,INACT,INMAY 254
254 1) 255
255 DATA WHERE/BNSTART/ 256
256 READ(5,5000) NTUTS,NSUBS,NTYPES,MAXWAY,NTYPE,LOUT,INACT,INMAY 257
257 CALL PAGE(0) 258
258 *WRITE(6,0010) *MAP,NTUTS,NSUBS,NTYPES,INACT,NTYPES 259
259 IF(NTUTS.LE.0) CALL ABORT(WHERE,1,"NUMBER OF BASES MUST BE GREATER 260
260 1 THAN 0") 261
261 IF(NSUBS.LE.0) CALL ABORT(WHERE,2,"NUMBER OF SUBS MUST BE GREATER 262
262 1 THAN 0") 263
263 IF(NTYPES.LE.0) CALL ABORT(WHERE,3,"NUMBER OF AIRCRAFT TYPES MUST 264
264 1BE GREATER THAN 0") 265
265 IF(NTYPES.LE.0) CALL ABORT(WHERE,4,"NUMBER OF MISSILE TYPES MUST B 266
266 1 GREATER THAN 0") 267
267 IF(MAXWAY.LE.0) CALL ABORT(WHERE,5,"MAXIMUM NUMBER OF RUNWAYS ON A 268
268 1 BASE MUST BE GREATER THAN 0") 269
269 IF((LOUT.NE.1).AND.(LOUT.NE.2)) CALL ABORT(WHERE,6,"LOUT MUST BE C 270
270 1 EITHER 1 OR 2") 271
271 IF(INACT.LE.0) CALL ABORT(WHERE,7,"THE TOTAL NUMBER OF AIRCRAFT MUS 272
272 1 BE GREATER THAN 0") 273
273 IF(INMAY.LE.0) CALL ABORT(WHERE,8,"THE NUMBER OF MARVAL RUNS CANN 274
274 1 BE NEGATIVE") 275
275 CALL PAGE(2) 276
276 RETURN 277
277 5000 FORMAT(1X,0) 278
278 0010 FORMAT(1X,0) 279
279 15,0 TARGETS, 0.15,0 SUB LOCATIONS, 0.10,0.15,0 TYPES OF AIRCRAFT 280
280 1 (TOTAL OF 0.15,0 ), AND 0.15,0 TYPES OF MISSILES,0) 281
281 282
282 283

```

```

283 SUBROUTINE HEADR(INITS,INSUBS,NTYPES,MTYPE,ISEL,TOTLAT,TOTLNG,UTCENT,MKWAYS,BRTIME,
284 * MELVAL,ISUBS,MKPS,MTYPE,ISEL,TOTLAT,TOTLNG,UTCENT,MKWAYS,BRTIME,
285 * PSI,CAL,DELTA,C,SUBLAT,SUBLON,DELTA,MEL,MKMIN,MKMAX,YIELD,BURST,
286 * PSI,MKPRUF,BRTIME,MKMIN,MKMAX,MKPS,MKVAL,
287 DIMENSION VAL(INITS,NTYPES),MELVAL(NTYPES),ISUBS(INSUBS),MKPS(INSUBS)
288 * ,MTYPE(INSUBS),ISEL(INITS),TOTLAT(INITS),TOTLNG(INITS),
289 * MKWAYS(NTYPES),BRTIME(NTYPES),PSI(NTYPES),CAL(NTYPES),DELTA(C,MK
290 * MAX,NTYPES,NTYPES),SUBLAT(INSUBS),SUBLNG(INSUBS),UTCENT(NTYPES),MEL(M
291 * KWAYS,MKMIN(NTYPES),MKMAX(NTYPES),YIELD(MTYPES),BURST(MTYPES),M
292 * KPS(MTYPES),MKPRUF(MTYPES),BRTIME(MKMAX,MTYPES),MKMIN(MKMAX,MTYPES)
293 * ,UTCENT(NTYPES),BASVAL(INITS)
294 * ,LEVEL,CAL,MELVAL,ISUBS,MKPS,MTYPE,ISEL,TOTLAT,TOTLNG,UTCENT,
295 * MKWAYS,BRTIME,PSI,CAL,DELTA,C,SUBLAT,SUBLNG,DELTA,MEL,MKMIN,MKMAX,
296 * YIELD,BURST,MKPS,MKPRUF,BRTIME,MKMIN,MKMAX,BASVAL
297 DATA MPRUF/0.17532425/
298 * ,MELVAL/0.17532425/
299 * ,MELVAL/0.17532425/
300 * ,MELVAL/0.17532425/
301 * ,MELVAL/0.17532425/
302 * ,MELVAL/0.17532425/
303 * ,MELVAL/0.17532425/
304 * ,MELVAL/0.17532425/
305 * ,MELVAL/0.17532425/
306 * ,MELVAL/0.17532425/
307 * ,MELVAL/0.17532425/
308 * ,MELVAL/0.17532425/
309 * ,MELVAL/0.17532425/
310 * ,MELVAL/0.17532425/
311 * ,MELVAL/0.17532425/
312 * ,MELVAL/0.17532425/
313 * ,MELVAL/0.17532425/
314 * ,MELVAL/0.17532425/
315 * ,MELVAL/0.17532425/
316 * ,MELVAL/0.17532425/
317 * ,MELVAL/0.17532425/
318 * ,MELVAL/0.17532425/
319 * ,MELVAL/0.17532425/
320 * ,MELVAL/0.17532425/
321 * ,MELVAL/0.17532425/
322 * ,MELVAL/0.17532425/
323 * ,MELVAL/0.17532425/
324 * ,MELVAL/0.17532425/
325 * ,MELVAL/0.17532425/
326 * ,MELVAL/0.17532425/
327 * ,MELVAL/0.17532425/
328 * ,MELVAL/0.17532425/
329 * ,MELVAL/0.17532425/
330 * ,MELVAL/0.17532425/
331 * ,MELVAL/0.17532425/
332 * ,MELVAL/0.17532425/
333 * ,MELVAL/0.17532425/

```

```

333      30 CONTINUE
334      FMAC=FLUAT(FMAC-INAC1)*1.0
335      NLINES=(FMAC-1.)/30.
336      CALL PAGE(-MAX(12,INTYPES)-NLINES-2)
337      WRITE(6,BU10)IBASVAL(1),TOTLAT(1),TOTLNG(1),NRWAYS(1),J,VAL(1,J)
338      *J=1,INTYPES)
339      IF((TOTLAT(1).LT.0.0).OR.(TOTLNG(1).LT.0.0)) CALL ABORT(WHERE*2,"
340      BASE LATITUDE AND LONGITUDE MUST BE GREATER THAN 0")
341      IF(NRWAYS(1).LE.0 .OR. NRWAYS(1).GT.MAXWAY) CALL ABORT(WHERE*3,"NO
342      NUMBER OF RUNWAYS ON A BASE MUST BE GREATER THAN 0 AND NOT GREATER T
343      HAN THE MAXIMUM NUMBER OF RUNWAYS")
344      DO 35 J=1,INTYPES
345      IF(VAL(1,J).LT.0.0) CALL ABORT(WHERE*4,"NUMBER OF AIRCRAFT OF A GI
346      VEN TYPE ON A GIVEN BASE CANNOT BE LESS THAN 0")
347      35 CONTINUE
348      WRITE(6,BU20)(ISEV(IAC),IAC=INAC1,INAC)
349      DO 37 IAC=INAC1,INAC
350      IF((ISEV(IAC).LE.0).OR.((ISEV(IAC).GT.INTYPES)) CALL ABORT(WHERE*5,"
351      IAC AIRCRAFT TYPE ON A BASE MUST BE GREATER THAN 0 AND NOT GREATER
352      THAN THE NUMBER OF TYPES")
353      37 CONTINUE
354      40 CONTINUE
355      *WRITE AIRCRAFT TYPE PARAMETERS
356      CALL PAGE(-INTYPES-3)
357      WRITE(6,BU30)(J,RELVAL(J),ORTIME(J),ULCENT(J),PSI(J),CAL(J),J=1,IN
358      *TYPES)
359      DO 45 J=1,INTYPES
360      IF(PSI(J).LE.0.0) CALL ABORT(WHERE*6,"AIRCRAFT OVERPRESSURE MUST
361      BE GREATER THAN 0")
362      IF(CAL(J).LE.0.0) CALL ABORT(WHERE*7,"THE VULNERABILITY LEVEL OF T
363      HE AIRCRAFT TO FREE-FIELD THERMAL ENERGY CANNOT BE LESS THAN 0")
364      CALL TO 0")
365      IF(ULCENT(J).LE.0.0) CALL ABORT(WHERE*8,"THE DISTANCE FROM ORIGIN
366      RELEASE POINT TO THE TURN POINT MUST BE GREATER THAN 0")
367      IF(ORTIME(J).LE.0.0) CALL ABORT(WHERE*9,"THE BRAKE RELEASE TIME MU
368      ST BE GREATER THAN 0")
369      45 CONTINUE
370      *WRITE TAKEOFF INTERVALS MAIN1X
371      CALL PAGE(-MAXWAY*INTYPES-3)
372      WRITE(6,BU40)((IIM*JLU,KFL,UELTAC(IIM*JLU,KFL)*KFL=1,INTYPES),
373      * JLU=1,INTYPES),IIM=1,MAXWAY)
374      DO 47 IIM=1,MAXWAY
375      DO 47 JLU=1,INTYPES
376      IF(UELTAC(IIM*JLU,KFL).LE.0.0) CALL ABORT(WHERE*10,"THE TAKE-OFF I
377      INTERVALS BETWEEN AIRCRAFT TYPES MUST BE GREATER THAN 0")
378      47 CONTINUE
379      *END SUB LOCATION CARDS
380      NMPNS=0
381      MAXMPS=0
382

```

```

383      DO 50 I=1,NSUBS
384      READ(5,5000)SUBLAT(I),SUBLONG(I),ISUBS(I),NMPS(I),MYPE(I)
385      MAXMPS=MAX0(MAXMPS,NMPS(I))
386      NMPS=NMPS+NMPS(I)
387      50 CONTINUE
388      WRITE SUB LOCATION CARDS
389      CALL PAGE(-NSUBS-2)
390      WRITE(6,6000)(I,SUBLAT(I),SUBLONG(I),ISUBS(I),NMPS(I),MYPE(I),
391      *I=1,NSUBS)
392      DO 55 I=1,NSUBS
393      IF (SUBLAT(I).LT.0.0).OR.(SUBLONG(I).LT.0.0))CALL ABORT(WHERE,I,"I
394      THE SUB LATITUDE AND LONGITUDE MUST BE GREATER THAN 0")
395      IF (ISUBS(I).LE.0) CALL ABORT(WHERE,I,"THE NUMBER OF SUBS AT A GIV
396      IEN LOCATION MUST BE GREATER THAN 0")
397      IF (NMPS(I).LE.0) CALL ABORT(WHERE,I,"THE NUMBER OF MISSILES ON A
398      IL SUBS AT A GIVEN LOCATION MUST BE GREATER THAN 0")
399      IF (MYPE(I).LE.0).OR.(MYPE(I).GT.1)CALL ABORT(WHERE,I,"THE
400      IE TYPE OF SUB MUST BE GREATER THAN 0 AND NOT GREATER THAN THE TOTA
401      EL NUMBER OF SUB TYPES")
402      55 CONTINUE
403      CALL PAGE(-MYPES-2)
404      DO 70 J=1,MYPES
405      NSUBT=0
406      DO 60 I=1,NSUBS
407      IF (MYPE(I).EQ.J)NSUBT=NSUBT+ISUBS(I)
408      60 CONTINUE
409      WRITE(6,6000)J,NSUBT
410      70 CONTINUE
411      READ SUB TYPE PARAMETERS AND PROFILES
412      DO 80 I=1,MYPES
413      READ(5,5000)DELTM(I),REL(I),KNOMIN(I),KNOMAX(I),YIELD(I),BURST(I),
414      *MVS(I)
415      READ(5,5000)MFM, (P,TIME(J),J=1,MFM)
416      IF (MFM.GT.MAXMFM) CALL ABORT(WHERE,I,"NUMBER OF TIME/DISTANCE PAIR
417      IS CANNOT BE GREATER THAN MAXMFM")
418      MPMOF(I)=MFM
419      80 CONTINUE
420      WRITE SUB TYPE PARAMETERS AND PROFILES
421      CALL PAGE(-MYPES-3)
422      WRITE(6,6000)(J,DELTM(J),REL(J),KNOMIN(J),KNOMAX(J),YIELD(J),BURST
423      *(J),MVS(J),J=1,MYPES)
424      DO 85 J=1,MYPES
425      IF (DELTM(J).LE.0.0) CALL ABORT(WHERE,I,"THE TIME INTERVAL BETWEEN
426      SALVO LAUNCHES MUST BE GREATER THAN 0")
427      IF ((REL(J).LE.0.0).OR.(REL(J).GE.1.0))CALL ABORT(WHERE,I,"THE REL
428      IABILITY OF A MISSILE MUST BE GREATER THAN 0 AND LESS THAN 1")
429      IF (KNOMAX(J).LE.KNOMIN(J)) CALL ABORT(WHERE,I,"THE MAXIMUM RANGE
430      OF THE MISSILE MUST BE GREATER THAN ITS MINIMUM RANGE")
431      IF (YIELD(J).LE.0.0) CALL ABORT(WHERE,I,"THE YIELD OF THE MISSILE
432

```

QUANTA 384  
 QUANTA 385  
 QUANTA 386  
 QUANTA 387  
 QUANTA 388  
 QUANTA 389  
 QUANTA 390  
 QUANTA 391  
 QUANTA 392  
 QUANTA 393  
 QUANTA 394  
 QUANTA 395  
 QUANTA 396  
 QUANTA 397  
 QUANTA 398  
 QUANTA 399  
 QUANTA 400  
 QUANTA 401  
 QUANTA 402  
 QUANTA 403  
 QUANTA 404  
 QUANTA 405  
 QUANTA 406  
 QUANTA 407  
 QUANTA 408  
 QUANTA 409  
 QUANTA 410  
 QUANTA 411  
 QUANTA 412  
 QUANTA 413  
 QUANTA 414  
 QUANTA 415  
 QUANTA 416  
 QUANTA 417  
 QUANTA 418  
 QUANTA 419  
 QUANTA 420  
 QUANTA 421  
 QUANTA 422  
 QUANTA 423  
 QUANTA 424  
 QUANTA 425  
 QUANTA 426  
 QUANTA 427  
 QUANTA 428  
 QUANTA 429  
 QUANTA 430  
 QUANTA 431  
 QUANTA 432  
 QUANTA 433



PAGE 13

404	0110F10.4.3A.0B.4.9A.F10.3.F10.3.F10.4.4A.F10.2.10A.F4.1)	QUA:IA	484
405	CUBU FURMAT (/13M MISSILE TYPE.11X.4M TIME.5A.CHANGE/113.5A.2F10.4/(10A	QUA:IA	485
406	1.2F10.4))	QUA:IA	486
406	END	QUA:IA	487

```

487 SUBROUTINE PROCES(PSI,CAL,YIELD,NTYPES,MTYPES,NPAP,NXAP,SDU,
488 * AXP,VS,VEL,ACCEL,NUDATA,PLPP,FTSA,PLRT,BURST)
489 QUANTA
490 QUANTA
491 QUANTA
492 QUANTA
493 QUANTA
494 QUANTA
495 QUANTA
496 QUANTA
497 QUANTA
498 QUANTA
499 QUANTA
500 QUANTA
501 QUANTA
502 QUANTA
503 QUANTA
504 QUANTA
505 QUANTA
506 QUANTA
507 QUANTA
508 QUANTA
509 QUANTA
510 QUANTA
511 QUANTA
512 QUANTA
513 QUANTA
514 QUANTA
515 QUANTA
516 QUANTA
517 QUANTA
518 QUANTA
519 QUANTA
520 QUANTA
521 QUANTA
522 QUANTA
523 QUANTA
524 QUANTA
525 QUANTA
526 QUANTA
527 QUANTA
528 QUANTA
529 QUANTA
530 QUANTA
531 QUANTA
532 QUANTA
533 QUANTA
534 QUANTA
535 QUANTA
536 QUANTA
537 QUANTA

SUBROUTINE PROCES(PSI,CAL,YIELD,NTYPES,MTYPES,NPAP,NXAP,SDU,
* AXP,VS,VEL,ACCEL,NUDATA,PLPP,FTSA,PLRT,BURST)
DIMENSION PSI(NTYPES),CAL(NTYPES),YIELD(NTYPES),S(INAP,NTYPES),
U(NXAP,NTYPES),A(NPAP,NTYPES),F(INPAP,NTYPES),G(INPAP,NTYPES),VS
(INPAP,NTYPES),VEL(INPAP,NTYPES),ACCEL(NPAP,NTYPES),NUDATA(NTYPES),
* PLPP(NTYPES),FTSA(NTYPES),PLRT(NTYPES),BURST(NTYPES),
* BURST(NTYPES)
THIS SUBROUTINE IS USED TO INPUT DATA FOR AIRCRAFT AND IS USED
TO GENERATE NOISE EFFECTS GEOMETRICALLY FOR SPECIFIED HAPNESS
LEVELS VIA SUBROUTINES SPARK AND SNAKE
DIMENSION JUM(13)
COMMON/PASS/KHU,VIS,PZ,MIE
LOGICAL SNWE,VALU
LEVEL 25 PSI,CAL,YIELD,U,S,A,F,G,VS,VEL,ACCEL,NUDATA,
* PLPP,FTSA,PLRT,BURST
DATA UELT,CMIT,CFM /1.0001,3.2000,0.3000/
DATA WHERE,BNPRUGES/
UU 130 I=1,NTYPES
CALL PAGE (U)
HEAD (5,500)M2
HEAD (5,500)N
NUDATA(I)=M
IF(AZ,LE,U,U) CALL ABOUT(WHERE,1,"THE LEVEL-OFF ALTITUDE OF THE AI
IRCRAFT MUST BE GREATER THAN 0")
IF(N,G,INPAP) CALL ABOUT(WHERE,2,"THE NUMBER OF DATA POINTS IN AIR
IRCRAFT PROFILE IS LARGER THAN NPAP")
ICAL=ICAL(I)
WRITE (6,600)I,NTYPES
WRITE (6,600) PSI(I),ICAL
WRITE (6,600)
CALL PAGE (17)
THE FOLLOWING READS AIRCRAFT PROFILE INPUT DATA AND ADJUSTS THE
ALTITUDE (IF NECESSARY) FOR USE BY AUSE WHICH REQUIRES IT TO BE
STRICTLY MONOTONICALLY INCREASING. A-ALTITUDE (FEET);
P-GROUND RANGE (FEET); J-TIME (SEC); VEL-MACH NUMBER;
ACCEL-ACCELERATION (FEET/SEC/SEC). THE VELOCITY OF SOUND (VS)
GIVEN ALTITUDE IS CALCULATED BY FUNCTION SSP.
HEAD (5,520) F(1),G(1),A(1),VEL(1),ACCEL(1)
IF(A(1),LT,0.0) CALL ABOUT(WHERE,3,"THE AIRCRAFT ALTITUDE CANNOT
BE LESS THAN 0")
IF(F(1),LT,0.0) CALL ABOUT(WHERE,4,"THE AIRCRAFT GROUND RANGE FM
THE BRAKE RELEASE POINT CANNOT BE LESS THAN 0")
IF(G(1),LT,0.0) CALL ABOUT(WHERE,5,"THE TIME FROM THE BRAKE RELEASE
POINT CANNOT BE LESS THAN 0")
ALT=CFM+A(1)
VS(1)=CMIT*SSP(ALT)

```





PAGE 18

```

507      WRITE (6,600) VMAZ,FMACH      QUANTA 588
508      FIMAZ=VMAZ*FMACH              QUANTA 589
509      FMAF=VMAF*FMACH              QUANTA 590
510      WRITE (6,610) FIMAZ,FMAF    QUANTA 591
511      IF (VMAZ.GT.FMACH) CALL ABORT('WHERE,16,"MACH AT LEVEL OFF CANNOT BE QUANTA 592
512      L GREATER THAN FINAL MACH") QUANTA 593
513      QUANTA 594
514      QUANTA 595
515      EQUATIONS OF MOTION: QUANTA 596
516      ACCZ=ACCAZ/2.0 QUANTA 597
517      MANAZ=AUSC(AZ,A(1,1),F(1,1),N) QUANTA 598
518      TIMAZ=AUSC(AZ,A(1,1),G(1,1),N) QUANTA 599
519      UU 50 J=1,N QUANTA 600
520      INDEX=J QUANTA 601
521      IF ( F(J,1).GE.MANAZ .OR. G(J,1).GE.TIMAZ ) GO TO 60 QUANTA 602
522      THE FIRST PART OF THE S AND U ARRAYS IS SIMPLY THE FLIGHT QUANTA 603
523      PROFILE (F,U) READ IN QUANTA 604
524      U(J,1)=F(J,1) QUANTA 605
525      S(J,1)=G(J,1) QUANTA 606
526      CONTINUE QUANTA 607
527      DO QUANTA 608
528      60 U(INDEX,1)=MANAZ QUANTA 609
529      S(INDEX,1)=TIMAZ QUANTA 610
530      VINT=FIMAZ QUANTA 611
531      INDEX=INDEX+1 QUANTA 612
532      IF (VMAZ.EQ.FMACH .OR. AZ.GE.ALTM .OR. XATI.EQ.U.0) GO TO 60 QUANTA 613
533      THE FOLLOWING DEFINES S AND U (PATTI ADDITIONAL VALUES FOR QUANTA 614
534      BOTH ARRAYS) FROM MACH AT LEVEL OFF TO FINAL MACH QUANTA 615
535      TC=TIMAZ**2 QUANTA 616
536      AT=ACCAZ*TIMAZ QUANTA 617
537      VINT=FMAF QUANTA 618
538      IF=TIMAZ*(VINT-TIMAZ)/ACCAZ QUANTA 619
539      U1=(TF-TIMAZ)/XATI QUANTA 620
540      K=INDEX QUANTA 621
541      S(K,1)=S(K-1,1)+UT QUANTA 622
542      SK=S(K,1) QUANTA 623
543      U(K,1)=KANAZ + FIMAZ*(SK-TIMAZ) + ACCZ*(SK**2+T2) -AT*SK QUANTA 624
544      INDEX=INDEX+1 QUANTA 625
545      IF (SK*U1.LT.IF .AND. INDEX.LT.NAAPP-1) GO TO 70 QUANTA 626
546      S(INDEX,1)=IF QUANTA 627
547      U(INDEX,1)=KANAZ + FIMAZ*(IF-TIMAZ) + ACCZ*(IF**2+T2) -AT*IF QUANTA 628
548      IF (ABS(IF-S(K,1)).LT.6.001) INDECA=K QUANTA 629
549      INDEX=INDEX+1 QUANTA 630
550      THE S AND U ARRAYS ARE COMPLETED WITH CONSTANT VELOCITY QUANTA 631
551      DO 90 K=INDEX,NAAPP QUANTA 632
552      S(K,1)=S(K-1,1)+TINT QUANTA 633
553      U(K,1)=U(K-1,1)+VINT*TINT QUANTA 634
554      CONTINUE QUANTA 635
555      WRITE (6,700) QUANTA 636
556      CALL PAUSE (10) QUANTA 637

```

```

637 C
638
639
640
641
642
643
644
645
646
647
648
649
650
651
652
653
654
655
656
657
658
659
660
661
662
663
664
665
666
667
668
669
670
671
672
673
674
675
676
677
678
679
680
681
682
683
684
685
686
687

      CONVERT FEET TO NM AND SECONDS TO MINUTES
      UU 100 N=1,NMAXP
      TEMP1=SIN(I)
      TEMP2=UIN(I)
      SIN(I)=SIN(I)/60.0
      UIN(I)=UIN(I)/600.0
      WRITE (6,10) TEMP2,TEMP1,U(N,I),SIN(I)
      CALL PAGE (1)
      CONTINUE
      COMPUTE OVERPRESSURE AND THERMAL EFFECTS AT A(N,I), MAX ALT
      UU 120 J=1,MYPES
      MBL=BLUMST(J)-MTE
      M=VIELU(J)
      IM=CAL(I)
      UPEPSI(I)
      AZ=A(N,I)-MTE
      MUMF=0.0
      ISA=0.0
      CALL SPARK(2,M,MBL,AZ,MTE,UUM(1),UUM(2),UUM(3),UUM(4),UP,POIN15,
      * AFA,XTPP,XMS,TFA,TTPP,TMS)
      IF (POIN15.EU.0.0) UU TO 110
      MUMF=XMS
      ISA=TMS
      IF (POIN15.EU.0.0) UU TO 110
      MUMF=AFA
      ISA=TFA
      FLAP(I,J)=MUMF/6000.0
      FISA(I,J)=ISA/60.0
      SNNEW=.TRUE.
      CALL SPARK(UUM(5),AZ,0.0,0.0,0.0,MBL,MTE,MHOU,VIS,PZ,U.0.0,0.0,
      * U,UUM,UM,TM,PUR,VALU,SNNEW)
      FLRT(I,J)=MUMF/6000.0
      CONTINUE
      NEXT AIRCRAFT TYPE
      CONTINUE
      RETURN
      FORMAT (6F10.0)
      FORMAT (15)
      FORMAT (15,5,0,2F10.0)
      FORMAT (4A,5SUBROUTINE PROCESS,///,AX,AIRCRAFT TYPE,IC,
      * OF ,IC,0 TYPE(5),/)
      FORMAT (11A,5VULNERABILITY CRITERIA FOR AIRCRAFT TYPE,/)
      * 10X,F5.2,DM PSI,10X,15,0 CAL/CM,3M,0,2/)
      * 10X,11A,0,DATA INPUT FOR AIRCRAFT PROFILE,12X,4M,CM,0,
      * 10X,6M,CM,0,15X,6M,FLIGHT,14X,8M,AIRCRAFT,13X,8M,VELOCITY,11A,
      * 4M,CM,0,5X,9M,LEVEL-UP,12X,8M,NUMBER,9X,5M,ACCEL,17X,4M,TIME,15A,
      * 4M,ALTITUDE,13X,8M,0 SOUND,10X,8M,NUMBER,9X,12,ACCELERATION,/)

```

[illegible]



P 02 22

750	5020 FORMALIN METH. DETECTION, IS 5020.100 100 FROM DETECTION. LINEAL WITH	5020.100	751
751	• = 5020.100 5020.100	5020.100	752
752	5030 FORMALIN (//)	5030.100	753
753	5040 FORMALIN DETECTION, IS 5040.100 100 FROM 5040.100 5040.100	5040.100	754
754	5050.100 PLUS 5050.100 5050.100	5050.100	755
755	END	5050.100	756





```

006      IF (IPLAGUE.EQ.2) CALL ABOMI(MHPEL,0,"ROOT CANNOT BE FOUND")
007      FIND HAS FOUND
008      AC=0
009      A1=XC
010      AC=Z*UTP
011      CALL MEPLALS(PAS,X1,X2,100,00,0,0,XFA,IPLAGUE,(1,1),A(1,1))
012      IF (IPLAGUE.EQ.1) GO TO 145
013      IF (IPLAGUE.EQ.2) CALL ABOMI(MHPEL,0,"ROOT CANNOT BE FOUND")
014      A=MAX1(PAS,XFA)
015      BACK UP POINT
016      MAC=AUSC(X,F(1,1),A(1,1),MAF)-NTE
017      MESURF((U-X)*02*(MAC-ME)*02)
018      RUMU=1
019      CALL BLINI(MH,MH,MAC,NTE,MTE,RUMU)
020      TSW=AP*PDSK/00.
021      IAP=POLUT(A/0000,0(1,1),0(1,1),000)
022      FETA-TSA
023      T=MAX1(0,1)
024      A=PHOFLOT(1,0(1,1),0(1,1),000)0000.
025      A=MAX1(P,0)
026      UHEU THERMAL EFFECT AT X
027      TEST=THML(X,F(1,1),A(1,1))
028      IF (TEST .LE. 0.) GO TO 200
029      FIND THERMAL BOUND
030      AC=0
031      A1=X2
032      AC=Z*UTP
033      CALL MEPLALS(IMML,X1,X2,100,00,0,0,XFA,IPLAGUE,(1,1),A(1,1))
034      IF (IPLAGUE.EQ.2) CALL ABOMI(MHPEL,0,"ROOT CANNOT BE FOUND")
035      IF (IPLAGUE.EQ.1) GO TO 100
036      A=ATH
037      IPSIDE=A
038      C
039      C
040      C
041      C
042      C
043      C
044      C
045      C
046      C
047      C
048      C
049      C
050      C
051      C
052      C
053      C
054      C
055      C
056      C
057      C
058      C
059      C
060      C
061      C
062      C
063      C
064      C
065      C
066      C
067      C
068      C
069      C
070      C
071      C
072      C
073      C
074      C
075      C
076      C
077      C
078      C
079      C
080      C
081      C
082      C
083      C
084      C
085      C
086      C
087      C
088      C
089      C
090      C
091      C
092      C
093      C
094      C
095      C
096      C
097      C
098      C
099      C
100      C
101      C
102      C
103      C
104      C
105      C
106      C
107      C
108      C
109      C
110      C
111      C
112      C
113      C
114      C
115      C
116      C
117      C
118      C
119      C
120      C
121      C
122      C
123      C
124      C
125      C
126      C
127      C
128      C
129      C
130      C
131      C
132      C
133      C
134      C
135      C
136      C
137      C
138      C
139      C
140      C
141      C
142      C
143      C
144      C
145      C
146      C
147      C
148      C
149      C
150      C
151      C
152      C
153      C
154      C
155      C
156      C
157      C
158      C
159      C
160      C
161      C
162      C
163      C
164      C
165      C
166      C
167      C
168      C
169      C
170      C
171      C
172      C
173      C
174      C
175      C
176      C
177      C
178      C
179      C
180      C
181      C
182      C
183      C
184      C
185      C
186      C
187      C
188      C
189      C
190      C
191      C
192      C
193      C
194      C
195      C
196      C
197      C
198      C
199      C
200      C
201      C
202      C
203      C
204      C
205      C
206      C
207      C
208      C
209      C
210      C
211      C
212      C
213      C
214      C
215      C
216      C
217      C
218      C
219      C
220      C
221      C
222      C
223      C
224      C
225      C
226      C
227      C
228      C
229      C
230      C
231      C
232      C
233      C
234      C
235      C
236      C
237      C
238      C
239      C
240      C
241      C
242      C
243      C
244      C
245      C
246      C
247      C
248      C
249      C
250      C
251      C
252      C
253      C
254      C
255      C
256      C
257      C
258      C
259      C
260      C
261      C
262      C
263      C
264      C
265      C
266      C
267      C
268      C
269      C
270      C
271      C
272      C
273      C
274      C
275      C
276      C
277      C
278      C
279      C
280      C
281      C
282      C
283      C
284      C
285      C
286      C
287      C
288      C
289      C
290      C
291      C
292      C
293      C
294      C
295      C
296      C
297      C
298      C
299      C
300      C
301      C
302      C
303      C
304      C
305      C
306      C
307      C
308      C
309      C
310      C
311      C
312      C
313      C
314      C
315      C
316      C
317      C
318      C
319      C
320      C
321      C
322      C
323      C
324      C
325      C
326      C
327      C
328      C
329      C
330      C
331      C
332      C
333      C
334      C
335      C
336      C
337      C
338      C
339      C
340      C
341      C
342      C
343      C
344      C
345      C
346      C
347      C
348      C
349      C
350      C
351      C
352      C
353      C
354      C
355      C
356      C
357      C
358      C
359      C
360      C
361      C
362      C
363      C
364      C
365      C
366      C
367      C
368      C
369      C
370      C
371      C
372      C
373      C
374      C
375      C
376      C
377      C
378      C
379      C
380      C
381      C
382      C
383      C
384      C
385      C
386      C
387      C
388      C
389      C
390      C
391      C
392      C
393      C
394      C
395      C
396      C
397      C
398      C
399      C
400      C
401      C
402      C
403      C
404      C
405      C
406      C
407      C
408      C
409      C
410      C
411      C
412      C
413      C
414      C
415      C
416      C
417      C
418      C
419      C
420      C
421      C
422      C
423      C
424      C
425      C
426      C
427      C
428      C
429      C
430      C
431      C
432      C
433      C
434      C
435      C
436      C
437      C
438      C
439      C
440      C
441      C
442      C
443      C
444      C
445      C
446      C
447      C
448      C
449      C
450      C
451      C
452      C
453      C
454      C
455      C
456      C
457      C
458      C
459      C
460      C
461      C
462      C
463      C
464      C
465      C
466      C
467      C
468      C
469      C
470      C
471      C
472      C
473      C
474      C
475      C
476      C
477      C
478      C
479      C
480      C
481      C
482      C
483      C
484      C
485      C
486      C
487      C
488      C
489      C
490      C
491      C
492      C
493      C
494      C
495      C
496      C
497      C
498      C
499      C
500      C
501      C
502      C
503      C
504      C
505      C
506      C
507      C
508      C
509      C
510      C
511      C
512      C
513      C
514      C
515      C
516      C
517      C
518      C
519      C
520      C
521      C
522      C
523      C
524      C
525      C
526      C
527      C
528      C
529      C
530      C
531      C
532      C
533      C
534      C
535      C
536      C
537      C
538      C
539      C
540      C
541      C
542      C
543      C
544      C
545      C
546      C
547      C
548      C
549      C
550      C
551      C
552      C
553      C
554      C
555      C
556      C
557      C
558      C
559      C
560      C
561      C
562      C
563      C
564      C
565      C
566      C
567      C
568      C
569      C
570      C
571      C
572      C
573      C
574      C
575      C
576      C
577      C
578      C
579      C
580      C
581      C
582      C
583      C
584      C
585      C
586      C
587      C
588      C
589      C
590      C
591      C
592      C
593      C
594      C
595      C
596      C
597      C
598      C
599      C
600      C
601      C
602      C
603      C
604      C
605      C
606      C
607      C
608      C
609      C
610      C
611      C
612      C
613      C
614      C
615      C
616      C
617      C
618      C
619      C
620      C
621      C
622      C
623      C
624      C
625      C
626      C
627      C
628      C
629      C
630      C
631      C
632      C
633      C
634      C
635      C
636      C
637      C
638      C
639      C
640      C
641      C
642      C
643      C
644      C
645      C
646      C
647      C
648      C
649      C
650      C
651      C
652      C
653      C
654      C
655      C
656      C
657      C
658      C
659      C
660      C
661      C
662      C
663      C
664      C
665      C
666      C
667      C
668      C
669      C
670      C
671      C
672      C
673      C
674      C
675      C
676      C
677      C
678      C
679      C
680      C
681      C
682      C
683      C
684      C
685      C
686      C
687      C
688      C
689      C
690      C
691      C
692      C
693      C
694      C
695      C
696      C
697      C
698      C
699      C
700      C
701      C
702      C
703      C
704      C
705      C
706      C
707      C
708      C
709      C
710      C
711      C
712      C
713      C
714      C
715      C
716      C
717      C
718      C
719      C
720      C
721      C
722      C
723      C
724      C
725      C
726      C
727      C
728      C
729      C
730      C
731      C
732      C
733      C
734      C
735      C
736      C
737      C
738      C
739      C
740      C
741      C
742      C
743      C
744      C
745      C
746      C
747      C
748      C
749      C
750      C
751      C
752      C
753      C
754      C
755      C
756      C
757      C
758      C
759      C
760      C
761      C
762      C
763      C
764      C
765      C
766      C
767      C
768      C
769      C
770      C
771      C
772      C
773      C
774      C
775      C
776      C
777      C
778      C
779      C
780      C
781      C
782      C
783      C
784      C
785      C
786      C
787      C
788      C
789      C
790      C
791      C
792      C
793      C
794      C
795      C
796      C
797      C
798      C
799      C
800      C
801      C
802      C
803      C
804      C
805      C
806      C
807      C
808      C
809      C
810      C
811      C
812      C
813      C
814      C
815      C
816      C
817      C
818      C
819      C
820      C
821      C
822      C
823      C
824      C
825      C
826      C
827      C
828      C
829      C
830      C
831      C
832      C
833      C
834      C
835      C
836      C
837      C
838      C
839      C
840      C
841      C
842      C
843      C
844      C
845      C
846      C
847      C
848      C
849      C
850      C
851      C
852      C
853      C
854      C
855      C
856      C
857      C
858      C
859      C
860      C
861      C
862      C
863      C
864      C
865      C
866      C
867      C
868      C
869      C
870      C
871      C
872      C
873      C
874      C
875      C
876      C
877      C
878      C
879      C
880      C
881      C
882      C
883      C
884      C
885      C
886      C
887      C
888      C
889      C
890      C
891      C
892      C
893      C
894      C
895      C
896      C
897      C
898      C
899      C
900      C
901      C
902      C
903      C
904      C
905      C
906      C
907      C
908      C
909      C
910      C
911      C
912      C
913      C
914      C
915      C
916      C
917      C
918      C
919      C
920      C
921      C
922      C
923      C
924      C
925      C
926      C
927      C
928      C
929      C
930      C
931      C
932      C
933      C
934      C
935      C
936      C
937      C
938      C
939      C
940      C
941      C
942      C
943      C
944      C
945      C
946      C
947      C
948      C
949      C
950      C
951      C
952      C
953      C
954      C
955      C
956      C
957      C
958      C
959      C
960      C
961      C
962      C
963      C
964      C
965      C
966      C
967      C
968      C
969      C
970      C
971      C
972      C
973      C
974      C
975      C
976      C
977      C
978      C
979      C
980      C
981      C
982      C
983      C
984      C
985      C
986      C
987      C
988      C
989      C
990      C
991      C
992      C
993      C
994      C
995      C
996      C
997      C
998      C
999      C
1000      C

```

BUSH BOUNDARIES ARE KNOWN.  
 LETHAL DISTANCE IS DISTANCE FROM BUSH SIDE TO IP SIDE.  
 MAKE BUSH SIDE AND IPSIDE RELATIVE TO BUSH POINT  
 BUSH SIDE=UNM-BUSH SIDE/0000.  
 IPSIDE=IPSIDE/0000.-00M  
 RETURN  
 END



PAGE 20

```

090 SUBROUTINE MEAFALS(FN,XA,BUM,BUM,NTUL,XTUL,XPTUL,XPLAGS,PAA)
091
092 THIS SUBROUTINE FINDS THE REAL ROOTS OF A FUNCTION GIVEN AS
093 AN EXTERNAL. THE USER MUST GIVE BOUNDARY POINTS THAT LIE ON
094 EITHER SIDE OF THE ROOT. THESE POINTS ARE PA AND PB.
095
096 GIVEN VARIABLES ARE:
097
098 FN - THE FUNCTION GIVEN BY THE USER
099 XA - THE LEFTMOST BOUND ON THE ROOT
100 XB - THE RIGHTMOST BOUND ON THE ROOT
101 NTUL - THE MAXIMUM NUMBER OF ITERATIONS ALLOWED BY USER
102 XTUL - THE TOLERANCE SPECIFIED BY USER FOR THE
103 DIFFERENCE BETWEEN TWO ITERATIONS
104 PTUL - THE MAXIMUM ERROR IN THE FUNCTION AT THE ROOT
105
106 * - THE VALUE OF THE ROOT
107 IFLAG - A FLAG TO TELL THE USER HOW THE PROGRAM RAN
108
109 0. THE ROOT WAS FOUND TO WITHIN THE USERS
110 TOLERANCE.
111 1. THE ENDPOINTS DO NOT BOUND A REAL ROOT
112 2. THE ROUTINE DID NOT CONVERGE TO WITHIN
113 THE USERS TOLERANCES.
114
115 LEVEL 2, PAA
116
117 A=0.0
118 B=0.0
119 P=FN(XA,PAA)
120 Q=FN(XB,PAA)
121
122 CHECK TO SEE IF THE ENDPOINTS BOUND A ROOT.
123
124 SP=SIGN(1.0,P)
125 IF ((SP*Q).LE.0.0001) GO TO 10
126 IFLAG=1
127 GO TO 50
128 IFLAG=0
129
130 W=A
131
132 DO 30 N=1,NTUL
133
134 CHECK FOR SMALL ENOUGH INTERVAL BETWEEN ROOTS
135 IF (ABS((B-A)/C).LE.XTUL) GO TO 50
136
137 CHECK FOR SMALL ENOUGH FUNCTION VALUES
138 IF (ABS(FN).LE.XPTUL) GO TO 50
139 W=((F*B)-(Q*A))/(F-G)
140 SP=SIGN(1.0,PW)
141 PW=FN(W,PAA)
142 IF ((SP*PW).LT.0.0001) GO TO 20
143
144 CALCULATE NEW A, P, AND CUT G IN HALF.
145
146 A=W
147 P=PW
148 IF ((SP*PW).GT.0.0001) G=0.5
149 GO TO 30

```

097 QUANTA  
 098 QUANTA  
 099 QUANTA  
 100 QUANTA  
 101 QUANTA  
 102 QUANTA  
 103 QUANTA  
 104 QUANTA  
 105 QUANTA  
 106 QUANTA  
 107 QUANTA  
 108 QUANTA  
 109 QUANTA  
 110 QUANTA  
 111 QUANTA  
 112 QUANTA  
 113 QUANTA  
 114 QUANTA  
 115 QUANTA  
 116 QUANTA  
 117 QUANTA  
 118 QUANTA  
 119 QUANTA  
 120 QUANTA  
 121 QUANTA  
 122 QUANTA  
 123 QUANTA  
 124 QUANTA  
 125 QUANTA  
 126 QUANTA  
 127 QUANTA  
 128 QUANTA  
 129 QUANTA  
 130 QUANTA  
 131 QUANTA  
 132 QUANTA  
 133 QUANTA  
 134 QUANTA  
 135 QUANTA  
 136 QUANTA  
 137 QUANTA  
 138 QUANTA  
 139 QUANTA  
 140 QUANTA  
 141 QUANTA  
 142 QUANTA  
 143 QUANTA  
 144 QUANTA  
 145 QUANTA  
 146 QUANTA

PAGE 21

```
946 C
947 C
948 C CALCULATE NEW D, G, AND CUT F IN HALF.
949 C D=D*
950 C IF ((S#*F#).GT.0.) F=F/2.
951 C CONTINUE
952 C
953 C SET IFLAG TO 2 IF THE PROGRAM DIDN'T CONVERGE WITHIN LIMITS
954 C IFLAG=2
955 C RETURN
956 C END
```

```
QUANTA
QUANTA
QUANTA
QUANTA
QUANTA
QUANTA
QUANTA
QUANTA
QUANTA
QUANTA
QUANTA
QUANTA
```

```
947
948
949
950
951
952
953
954
955
956
957
```

PAGE 28

```
957 C FUNCTION TPPI(X,F,A)
958 C TRIPLE POINT PATH INTERCEPT.....USED IN OUTLINE
959 COMMON /STUFF/W
960 COMMON /FLICK/UL(5),GU,CTP
961 COMMON /CSTIME/UC(4),NAF
962 LEVEL 2,F,A
963 M1=GU*CTP*(ABS(Q-X)/60-1.)*.01
964 NC=ABS(C(A,F,A,NAF))
965 TPPI=M1-M2
966 RETURN
967 END
```

```
QUANTA
QUANTA
QUANTA
QUANTA
QUANTA
QUANTA
QUANTA
QUANTA
QUANTA
QUANTA
QUANTA
```

```
958
959
960
961
962
963
964
965
966
967
968
```

PAGE 29

```

908      REAL FUNCTION MS(X*0.5)
909      C      MACH SHUCK.....USED IN ULINE
910      COMMON /STUFF/J*HTE
911      COMMON /JUSTIME/MS*HAKUIM*HAKUUP*HAF
912      LEVEL 0*0.5
913      HAF=AUSC(X*0.5*HAF)*HTE
914      KORD=1
915      CALL BLINT(MS*HAF*HTE*HTE*HTE)
916      MS=SUMT(U-A)*0.5*HAF*HTE
917      MS=TPPRUP(S*HTE*HTE*HTE)-HAKUUP
918      RETURN
919      END

```

```

QUANTA 909
QUANTA 910
QUANTA 911
QUANTA 912
QUANTA 913
QUANTA 914
QUANTA 915
QUANTA 916
QUANTA 917
QUANTA 918
QUANTA 919
QUANTA 920

```

901	QUA1A
902	QUA1A
903	QUA1A
904	QUA1A
905	QUA1A
906	QUA1A
907	QUA1A
908	QUA1A
909	QUA1A
910	QUA1A
911	QUA1A
912	QUA1A

```

900      FUNCTION FAS(A,F,A)
901      C FREE AID SHUCK.....USED IN DLINE
902      COMMON /STUP/U,HTC
903      COMMON /LSIME/MB,MARUTH,MARUUP,MMAT
904      LEVEL 2,F,A
905      MAC=AUSC(A,F,A,NAT)-MTE
906      KMDU=1
907      CALL BLINIT(MD,M,MAC,MTE,MTE,KMDU)
908      SM=SUPT((J-A)*%2*(MAC-MB)%2)
909      FAS=MF*RUUP(SM)-MARUUP
910      RETURN
911      END

```

```

997      FUNCTION TRMML(XAF,A)
998      TRMML EFFECTS.....USED IN ULINE
999      COMMON /STUFF/U,MTE
1000     COMMON /CUTIME/MO,MARUTH,MARLOP,M,NAP
1001     COMMON /PASS/MMU,VIS,PZ
1002     LEVEL 2,PFA
1003     LOGICAL SNEW,VALIU
1004     MCL=AUC(XAF,A,NAP)-MLE
1005     CALL SHAME(ABS(U-A),MAC,U,U,0.0,U,M,M,M,MLE,RMC,VIS,PZ,U,U,0.0,U,S)
1006     I=CALL(U,U,SUM,-I,UDUM,VALIU,SNEW)
1007     TRMML=CAL-MARUTH
1008     RETURN
1009     END

```



PAGE 33

1055 40  
1056  
1057  
1058  
1059  
1060  
1061  
1062

ITB=PROFLU(XBMSI,U(1,ITYPE),S(1,ITYPE),NSU)  
I=ITO-TSA  
I=AMAX1(U,IT)  
UIS=XBMSI-PROFLU(T,S(1,ITYPE),U(1,ITYPE),NSU)  
NOW FIND THE TOTAL LETHAL AREA  
UIA=EA=THUPA(KUP,UNM,KTH,UIS,THEIA)  
RETURN  
END

QUANTA 1056  
QUANTA 1057  
QUANTA 1058  
QUANTA 1059  
QUANTA 1060  
QUANTA 1061  
QUANTA 1062  
QUANTA 1063



```

1063 FUNCTION THUPA(RUP,QUANT,THETA)
1064 LEVEL 200
1065
1066 PURPOSE
1067 TO COMPUTE THE AREA OF THE FLOURE FORMED BY THE UNION OF THE
1068 OVER PRESSURE "SQUISH" AND THE THERMAL CIRCLE INTERSECTION WITH
1069 THE SPACE TO THE SIDE OF THE LINE OF FLIGHT WITH DECREASING
1070 THETA.
1071
1072 LOGICAL EXIST,CEXIST
1073 DATA NJINC /500/
1074 DATA EPSLON/-1.0E-8/
1075 INITIALIZE.
1076
1077 THUPA=0.0
1078 THETA=ABS(THETA)
1079 RUPSU=RUP*PRUP
1080 RTHSU=RTH*PRTH
1081 SI=0.
1082 KULU=AMVAL(U*PRUP-PRUJ,QU*PRTH)
1083 KULU=AMVAL(U*PRUP-PRUJ,QU*PRTH)
1084 KULU=U*PRUP-PRUJ
1085 KULU=U*PRUP-PRUJ
1086 KULU=U*PRUP-PRUJ
1087 KULU=U*PRUP-PRUJ
1088 KULU=U*PRUP-PRUJ
1089
1090 IF (U*GE*PRTH).AND.(U*GE*PRUP) THEN TA=AMVAL(THETA,AMVAL(ASIN(RUP/QU)).
1091 1 ASIN(RTH/QU)))
1092 U*THETA=THETA /FLUAT(NJINC)
1093
1094 STARTING AT ZERO INCREMENT SI UP TO THETA COMPUTING AREAS AT
1095 EACH INCREMENT
1096
1097 DO 40 J=1,NJINC
1098 SET UP THE ANGLE.
1099
1100 SI=FLUAT(J)*U*THETA
1101 CUSI=COS(SI)*U
1102 SINI=SIN(SI)*U
1103 SINQU=SIN(SI)*SINI
1104 COMPUTE THE POINTS OF INTERSECTION.
1105 A=1.0E295
1106 B=-1.0E295
1107 EXIST=.FALSE.
1108
1109 DESC=RUPSU-SINQU
1110 IF (DESC.GT.EPSLON.AND.DESC.LT.0.0) DESC = 0.0
1111 IF (DESC.LT.0.0) DO 10
1112 DESC=SUM(DESC)

```

QUANTA 1064  
 QUANTA 1065  
 QUANTA 1066  
 QUANTA 1067  
 QUANTA 1068  
 QUANTA 1069  
 QUANTA 1070  
 QUANTA 1071  
 QUANTA 1072  
 QUANTA 1073  
 QUANTA 1074  
 QUANTA 1075  
 QUANTA 1076  
 QUANTA 1077  
 QUANTA 1078  
 QUANTA 1079  
 QUANTA 1080  
 QUANTA 1081  
 QUANTA 1082  
 QUANTA 1083  
 QUANTA 1084  
 QUANTA 1085  
 QUANTA 1086  
 QUANTA 1087  
 QUANTA 1088  
 QUANTA 1089  
 QUANTA 1090  
 QUANTA 1091  
 QUANTA 1092  
 QUANTA 1093  
 QUANTA 1094  
 QUANTA 1095  
 QUANTA 1096  
 QUANTA 1097  
 QUANTA 1098  
 QUANTA 1099  
 QUANTA 1100  
 QUANTA 1101  
 QUANTA 1102  
 QUANTA 1103  
 QUANTA 1104  
 QUANTA 1105  
 QUANTA 1106  
 QUANTA 1107  
 QUANTA 1108  
 QUANTA 1109  
 QUANTA 1110  
 QUANTA 1111  
 QUANTA 1112

PAGE 35

```

1113      W=CROSS*(PMU)-DESC
1114      B=CROSS*(PMU)*DESC
1115      W=AMAX1(W,0.0)
1116      B=AMAX1(B,0.0)
1117      BEAST1=BEAST
1118
1119      C
1120      U=1.0E295
1121      U=1.0E295
1122      BEAST1=BEAST
1123
1124      W=C*(MISU-SINSU)
1125      IF (DESCUT.EPSLON*AMU*DESC.LT.0.0) DESC = 0.0
1126      IF (DESC.LT.0.0) GO TO 26
1127      W=CROSS1-SUMT(DESC)
1128      W=AMAX1(W,0.0)
1129      W=AMAX1(W,0.0)
1130
1131      C
1132      C
1133      C
1134      C
1135      C
1136      C
1137      C
1138      C
1139      C
1140      C
1141      C
1142      C
1143      C
1144      C
1145      C
1146      C
1147      C
1148      C
1149      C
1150      C
1151      C
1152      C
1153      C
1154      C

```

PAGE 36

1154		SUBROUTINE ZERO (NTOTS,NSUBS)	QUANTA	1155
1155	C		QUANTA	1156
1156	C	INITIALIZES PLAYS TO ZERO	QUANTA	1157
1157	C		QUANTA	1158
1158		COMMON/MNGFLU/BASENU(4/),NOLTS	QUANTA	1159
1159		DATA NUBASE/47/	QUANTA	1160
1160		DATA NOLTS/50/	QUANTA	1161
1161	C		QUANTA	1162
1162	C	CHECK FOR TOO MANY BASES	QUANTA	1163
1163	C	IF (NTOTS.GT.NUBASE) STOP "IN ZERO"	QUANTA	1164
1164	C	CHECK FOR TOO MANY SUBS	QUANTA	1165
1165		IF (NSUBS.GT.NOLTS) STOP "IN ZERO"	QUANTA	1166
1166		GO TO 1167	QUANTA	1167
1167		BASENU(1)=0.	QUANTA	1168
1168	10	CONTINUE	QUANTA	1169
1169	C		QUANTA	1170
1170		RETURN	QUANTA	1171
1171		END	QUANTA	1172

```

1172 SUBROUTINE SKVMAT(SKVLN,SKVPC,BRTIME,BRT,NRWAYS,ISEU,DELTA,
1173   * TOTLAT,TOTLNG,SUBLNG,SUBNG,MTYPE,MEL,KVS,RNGMIN,RNGMAX,MPHUF,
1174   * FAKG,FMIME,NMPS,DELTM,AREAL,DIAM,UTCENT,ISU,RA,UGTS,NMPS,
1175   * MANAP,NTYPES,MTYPES,NTGTS,NACT,MANWAT,NSUBS,MANPR,NSU,VAL,
1176   * DIMENSION SKVLN(NMPS,MANAP),SKVPC(NMPS,MANAP),BRTIME(NTYPES),
1177   * BRT(MANAP),NRWAYS(NTGTS),ISEU(NACT),DELTA(NRWAY,NTYPES,NTYPES),
1178   * TOTLAT(NTGTS),TOTLNG(NTGTS),SUBLAT(NSUBS),SUBLNG(NSUBS),
1179   * MTYPE(NSUBS),MEL(MTYPES),MVS(MTYPES),RNGMIN(MTYPES),RNGMAX
1180   * (MTYPES),MPHUF(MTYPES),MPKVG(MMPS,MTYPES),FMIME(MMPS,MTYPES),
1181   * NMPS(NSUBS),DELTM(MTYPES),AREAL(UGTS,MTYPES),
1182   * DIAM(UGTS,MTYPES),UTCENT(NTYPES),UGTS(UGTS),MAN(MANAP),
1183   * INSU(NTYPES),INSU(NTYPES),VAL(NTGTS,NMPS),
1184   * LEVEL,SKVLN,SKVPC,BRTIME,BRT,NRWAYS,ISEU,DELTA,TOTLAT,
1185   * TOTLNG,SUBLAT,SUBLNG,MTYPE,MEL,KVS,RNGMIN,RNGMAX,MPHUF,SKVNG,
1186   * FMIME,NMPS,DELTM,AREAL,DIAM,UTCENT,ISU,UGTS,VAL,MAN,
1187   * DATA P1/J,1=159205/
1188   CALL PAGE (U)
1189   LAST=0
1190   DO 140 I=1,NTGTS
1191     C
1192     C COMPUTE SURVIVABILITY OF EACH AIRCRAFT ON BASE FROM ALL WEAPONS
1193     C
1194     C
1195     IFST=LAST+1
1196     DO 10 JT=1,NTYPES
1197       LAST=LAST+INT(VAL(I,JT)*.1)
1198       NAC=LAST-IFST+1
1199       C COMPUTE THE BRAKE RELEASE TIMES(BRT) OF ALL AIRCRAFT
1200       C ON BASE I.
1201       NWY=NRWAYS(I)
1202       ITYPE=ISLQ(IFST)
1203       BRT(I)=BRTIME(ITYPE)
1204       C IF THERE IS ONLY ONE PLANE ON BASE, DUNT GO THRU LOOP
1205       IF (NAC.EQ.1) GO TO 30
1206       IAC=IFST
1207       DO 20 NI=2,NAC
1208         IAC=IAC+1
1209         ITP1=ITYPE
1210         ITP2=ISLQ(IAC)
1211         BRT(NI)=BRT(NI-1)+DELTA(NWY,ITYP1,ITYPE)
1212       CONTINUE
1213       C COMPUTE THE AVERAGE DISTANCE TO THE TURN POINT
1214       SUM=0.
1215       DO 35 IAC=IFST,LAST
1216         JT=ISLQ(IAC)
1217         SUM=SUM+UTCENT(JT)
1218       CONTINUE
1219       AVUTC=SUM/FLOAT(NAC)
1220     C
1221     C BEGIN THE OUTER LOOP FOR SUBMARINE LOCATIONS
1222

```

PAGE 38

```

1222 C
1223 ISALVU=U
1224 UU 120 KSUB=1+NSUBS
1225 DIST=U*IST(TOTLAT(1),TOTLNG(1),SUBLAT(KSUB),SUBLNG(KSUB))
1226 MISTYPE=MIST(KSUB)
1227 NMIS=NMPS(KSUB)
1228 CALL PAGE(122)
1229 WHITE(6,010) 1,KSUB,DIST,AVDTC
1230 C
1231 IF THE DISTANCE BETWEEN SUB KSUB AND BASE 1) IS OUT OF
1232 RANGE, MAKE THE SURVIVABILITY OF THE AIRCRAFT 1.
1233 IF (DIST-GE*MIN(MISTYPE),AND,DIST-LE*MAX(MISTYPE)) GO TO 50
1234 CALL SET(1,KSUB)
1235 LST=ISALVU*NMIS
1236 ISALVU=ISALVU*1
1237 UU 40 NI=1,MAC
1238 UU 40 K=ISALVU,LST
1239 SHVPC(K,NI)=.
1240 SHVLN(K,NI)=1.
1241 CONTINUE
1242 ISALVU=LST
1243 CONTINUE TO THE NEXT SUB LOCATION
1244 UU TO 130
1245 C
1246 C
1247 C
1248 C
1249 C
1250 C
1251 C
1252 C
1253 C
1254 C
1255 C
1256 C
1257 C
1258 C
1259 C
1260 C
1261 C
1262 C
1263 C
1264 C
1265 C
1266 C
1267 C
1268 C
1269 C
1270 C
1271 C

```

COMPUTE THE FIRST WEAPON'S TIME OF ARRIVAL (TOAR) IN MINUTES  
 MPROFAX=MPROF(MISTYPE)  
 TOAR = AOSC(DIST,FMRNG(1,MISTYPE),FMTIME(1,MISTYPE),MPROFAX)  
 START THE INNER LOOP FOR MISSILE SALVUS AT KSUB SUB LOC.  
 KVSMEV(MISTYPE)  
 HELMERE(MISTYPE)  
 UU 120 KSALE=1+NMIS  
 ISALVU=ISALVU\*1  
 TOA=TOAR+PLAT(KSALE-1)\*DELTIM(MISTYPE)  
 COMPUTE THE GROUND RANGE FROM OFAKE RELEASE, OF EACH  
 AIRCRAFT (KAR) AT THE TIME OF WEAPON ARRIVAL  
 NI=0  
 MFA=0.  
 UU 60 IAC=IPKST+LAST  
 NI=NI+1  
 JT=ISEU(IAC)  
 KTUA=TOA-BRT(JT)  
 KA = PROFLU(KTUA,S(1,JT),U(1,JT),NSU)  
 KAR(NI)=KA  
 MFA=MAAI(KA,KFA)  
 CONTINUE  
 RANGE OF THE FARTHEST AIRCRAFT IF RELATIVE TO THE TURN PT  
 MFA=MFA-AVDTC  
 IF (KSALE-1) GO TO 65  
 WHITE(6,020)TOA,ISALVU,(KAR(IAC),IAC=I+NI)

```

1272 CALL PADE (2*(NAC-1)/10)
1273 CONTINUE
1274
1275
1276
1277
1278
1279
1280
1281
1282
1283
1284
1285
1286
1287
1288
1289
1290
1291
1292
1293
1294
1295
1296
1297
1298
1299
1300
1301
1302
1303
1304
1305
1306
1307
1308
1309
1310
1311
1312
1313
1314
1315
1316
1317
1318
1319
1320
1321
1322

```

QUANTA 1273  
 QUANTA 1274  
 QUANTA 1275  
 QUANTA 1276  
 QUANTA 1277  
 QUANTA 1278  
 QUANTA 1279  
 QUANTA 1280  
 QUANTA 1281  
 QUANTA 1282  
 QUANTA 1283  
 QUANTA 1284  
 QUANTA 1285  
 QUANTA 1286  
 QUANTA 1287  
 QUANTA 1288  
 QUANTA 1289  
 QUANTA 1290  
 QUANTA 1291  
 QUANTA 1292  
 QUANTA 1293  
 QUANTA 1294  
 QUANTA 1295  
 QUANTA 1296  
 QUANTA 1297  
 QUANTA 1298  
 QUANTA 1299  
 QUANTA 1300  
 QUANTA 1301  
 QUANTA 1302  
 QUANTA 1303  
 QUANTA 1304  
 QUANTA 1305  
 QUANTA 1306  
 QUANTA 1307  
 QUANTA 1308  
 QUANTA 1309  
 QUANTA 1310  
 QUANTA 1311  
 QUANTA 1312  
 QUANTA 1313  
 QUANTA 1314  
 QUANTA 1315  
 QUANTA 1316  
 QUANTA 1317  
 QUANTA 1318  
 QUANTA 1319  
 QUANTA 1320  
 QUANTA 1321  
 QUANTA 1322

COMPUTE THE SURVIVABILITY FOR EACH AIRCRAFT ON BASE 1.  
 THE SURVIVABILITY MATRICES FOR A WEAPON PLACED:  
 CASE 1-- ON THE RUNWAY (SKVLN)-ALL MVS WILL BE EVENLY DISTRIBUTED  
 ON THE RUNWAY (FROM THE BRAKE RELEASE POINT TO THE TURN POINT).  
 CASE 2-- PAST THE CENTROID (SKVPC)-MVS WILL BE UNIFORMLY DISTRIBUTED  
 IN THE AREA OF THE CIRCLE SWEEPED OUT BY THE FARTHEST AIRCRAFT MINUS THE RUNWAY.

JTLN=-1  
 JTPC=-1  
 NI=0  
 DO 120 IAC=1,MST,LAST  
 NI=NI+1  
 JT=ISCU(IAC)  
 COMPUTE RADIUS OF A 180 TURN FOR THIS TYPE OF AC  
 TP=PROFLC(AVUTC,UI(JT),S(1,JT),NSU)+1.  
 JTP=PROFLC(TTP,S(1,JT),U(1,JT),NSU)-AVUTC  
 TPN=2.\*JTP/PI  
 IF (KAGINI).GT.AVUTC+TMN) GO TO 90  
 IF (JT.LE.JTLN) GO TO 110  
 JTLN=JT  
 THIS PLANE IS VULNERABLE TO A LINE ATTACK.  
 CONSIDER A "TOTAL" LETHAL DIAMETER FROM FWH. TO AVUTC  
 SUM=0.  
 AINT=AVUTC/MVSM  
 NINT=KASM  
 A=XINT+.5  
 TPE=-AVUTC  
 DO 80 IN=1,NINT  
 A=X\*INT  
 BM = AUSC(X,PTS,DIAM(1+JT,MISTYP),13)  
 TP = AUSC(X,PTS,DIAM(13+JT,MISTYP),13)  
 SUM=SUM+BM\*TP  
 SUM=SUM-AMAA1(0.,TPE+BM-XINT)  
 TPE=TP  
 CONTINUE  
 SUM=SUM-AMAA1(0.,X\*TP-AVUTC-TMN)  
 FOR CASE 1- THE SURV. DEPENDS ON THE RELIABILITY OF THE MISSILE.  
 THIS TOTAL LETHAL DIAMETER AND THE LENGTH OF THE "RUNWAY".  
 FOR CASE 2- SURV=1.  
 PR=SUM/(AVUTC+TMN)  
 PR=AMINI(1.,PR)  
 SKVLN((SALVUINI)=1.-PR\*OHELM  
 SHVPC((SALVUINI)=1.  
 CONTINUE TO THE NEXT AIRCRAFT  
 GO TO 120

PAGE 40

```

1322 C
1323 C
1324 C
1325 C
1326 C
1327 C
1328 C
1329 C
1330 C
1331 C
1332 C
1333 C
1334 C
1335 C
1336 C
1337 C
1338 C
1339 C
1340 C
1341 C
1342 C
1343 C
1344 C
1345 C
1346 C
1347 C
1348 C
1349 C
1350 C
1351 C
1352 C
1353 C
1354 C
1355 C
1356 C
1357 C
1358 C
1359 C
1360 C
1361 C
1362 C
1363 C
1364 C
1365 C
1366 C
1367 C
1368 C
1369 C
1370 C
1371 C
1372 C

IF (JT*EU*JTPC) GO TO 110
JTPC=JT
THIS PLANE IS VULNERABLE TO A DAMAGE ATTACK.
SINCE THE LETHAL AREAS DIMINISH AS THEY MOVE OUT FROM THE
CENTROID, A WEIGHTED AVERAGE AREA WILL BE USED.
IN=2
SUM=0.0
DELTA=AREAAL(IN-1,JT,MISTYP)-AREAAL(IN,JT,MISTYP)
SUM=SUM+DELTA*(UPTS(IN)*UPTS(IN-1))**2)
IN=IN+1
IF (IN.LE.30 .AND. UPTS(IN).LT.RFA) GO TO 100
RHU=(RFA*UPTS(IN-1))**2
T1=AREAAL(IN-1,JT,MISTYP)*RHU
AK=AOSC(RFA*UPTS(IN-1)*RHU)
T2=AREAAL(4.0*(RFA**2)-RHU)
SUM=(SUM+T1+T2)/(4.0*RFA**2)
RHU=SUM*(SUM/PI)
BP=(RFA*TRN)*0.5
UTC=AVUTC
WAREA=CIRINT(RFA*RHU*BP) - CIRINT(TRN*RHU*BP)
IF (RFA.LE.UTC) TA=(RFA**2)*PI-ASIN(TRN/RFA) - PI*(TRN**2)/2.
* - TRN*(SQRT(RFA**2-TRN**2))
IF (RFA.GT.UTC .AND. RFA.LT.UTC*TRN) TA=RFA**2*PI - 2.0*TRN*UTC
* - CIRINT(RFA*TRN*UTC)
IF (RFA.GE.UTC*TRN) TA=PI*(RFA**2-TRN**2) - 2.0*TRN*UTC
FOR CASE 1- SURV=1
FOR CASE 2- THE SURV. DEPENDS ON THE RELIABILITY OF THE MISSILE,
THE WEIGHTED AREA, AND THE AREA THAT THE PLANE IS IN.
SKVLN(ISALVU,N1)=1.
PK=WAREA*WVSM/TA
PK=AMIN(1.0,PK)
SKVPC(ISALVU,N1)=1.0 - PK*WELM
SKVPC(ISALVU,N1)=SKVPC(ISALVU,N1-1)
GO TO 120

PLANES OF THE SAME TYPE, HAVING THE SAME POSITION (FALL UNDER
THE SAME ATTACK POSITIONS) HAVE THE SAME SURVIVAL.
CONTINUE
SKVLN(ISALVU,N1)=SKVLN(ISALVU,N1-1)
SKVPC(ISALVU,N1)=SKVPC(ISALVU,N1-1)
CONTINUE
IN=2*(I-1)
CALL WHITMS(4,SKVLN(I,1),N*PNS*MXNAPB,IN*1)
CALL WHITMS(4,SKVPC(I,1),N*PNS*MXNAPB,IN*2)
CONTINUE
REFURN
FORMAT (/0 THE DISTANCE TO TARGET *13.0 FROM SUB *12.0 IS 0.
* F10.4,DA,0 THE AVERAGE DISTANCE TO THE TURN POINT IS *7.2.0 NM*)

```

2024

1372  
1373  
1374  
1375

020 FURMAT (O AFTER 0910.00 MINUTES, WHEN ALAPUN O, 14, O ARRIVES, THE  
O MANGES(NH) OF AIRCRAFT ARE O/2K, 10F10.4))  
END

QUANTA  
QUANTA  
QUANTA



```

1375 FUNCTION CIRCLEINTERSECT
1376 DATA PI/3.141592654
1377 CIRCLEINT COMPUTES THE INTERSECTION OF TWO CIRCLES WITH RADIUS
1378 MI AND MC. U IS THE DISTANCE BETWEEN THEM.
1379 IF (MI+MC<U) MC=U-MI GO TO 1
1380 IF (MI-MC>U) U TO 1
1381 IF (MI+MC<U) U TO 2
1382 IF (MI-MC>U) U TO 2
1383 IF (MC<U-MI) U TO 3
1384 IF A IS THE DISTANCE BETWEEN THE CENTER OF THE CIRCLE AND THE
1385 CORD LINE CORD IS THE LINE SEGMENT THAT CONNECTS THE
1386 POINTS OF INTERSECTION OF THE TWO CIRCLES. THEN THE TA
1387 HALF THE ANGLE THAT SWEEPS OUT THE SECTOR. IS THE
1388  $APCOS(X/R)$  WHERE R IS THE RADIUS.
1389 THEREFORE THE INTERSECTION IS THE SUM OF THE TWO SECTORS
1390  $(R^2 * THETA) - (MC^2 * U * U) / (2 * MI)$ 
1391  $COST1 = 0.5 * (MI^2 - MC^2 * U * U) / (2 * MI)$ 
1392  $THETA1 = ACOS(COST1)$ 
1393  $COST2 = 0.5 * (MC^2 - MI^2 * U * U) / (2 * MC)$ 
1394  $THETA2 = ACOS(COST2)$ 
1395  $CIRCLEINT = MI^2 * THETA1 + MC^2 * THETA2 - U * MI * SIN(THETA1)$ 
1396 RETURN
1397 TWO CIRCLES DO NOT INTERSECT
1398 CIRCLEINT=0.
1399 RETURN
1400 MC CIRCLE ENCOMPASSES MI CIRCLE
1401 CIRCLEINT=PI*MI^2
1402 RETURN
1403 MI CIRCLE ENCOMPASSES MC CIRCLE
1404 CIRCLEINT=PI*MC^2
1405 RETURN
1406 END

```

1376 QUANTA  
 1377 QUANTA  
 1378 QUANTA  
 1379 QUANTA  
 1380 QUANTA  
 1381 QUANTA  
 1382 QUANTA  
 1383 QUANTA  
 1384 QUANTA  
 1385 QUANTA  
 1386 QUANTA  
 1387 QUANTA  
 1388 QUANTA  
 1389 QUANTA  
 1390 QUANTA  
 1391 QUANTA  
 1392 QUANTA  
 1393 QUANTA  
 1394 QUANTA  
 1395 QUANTA  
 1396 QUANTA  
 1397 QUANTA  
 1398 QUANTA  
 1399 QUANTA  
 1400 QUANTA  
 1401 QUANTA  
 1402 QUANTA  
 1403 QUANTA  
 1404 QUANTA  
 1405 QUANTA  
 1406 QUANTA

PL02 43

1406	C	SUBROUTINE SET (I,KSUB)	QUANTA	1407
1407	C		QUANTA	1408
1408	C	SETS BIT TO SIGNIFY PARTICULAR SUB IS OUT OF RANGE OF A PARTICULAR	QUANTA	1409
1409	C	BASE.	QUANTA	1410
1410	C	EACH WORD OF BASENO REPRESENTS A BASE	QUANTA	1411
1411	C	EACH BIT OF BASENO(I) REPRESENTS A SUBS RANGE FROM 1-TH BASE	QUANTA	1412
1412	C	EACH BIT (I. E. SUB) IS COUNTED FROM THE LEFT OF WORD BASENO(I)	QUANTA	1413
1413	C		QUANTA	1414
1414	C	COMMON/MINOFLO/BASENO(47),NOBITS	QUANTA	1415
1415	C		QUANTA	1416
1416	C	TEMP=SHIFT(BASENO(I),KSUB).OR.1B	QUANTA	1417
1417	C	BASENO(I)=SHIFT(TEMP,NBITS-KSUB)	QUANTA	1418
1418	C		QUANTA	1419
1419	C	RETURN	QUANTA	1420
1420	C	END	QUANTA	1421

PAGE 44

```

1421 SUBROUTINE MARKV(NMARKV,CUT,IMARKV)
1422 DIMENSION CUT(NMARKV)
1423 LEVEL = 0
1424 DATA WHERE/5,NMARKV/
1425 IMARKV=0
1426 IF (NMARKV.LE.0) RETURN
1427 DO 10 I=1,NMARKV
1428 READ(5,5000) (CUT(I),I=1,NMARKV)
1429 IF (CUT(I).LT.0.0) CALL ABORT(WHERE,I,"CUT CANNOT BE LESS THAN 0")
1430 CONTINUE
1431 IMARKV=I
1432 WRITE (6,6000) NMARKV,NMARKV,(CUT(I),I=1,NMARKV)
1433 CALL PAGE(3)
1434 RETURN
1435 5000 FORMAT(7F10.5)
1436 6000 FORMAT(//14H THERE WILL BE 16.30H MARKVAL RUN(S) FOR THIS CASE./,
1437 *24H THE CUT-OFF VALUES ARE,=(2X,F10.5))
1438 END
1439
1422 QUANTA
1423 QUANTA
1424 QUANTA
1425 QUANTA
1426 QUANTA
1427 QUANTA
1428 QUANTA
1429 QUANTA
1430 QUANTA
1431 QUANTA
1432 QUANTA
1433 QUANTA
1434 QUANTA
1435 QUANTA
1436 QUANTA
1437 QUANTA
1438 QUANTA
1439 QUANTA

```

```

1439 SUBROUTINE ALLOC(NTUTS,NSUBS,MNPN,ALUC,ALUCU,ISUBS,MNPN)
1440 * ITGTO)
1441 QUANTA 1440
1442 QUANTA 1441
1443 QUANTA 1442
1444 QUANTA 1443
1445 QUANTA 1444
1446 QUANTA 1445
1447 QUANTA 1446
1448 QUANTA 1447
1449 QUANTA 1448
1450 QUANTA 1449
1451 QUANTA 1450
1452 QUANTA 1451
1453 QUANTA 1452
1454 QUANTA 1453
1455 QUANTA 1454
1456 QUANTA 1455
1457 QUANTA 1456
1458 QUANTA 1457
1459 QUANTA 1458
1460 QUANTA 1459
1461 QUANTA 1460
1462 QUANTA 1461
1463 QUANTA 1462
1464 QUANTA 1463
1465 QUANTA 1464
1466 QUANTA 1465
1467 QUANTA 1466
1468 QUANTA 1467
1469 QUANTA 1468
1470 QUANTA 1469
1471 QUANTA 1470
1472 QUANTA 1471
1473 QUANTA 1472
1474 QUANTA 1473
1475 QUANTA 1474
1476 QUANTA 1475
1477 QUANTA 1476
1478 QUANTA 1477
1479 QUANTA 1478
1480 QUANTA 1479
1481 QUANTA 1480
1482 QUANTA 1481
1483 QUANTA 1482
1484 QUANTA 1483
1485 QUANTA 1484

```

SUBROUTINE ALLOC(NTUTS,NSUBS,MNPN,ALUC,ALUCU,ISUBS,MNPN)  
 \* ITGTO)  
 DIMENSION ALLOC(NTUTS,MNPN),ALUC(MNPN),ISUBS(MNPN)  
 \* (MNPNS,NSUBS),ITGTO(MNPN)  
 COMMON /REAL/ ITGTO,EPSCUT,ITCUT,ICMGAU  
 LEVEL,ALUCU,NSUBS,MNPN,ITGTO,ALUCU  
 DATA WHERE/MNPN/  
 REAL(545000)CMGAL,ITCUT,ITCUT2,EPSCUT  
 IF (CMGAL.LE.0.0) CALL ABORT(WHERE,1,"WHAT IS CONSIDERED TO BE A  
 INCREASE IN MLL MUST BE GREATER THAN 0")  
 IF (EPSCUT.LE.0.0) CALL ABORT(WHERE,2,"THE CONVERGENCE TEST FOR THE  
 LAGRANGIAN MATRIX MUST BE GREATER THAN 0")  
 IF (ITCUT1.LE.0.0) CALL ABORT(WHERE,3,"THE MAXIMUM NUMBER OF ITCUT  
 ITERATIONS MUST BE GREATER THAN 0")  
 IF (ITCUT2.LE.0.0) CALL ABORT(WHERE,4,"THE NUMBER OF ITERATIONS NEW  
 IUTED TO CHECK FOR INCREASE MUST BE GREATER THAN 0")  
 DO 20 J=1,MNPN  
 ALUCU(J)=0.0  
 DO 20 I=1,NTUTS  
 DO 20 K=1,3  
 ALUC(I,J,K)=0.  
 20 CONTINUE  
 READ INPUT INITIAL ALLOCATION.  
 MNPNE  
 DO 50 J=1,NSUBS  
 JLM=ISUBS(J)  
 ILM=MNPNS(J)  
 DO 50 JSUB=1,ILM  
 READ(5,50)ITGTO(I),I=1,ILM  
 DO 40 I=1,ILM  
 MNPNE=MNPNE+1  
 I=ITGTO(I)  
 IF (I.LT.1.0) CALL ABORT(WHERE,5,"THE TARGET NUM  
 BER RECEIVING THIS REASON MUST BE BETWEEN -1 AND NTUTS")  
 IF (I.EQ.0) GO TO 40  
 IF (I.LT.-1) ALUC(MNPNE)=ALUC(MNPNE)+1.  
 IF (I.LT.-1) ALUC(I,MNPNE,3)=ALUC(I,MNPNE,3)+1.  
 40 CONTINUE  
 IF (JSUB.EQ.1,ILM) MNPNE=MNPNE+ILM  
 50 CONTINUE  
 RETURN  
 5000 FORMAT(10,4,2D,10.4)  
 5010 FORMAT(14,5)  
 END

```

1404 SUBROUTINE TOTAL (INTS, NMPS, NTYPES, ALUC, SHVLN, VAL, RELVAL, FLAMB,
1405 * PROD, VILL, MANAP, NACT, ISE, SKVPC, BONUS, BASVAL, MTYPE, MEL,
1406 * NMPS, NSUBS, MTYPES, SUB)
1407 DIMENSION ALUC (INTS, NMPS, SUB), SHVLN (NMPS, MANAP, RELVAL (INTYPES)),
1408 * SKVPC (NMPS, MANAP), VAL (INTS, NTYPES), FLAMB (INTS, NMPS, SUB),
1409 * PROD (NACT), VILL (INTS), ISE (NACT), BONUS (INTS), BASVAL (INTS),
1410 * MTYPE (NSUBS), REL (MTYPES), NMPS (NSUBS), PS (MTYPES),
1411 * LEVEL, ALUC, SKVPC, SHVLN, VAL, RELVAL, FLAMB, PROD, VILL, ISE,
1412 * BONUS, BASVAL, MTYPE, REL, NMPS, PS
1413 C
1414 C TOTAL CALCULATES THE APRAIS WHICH DEFINE THE OBJECTIVE
1415 C FUNCTION (PROD, BONUS, VILL) AND THE LAZARUSIAN MULTIPLIER
1416 C MATRIX (FLAMB)
1417 C
1418 C
1419 C
1420 C
1421 C
1422 C
1423 C
1424 C
1425 C
1426 C
1427 C
1428 C
1429 C
1430 C
1431 C
1432 C
1433 C
1434 C
1435 C
1436 C
1437 C
1438 C
1439 C
1440 C
1441 C
1442 C
1443 C
1444 C
1445 C
1446 C
1447 C
1448 C
1449 C
1450 C
1451 C
1452 C
1453 C
1454 C
1455 C
1456 C
1457 C
1458 C
1459 C
1460 C
1461 C
1462 C
1463 C
1464 C
1465 C
1466 C
1467 C
1468 C
1469 C
1470 C
1471 C
1472 C
1473 C
1474 C
1475 C
1476 C
1477 C
1478 C
1479 C
1480 C
1481 C
1482 C
1483 C
1484 C
1485 C
1486 C
1487 C
1488 C
1489 C
1490 C
1491 C
1492 C
1493 C
1494 C
1495 C
1496 C
1497 C
1498 C
1499 C
1500 C
1501 C
1502 C
1503 C
1504 C
1505 C
1506 C
1507 C
1508 C
1509 C
1510 C
1511 C
1512 C
1513 C
1514 C
1515 C
1516 C
1517 C
1518 C
1519 C
1520 C
1521 C
1522 C
1523 C
1524 C
1525 C
1526 C
1527 C
1528 C
1529 C
1530 C
1531 C
1532 C
1533 C
1534 C

```

PAGE 47

```

1534 VAL1(I)=VAL(I)+BASVAL(I)*(-BONUS(I))
1535      COMPUTE THE MULTIPLIER MATRIA (FLAMB)
1536      UU 70 J=1,NMIPS
1537      SUMC=0.
1538      SUML=0.
1539      ISUMV=0
1540      UU 60 IAC=NAL,NAL
1541      ISUMV=ISUMV+1
1542      JI=ISEL(IAC)
1543      FLAMB(I)=PMUL(IAC)*ALOG(SHVP(I)*ISUMV))*RELVAL(JI)
1544      SUMC=SUMC+FLAMB(I)
1545      FLAMB(I)=PMUL(IAC)*ALOG(SHVL(I)*ISUMV))*RELVAL(JI)
1546      SUML=SUML+FLAMB(I)
1547      CONTINUE
1548      UU 80 MI=1,MIPES
1549      FLAMB(I,J)=SUMC
1550      FLAMB(I,J)=SUML
1551      JFINE THE ARRAY PSB (LN OF THE SURVIV. OF THE BASE)
1552      UU 80 MI=1,MIPES
1553      PSB(MI)=ALOG(1.-REL(MI))
1554      CONTINUE
1555      COMPUTE ADDITIONAL LAMBUA FOR BASE ATTACK
1556      J=0
1557      UU 90 ISUB=1,NSUBS
1558      MI=MI*PSB(ISUB)
1559      NMIS=NIPS(ISUB)
1560      UU 90 K=1,NMIS
1561      J=J+1
1562      FLAMB(I,J)=-(BASVAL(I)*BONUS(I)*PSB(MI))
1563      CONTINUE TO NEXT BASE
1564      RETURN
1565      END

```

1535  
 1536  
 1537  
 1538  
 1539  
 1540  
 1541  
 1542  
 1543  
 1544  
 1545  
 1546  
 1547  
 1548  
 1549  
 1550  
 1551  
 1552  
 1553  
 1554  
 1555  
 1556  
 1557  
 1558  
 1559  
 1560  
 1561  
 1562  
 1563  
 1564  
 1565  
 1566









```

1707 CALL SEARCH(PLAMM,MIJCOL,TYPE,SPR,MI,MAX,MAN,VCUT,IR,MAX)
1708 * ALLOC(MAN)
1709 * IF (MAX=0) GO TO 30
1710 * IF (PLAMM=0) GO TO 30
1711 * IF (SPR=0) GO TO 30
1712 * IF (MI=0) GO TO 30
1713 * IF (TYPE=0) GO TO 30
1714 * IF (MAX=0) GO TO 30
1715 * IF (PLAMM=0) GO TO 30
1716 * IF (SPR=0) GO TO 30
1717 * IF (MI=0) GO TO 30
1718 * IF (TYPE=0) GO TO 30
1719 * IF (MAX=0) GO TO 30
1720 * IF (PLAMM=0) GO TO 30
1721 * IF (SPR=0) GO TO 30
1722 * IF (MI=0) GO TO 30
1723 * IF (TYPE=0) GO TO 30
1724 * IF (MAX=0) GO TO 30
1725 * IF (PLAMM=0) GO TO 30
1726 * IF (SPR=0) GO TO 30
1727 * IF (MI=0) GO TO 30
1728 * IF (TYPE=0) GO TO 30
1729 * IF (MAX=0) GO TO 30
1730 * IF (PLAMM=0) GO TO 30
1731 * IF (SPR=0) GO TO 30
1732 * IF (MI=0) GO TO 30
1733 * IF (TYPE=0) GO TO 30
1734 * IF (MAX=0) GO TO 30
1735 * IF (PLAMM=0) GO TO 30
1736 * IF (SPR=0) GO TO 30
1737 * IF (MI=0) GO TO 30
1738 * IF (TYPE=0) GO TO 30
1739 * IF (MAX=0) GO TO 30
1740 * IF (PLAMM=0) GO TO 30
1741 * IF (SPR=0) GO TO 30
1742 * IF (MI=0) GO TO 30
1743 * IF (TYPE=0) GO TO 30
1744 * IF (MAX=0) GO TO 30
1745 * IF (PLAMM=0) GO TO 30
1746 * IF (SPR=0) GO TO 30
1747 * IF (MI=0) GO TO 30
1748 * IF (TYPE=0) GO TO 30
1749 * IF (MAX=0) GO TO 30
1750 * IF (PLAMM=0) GO TO 30
1751 * IF (SPR=0) GO TO 30
1752 * IF (MI=0) GO TO 30
1753 * IF (TYPE=0) GO TO 30
1754 * IF (MAX=0) GO TO 30
1755 * IF (PLAMM=0) GO TO 30
1756 * IF (SPR=0) GO TO 30
1757 * IF (MI=0) GO TO 30

```



PAGE 53

```

1807 PLAMTLCUM*MAXITER=DEL
1808 CONTINUE
1809
1810 GO TO 120
1811
1812 SUM IS THE SUM OF LAMCET
1813
1814 ALLOCUTEL=ALOCUTEL+DELTA
1815 UNDSUM=UNDSUM+DELTA*DELTA
1816 IF THE USER HAS REQUESTED (AOCITEL*2) INFORMATION
1817 WILL BE PRINTED EACH TIME A WEAPON IS MOVED
1818
1819 CALL PAGE(1) GO TO 130
1820
1821 CALL PAGE(1) IFX
1822
1823 AMITE(10,100) IFX
1824
1825 AMITE(10,100) UNDSUM
1826
1827 UNDSUM=UNDSUM+UNDSUM
1828
1829 UNDSUM=UNDSUM
1830
1831 CALL PAGE(1) MAXITER=DEL
1832
1833 CALL PAGE(1) MAXITER=DEL
1834
1835 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1836
1837 CALL PAGE(1) MAXITER=DEL
1838
1839 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1840
1841 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1842
1843 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1844
1845 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1846
1847 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1848
1849 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1850
1851 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1852
1853 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1854
1855 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1856
1857 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1858
1859 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1860
1861 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1862
1863 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1864
1865 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1866
1867 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1868
1869 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1870
1871 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1872
1873 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1874
1875 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1876
1877 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1878
1879 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1880
1881 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1882
1883 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1884
1885 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1886
1887 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1888
1889 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1890
1891 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1892
1893 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1894
1895 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1896
1897 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1898
1899 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1900
1901 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1902
1903 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1904
1905 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1906
1907 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1908
1909 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1910
1911 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1912
1913 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1914
1915 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1916
1917 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1918
1919 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1920
1921 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1922
1923 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1924
1925 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1926
1927 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1928
1929 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1930
1931 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1932
1933 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1934
1935 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1936
1937 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1938
1939 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1940
1941 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1942
1943 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1944
1945 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1946
1947 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1948
1949 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1950
1951 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1952
1953 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1954
1955 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1956
1957 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1958
1959 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1960
1961 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1962
1963 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1964
1965 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1966
1967 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1968
1969 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1970
1971 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1972
1973 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1974
1975 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1976
1977 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1978
1979 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1980
1981 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1982
1983 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1984
1985 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1986
1987 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1988
1989 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1990
1991 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1992
1993 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1994
1995 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1996
1997 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
1998
1999 IF (AOCITEL*2) UNDSUM=UNDSUM+ALOCUTEL*ALOCUTEL
2000

```

100 100

101 102 103

104 105 106

107 108 109

110 111 112

113 114 115

116 117 118

119 120 121

122 123 124

125 126 127

128 129 130

131 132 133

134 135 136

137 138 139

140 141 142

143 144 145

146 147 148

149 150 151

152 153 154

155 156 157

158 159 160

161 162 163

164 165 166

167 168 169

170 171 172

1955	1956	1957	1958	1959	1960	1961	1962	1963	1964	1965
1966	1967	1968	1969	1970	1971	1972	1973	1974	1975	1976

IDENT SUBVOL  
ILLU. WRITTEN MESSAGE TO OPERATIONS SUBVOL UNIT.  
COMMENT WRITTEN MESSAGE TO OPERATIONS SUBVOL UNIT.  
EXTN SUBVOL  
EG \*1517  
MESSAGE AT01  
EG SUBVOL  
END  
END

PAGE 56

1875	IDENT	PPALTEX	1876
1876			1877
1877		COMMENT PERMANENT FILE ALTER/EXTEND ROUTINE. 18 MAY 1977.	1878
1878		TITLE PERMANENT FILE ALTER/EXTEND ROUTINE. 18 MAY 1977.	1879
1879			1880
1880		ENABLES ALTER/EXTEND CONTROL OF THE FOLLOWING PERMANENT FILE -	1881
1881		(TAPL13,QUEST,INT,IDE=DMYAJJ0)	1882
1882		N O T E -- THIS ROUTINE REQUIRES //PPMTEAT//.	1883
1883			1884
1884		ENTRY ALTER,EXTEND	1885
1885			1886
1886		SUBROUTINE ALTER	1887
1887	ALTER	ENTRY/EXIT POINT.	1888
1888			1889
1889		RETURN.	1890
1890			1891
1891		SUBROUTINE EXTEND	1892
1892	EXTEND	ENTRY/EXIT POINT.	1893
1893			1894
1894		RETURN.	1895
1895			1896
1896	ALTER	F00 TAPL13,QUEST,INT,IDE=DMYAJJ0	1897
1897			1898
1898			1899

```

1999 SUBROUTINE MSTART (ISTART,IMAPV,UBJSUM,ALUC,FLAMB,PMOU,VKILL,ALUCU
1900 *INTOTS,MAPV,NAUFI)
1901 COMMON/KLC/EPSS,J,ISALV,MSUB,ISSWZ,UBHULU
1902 DIMENSION ALUC(INTOTS,PMPS,3), FLAMB(INTOTS,PMPS,3), PMOU(NAUFI),
1903 *VKILL(INTOTS), ALUC(PMPS)
1904 INTEGER IUDAT,NUM
1905 LEVEL=2, ALUC,FLAMB,PMOU,VKILL,ALUCU
1906
1907 REMIND 13
1908 IF (ISTART.EQ.2) GO TO 1
1909 READ MSTART TAPE 13
1910 READ (13) IUDAT,NUM
1911 IF (IUDAT(13).NE.0) GO TO 2
1912 READ(13) IMAPV,EPSS,J,ISALV,MSUB,UBHULU,UBJSUM
1913 READ (13) ((ALUC(K,L,M),K=1,INTOTS),L=1,PMPS),M=1,3)
1914 READ (13) ((FLAMB(K,L,M),K=1,INTOTS),L=1,PMPS),M=1,3)
1915 READ (13) (PMOU(K),K=1,NAUFI)
1916 READ (13) (VKILL(K),K=1,INTOTS)
1917 READ (13) (ALUC(K),K=1,PMPS)
1918 WRITE (5,3) IUDAT,NUM
1919 GO TO 2
1920
1921 WRITE MSTART TAPE 13
1922
1923 1 CONTINUE
1924 IF (ISSWZ.EQ.1) CALL ALTER
1925 CALL DATE (IUDAT)
1926 CALL TIME (NUM)
1927 WRITE (13) IUDAT,NUM
1928 WRITE (13) IMAPV,EPSS,J,ISALV,MSUB,UBHULU,UBJSUM
1929 WRITE (13) ((ALUC(K,L,M),K=1,INTOTS),L=1,PMPS),M=1,3)
1930 WRITE (13) ((FLAMB(K,L,M),K=1,INTOTS),L=1,PMPS),M=1,3)
1931 WRITE (13) (PMOU(K),K=1,NAUFI)
1932 WRITE (13) (VKILL(K),K=1,INTOTS)
1933 WRITE (13) (ALUC(K),K=1,PMPS)
1934 WRITE (13) IUDAT,NUM
1935
1936 END FILE 13
1937 REMIND 13
1938 IF (ISSWZ.EQ.1) CALL EXTEND
1939
1940 2 RETURN
1941
1942 3 FORMAT (3A,20H000 MSTART TAPE MEAN. 000,5X,2A10)
1943 4 FORMAT (3X,20H000 MSTART TAPE M'ITEN. 000,5X,2A10)
1944
1945 END

```



PAGE 58

1943	SUBROUTINE TERM (10011+ISSW1)	UOANIA	1944
1944	IF (10011.EQ.1) WRITE (6,1)	UOANIA	1945
1945	IF (ISSW1.EQ.1) WRITE (6,2)	UOANIA	1946
1946	IF (10011.EQ.1) CALL REMARK (330000 UOANIA TERMINATED BY TIME 000)	UOANIA	1947
1947	IF (ISSW1.EQ.1) CALL REMARK (330000 UOANIA TERMINATED BY SSW1 000)	UOANIA	1948
1948	STOP	UOANIA	1949
1949		UOANIA	1950
1950	1 FORMAT (20X,330000 UOANIA TERMINATED BY TIME 000)	UOANIA	1951
1951	2 FORMAT (20X,330000 UOANIA TERMINATED BY SSW1 000)	UOANIA	1952
1952	END	UOANIA	1953



PLAGE 00

```

1994 SUBROUTINE SEARCH(FLAMB,ALUC,IT,IS,INPINS,MMI,MMAX,MMIN,MMAX,CUT)
1995 * (MMAX,ALUC,MSUB)
1996 * DIMENSION FLAMB(IT,IS,INPINS),ALUC(IT,IS,INPINS),CUT(MMAX)
1997 * ALUC(MMINS)
1998 LEVEL=FLAMB*ALUC,CUT,ALUC
1999 COMMON/IFF/LUM,MAX,MMAX,LUMPL
2000 LOGICAL OUTING
2001 C SEARCH FOR MIN AND MAX LAMBDA FROM WEAPON GROUP J
2002 C MAX DEFINES THE BASE WITH THE LARGEST VALUE WHILE LUM
2003 C DEFINES THE BASE WITH THE SMALLEST VALUE
2004 C MMAX AND LUMPL ARE THE ATTACK POINTS ON BASE MAX AND LUM
2005 C RESPECTIVELY
2006 MMAX=-1
2007 MMIN=999
2008 MMAX=1
2009 LUM=1
2010 DO 20 IF=1,3
2011 DO 20 I=1,NTGT
2012 TEST=FLAMB(I,J)*I
2013 IF (CUT(MMINS).GT.TEST,LE,MMAX) GO TO 10
2014 MMAX=TEST
2015 MMAX=1
2016 MMAX=1
2017 IF THE NO. OF WEAPONS ON BASE IS NOT LARGE ENOUGH
2018 C CONTINUE TO THE NEXT BASE
2019 IF (ALUC(I,J).LT.0.001,MMAX,MMIN) GO TO 20
2020 MMIN=TEST
2021 LUM=1
2022 LUMPL=1
2023 C CONTINUE
2024 IF (MMAX,LE,0) GO TO 40
2025 C SINCE THIS IS A MAXVAL RUN, CHECK OUT THE DUMMY BASE
2026 CUTOFF=CUT(MMAX)
2027 IF (CUTOFF,LE,MMAX) GO TO 30
2028 MMAX=CUTOFF
2029 MMAX=-1
2030 IF (ALUC(I,J).LT.0.001,MMAX,CUTOFF,MMIN) GO TO 40
2031 MMIN=CUTOFF
2032 LUM=-1
2033 C CONTINUE
2034 C RETURN
2035 C
2036 END

```

1995 GUANTIA  
 1996 GUANTIA  
 1997 GUANTIA  
 1998 GUANTIA  
 1999 GUANTIA  
 2000 GUANTIA  
 2001 GUANTIA  
 2002 GUANTIA  
 2003 GUANTIA  
 2004 GUANTIA  
 2005 GUANTIA  
 2006 GUANTIA  
 2007 GUANTIA  
 2008 GUANTIA  
 2009 GUANTIA  
 2010 GUANTIA  
 2011 GUANTIA  
 2012 GUANTIA  
 2013 GUANTIA  
 2014 GUANTIA  
 2015 GUANTIA  
 2016 GUANTIA  
 2017 GUANTIA  
 2018 GUANTIA  
 2019 GUANTIA  
 2020 GUANTIA  
 2021 GUANTIA  
 2022 GUANTIA  
 2023 GUANTIA  
 2024 GUANTIA  
 2025 GUANTIA  
 2026 GUANTIA  
 2027 GUANTIA  
 2028 GUANTIA  
 2029 GUANTIA  
 2030 GUANTIA  
 2031 GUANTIA  
 2032 GUANTIA  
 2033 GUANTIA  
 2034 GUANTIA  
 2035 GUANTIA  
 2036 GUANTIA  
 2037 GUANTIA

PAGE 61

037 0  
038 0  
039 0  
040 0  
041 0  
042 0  
043 0  
044 0  
045 0  
046 0  
047 0  
048 0

LOGICAL FUNCTION OUTRNG(I,KSUB)  
TESTS SUB (I.E. BIT) TO SEE IF IT IS OUT OF RANGE.  
COMMON/NGFLUX/DASENU(47),NSITS  
TEMP=SHIFT(DASENU(I),KSUB).AND.15  
OUTNG=.FALSE.  
IF (TEMP.NE.6) OUTNG=.TRUE.  
RETURN  
END

049 0  
050 0  
051 0  
052 0  
053 0  
054 0  
055 0  
056 0  
057 0  
058 0  
059 0

[illegible]



[illegible]

[illegible]



```

210 SUBROUTINE ADJLAM(NAL,NAL,NWPN,INTYPE,MANAPB,ISURV,PHOU,NACT,
211 * SURV,RELVAL,FLAMB,NTGTS,IFLAG,IBASE)
212 * DIMENSION ISEU(NACT),PHOU(NACT),SURV(NWPN,MANAPB),RELVAL(INTYPE),
213 * FLAMB(NTGTS,NWPN,3)
214 LEVEL=ISEU,PHOU,SURV,RELVAL,FLAMB
215 ADJLAM RECALCULATES THE MULTIPLIER MATRIX ACCORDING TO THE
216 CHANGE IN THE PRODUCT MATRIX (WHICH RESULTED FROM THE CHANGE
217 IN ALLOCATION)
218 DO 20 J=1,NWPN
219 SUM=0.
220 ISK=0
221 DO 10 I=NAL,NAL
222 ISK=ISK+1
223 JT=ISEU(I)
224 X=-PHOU(I)*ALOG(SURV(J,ISK))*RELVAL(JT)
225 SUM=SUM+X
226 CONTINUE
227 FLAMB(IBASE,J,IFLAG)=SUM
228 CONTINUE
229 * HEAD IN THE SURVIVABILITY OF THE AIRCRAFT AGAINST WEAPONS
230 * PLACED AT THE OTHER POINT ON BASE.
231 IF (IFLAG.EQ.2) GO TO 30
232 IN=2*(IBASE-1)+1
233 CALL HEADMS(4,SURV(1,1),NWPN,MANAPB,IN)
234 I1=2
235 GO TO 50
236
237 IN=2*(IBASE-1)+2
238 CALL HEADMS(4,SURV(1,1),NWPN,MANAPB,IN)
239 I1=3
240 * CALCULATE THE REMAINDER OF THE MULTIPLIER MATRIX
241 DO 70 J=1,NWPN
242 SUM=0.
243 ISK=0
244 DO 60 I=NAL,NAL
245 ISK=ISK+1
246 JT=ISEU(I)
247 X=-PHOU(I)*ALOG(SURV(J,ISK))*RELVAL(JT)
248 SUM=SUM+X
249 CONTINUE
250 FLAMB(IBASE,J,I1)=SUM
251 CONTINUE
252 RETURN
253 END

```

2211 QUANTA  
 2212 QUANTA  
 2213 QUANTA  
 2214 QUANTA  
 2215 QUANTA  
 2216 QUANTA  
 2217 QUANTA  
 2218 QUANTA  
 2219 QUANTA  
 2220 QUANTA  
 2221 QUANTA  
 2222 QUANTA  
 2223 QUANTA  
 2224 QUANTA  
 2225 QUANTA  
 2226 QUANTA  
 2227 QUANTA  
 2228 QUANTA  
 2229 QUANTA  
 2230 QUANTA  
 2231 QUANTA  
 2232 QUANTA  
 2233 QUANTA  
 2234 QUANTA  
 2235 QUANTA  
 2236 QUANTA  
 2237 QUANTA  
 2238 QUANTA  
 2239 QUANTA  
 2240 QUANTA  
 2241 QUANTA  
 2242 QUANTA  
 2243 QUANTA  
 2244 QUANTA  
 2245 QUANTA  
 2246 QUANTA  
 2247 QUANTA  
 2248 QUANTA  
 2249 QUANTA  
 2250 QUANTA  
 2251 QUANTA  
 2252 QUANTA  
 2253 QUANTA  
 2254 QUANTA

```

254 SUBROUTINE ALINT(INTGTS,NWPNS,ALUC,ALUCU)
255 DIMENSION ALUC(INTGTS,NWPNS,J),ALUCU(NWPNS)
256 LEVEL = ALUC,ALUCU
257 C INTEGERIZE THE ALLOCATION MATRIX BY WEAPON GROUPS.
258 C
259 C
260 C
261 C
262 C
263 C
264 C
265 C
266 C
267 C
268 C
269 C
270 C
271 C
272 C
273 C
274 C
275 C
276 C
277 C
278 C
279 C
280 C
281 C
282 C
283 C
284 C
285 C
286 C
287 C
288 C
289 C
290 C
291 C
292 C
293 C
294 C
295 C
296 C
297 C

```

FIND THE TOTAL NUMBER OF WEAPONS ALLOCATED FROM GROUP J  
 ISUM=0  
 MSUM=0  
 DO 10 I=1,NTUTS  
 ISUM=ISUM+INT(ALUC(I,J,1))+INT(ALUC(I,J,2))+INT(ALUC(I,J,3))  
 MSUM=MSUM+ALUC(I,J,1)+ALUC(I,J,2)+ALUC(I,J,3)  
 CONTINUE  
 ISUM = ISUM \* INT(ALUCU(J))  
 MSUM=MSUM\*ALUCU(J)  
 COMPUTE EXCESS NUMBER TO ALLOCATE.  
 N=MSUM-PLANT(I,ISUM)\*.5  
 IF (N.EQ.0) GO TO 40  
 DO 30 IN=1,N  
 FIND MAXIMUM NUMBER IN ALLOCATION ARRAYS.  
 MMAX=0  
 DO 20 IF=1,J  
 DO 20 I=1,NTUTS  
 TEST=ALUC(I,J,IF)-AINT(ALUCU(I,J,IF))  
 IF (TEST.LE.MMAX) GO TO 20  
 MMAX=TEST  
 MAX=I  
 LOC=IF  
 CONTINUE  
 TEST = ALUCU(J) - AINT(ALUCU(J))  
 ALLOCATE ONE TO BASE MAX. ATTACK POINT LOC. FROM GROUP J  
 IF (TEST.LE.MMAX) ALUC(MAX,J,LOC)=AINT(ALUCU(MAX,J,LOC)+1.0)  
 IF (TEST.GT.MMAX) ALUCU(J)=AINT(ALUCU(J)+1.0)  
 CONTINUE  
 FINISH INTEGRIZATION.  
 DO 50 IF=1,J  
 DO 50 I=1,NTUTS  
 ALUC(I,J,IF)=AINT(ALUCU(I,J,IF))  
 CONTINUE  
 ALUCU(J)=AINT(ALUCU(J))  
 CONTINUE TO THE NEXT WEAPON GROUP.  
 CONTINUE  
 RETURN  
 END

PAGE 00

```
2298 SUBROUTINE ALLOCINTG(SUBS,NMPS,ALUC,ISUBS,NMPS)
2299 DIMENSION ALLOCINTG(SUBS,NMPS),ISUBS(SUBS),NMPS(SUBS)
2300 LEVEL = ALUC/ISUBS/NMPS
2301 ALLOC PRINTS OUT ALLOCATION INFORMATION.
2302
2303 CALL PAGE (0)
2304 PRINT OUT BY TARGET LOCATION.
2305 WRITE (0,000)
2306 CALL PAGE (1)
2307 UU 10 1=1,NMPS
2308 CALL PAGE (-2)
2309 WRITE (0,010) *
2310 NMPS=0
2311 UU 10 J=1,NSUBS
2312 NMPS=NMPS(J)
2313 UU 10 K=1,NMPS
2314 NMPS=NMPS+1
2315 ALLOC=ALUC/(NMPS+1)
2316 ALLOC=ALUC/(NMPS+2)
2317 ALPC=ALUC/(NMPS+3)
2318 IF (ALOC*ALOC*ALPC*10.0001) GO TO 10
2319 WRITE (0,020) J,SUBS(J),ALOC,ALPC,ALPC*ALPC
2320 CALL PAGE (1)
2321 CONTINUE
2322
2323 PRINT OUT BY SUBMARINE LOCATION.
2324 NMPS=0
2325 UU 20 J=1,NSUBS
2326 CALL PAGE (-2)
2327 WRITE (0,030) J,ISUBS(J)
2328 NMPS=NMPS(J)
2329 UU 20 K=1,NMPS
2330 NMPS=NMPS+1
2331 UU 20 1=1,NMPS
2332 ALLOC=ALUC/(NMPS+1)
2333 ALLOC=ALUC/(NMPS+2)
2334 ALPC=ALUC/(NMPS+3)
2335 A=ALOC*ALOC*ALPC
2336 IF (A*10.0001) UU 10 20
2337 WRITE (0,040) A*10.0001
2338 CALL PAGE (1)
2339 CONTINUE
2340 RETURN
2341
2342 FUMMAT(0A,25,100),PRINTOUT OF THE OPTIMUM ALLOCATION OF *
2343 * * * * *
2344 FUMMAT(0A,25,100),PRINTOUT OF THE OPTIMUM ALLOCATION OF *
2345 * * * * *
2346 FUMMAT(0A,25,100),PRINTOUT OF THE OPTIMUM ALLOCATION OF *
2347 * * * * *
```

PAGE 69

2348  
2349  
2350

0300 FORMAT(10X,F10.1,0 MISSILES FROM SALVO,13,0 TO TARGET,14,  
0,0 (0,015,1,0 TO BASE),\*)  
END

QUANTA  
QUANTA  
QUANTA

2349  
2350  
2351

```

3331 FUNCTION PMUFLU (XLU,X,Y,NPTS)
3332 DIMENSION X(NPTS), Y(NPTS)
3333 LEVEL=2,X=Y
3334 IF (ALU.LE.X(NPTS),ANU=ALU*DE.X(1)) GO TO 10
3335 IF (ALU.GT.X(NPTS)) GO TO 20
3336 PMUFLU=Y(1)
3337 RETURN
3338
3339 C
3340
3341 I0 N=NPTS
3342 PMUFLU=AUSC(XLU,X,Y,N)
3343 PMUFLU=AMAX1(PMUFLU,Y(1))
3344 RETURN
3345
3346 C
3347
3348 I0 SLOPE=(Y(NPTS)-Y(NPTS-1))/(X(NPTS)-X(NPTS-1))
3349 PMUFLU=Y(NPTS)+SLOPE*(ALU-X(NPTS))
3350 RETURN
3351 ENU
3352
3353 QUANTA
3354
3355 QUANTA
3356
3357 QUANTA
3358
3359 QUANTA
3360
3361 QUANTA
3362
3363 QUANTA
3364
3365 QUANTA
3366
3367 QUANTA
3368
3369 QUANTA
3370

```

QUANTIA	2352
QUANTIA	2353
QUANTIA	2354
QUANTIA	2355
QUANTIA	2356
QUANTIA	2357
QUANTIA	2358
QUANTIA	2359
QUANTIA	2360
QUANTIA	2361
QUANTIA	2362
QUANTIA	2363
QUANTIA	2364
QUANTIA	2365
QUANTIA	2366
QUANTIA	2367
QUANTIA	2368

PAGE 71

```

369  FUNCTION DIST (ALAT,ALNG,YLAT,YLNG)
370  LEVEL 2,ALAT,ALNG,YLAT,YLNG
371  THIS FUNCTION COMPUTES THE GREAT CIRCLE DISTANCE (IN N.M.) BETWEEN
372  POINTS X AND Y WITH LATITUDES AND LONGITUDES GIVEN IN TERMS OF
373  NAUTICALS (NORTH AND WEST ARE POSITIVE).
374  DATA PI/180,PI/90,PI/360
375  A=ABS(ALNG-YLNG)
376  B=PI2-ALAT
377  C=PI2-YLAT
378  CBPC=COS(B-C)
379  X=(.5*(CBPC+CBMC)) + (.5*(COS(A)*(CBMC-CBPC))
380  DIST=3442.2*ALUS(X)
381  RETURN
382  END

```

UUANIA  
 UUANIA  
 UUANIA  
 UUANIA  
 UUANIA  
 UUANIA  
 UUANIA  
 UUANIA  
 UUANIA  
 UUANIA  
 UUANIA  
 UUANIA  
 UUANIA  
 UUANIA  
 UUANIA  
 UUANIA

2369  
 2370  
 2371  
 2372  
 2373  
 2374  
 2375  
 2376  
 2377  
 2378  
 2379  
 2380  
 2381  
 2382  
 2383

PAGE 72

```
2383 SUBROUTINE PAGE (N)
2384 C
2385 C
2386 C
2387 C
2388 C
2389 C
2390 C
2391 C
2392 C
2393 C
2394 C
2395 C
2396 C
2397 C
```

DATA LINE=NP/0.50/

IF (LINE.GT.0) GO TO 1

LINE=LINE+ABS(N)

IF (LINE.LT.0) GO TO 2

NP=NP+1

WRITE(6,N) NP

LINE=0

IF (LINE.LT.0) LINE=-N

RETURN

FORMAT(1MI,3N) PAGE=14/)

END

QUANTIA 2384

QUANTIA 2385

QUANTIA 2386

QUANTIA 2387

QUANTIA 2388

QUANTIA 2389

QUANTIA 2390

QUANTIA 2391

QUANTIA 2392

QUANTIA 2393

QUANTIA 2394

QUANTIA 2395

QUANTIA 2396

QUANTIA 2397

PAGE 73

```

2397 C
2398 C
2399 C
2400 C
2401 C
2402 C
2403 C
2404 C
2405 C
2406 C
2407 C
2408 C
2409 C
2410 C
2411 C
2412 C
2413 C
2414 C
2415 C
2416 C
2417 C
2418 C
2419 C
2420 C
2421 C
2422 C
2423 C
2424 C
2425 C
2426 C
2427 C
2428 C
2429 C
2430 C
2431 C
2432 C
2433 C

FUNCTION SSPT (MM)
ROUTINE TO COMPUTE SOUND SPEED IN METERS/SECOND AS A FUNCTION OF
GEOMETRIC ALTITUDE IN METERS.
BASED ON DATA PRESENTED IN //U.S. STANDARD ATMOSPHERE, 1962//.
ROUTINE BY HARRY M. MURPHY, JR., 29APR71, CORRECTED 30C172 (HMM)
DIMENSION ALT(10), TM(10), UTUZ(10)
DATA ALT/-4996.0,0.0,11019.0,20063.0,32162.0,47350.0,52425.0,61591
1.0,79994.0,90000.0/
DATA TM/320.05,288.15,216.05,216.05,220.05,270.05,252.05,18
10.05,160.05/
DATA UTUZ/-6.50522E-3,-6.4444E-3,0.0,9.9162E-4,2.7653E-3,0.0,-1.997
14E-3,-3.9124E-3,0.0,0.0/
Z=MM
I=1
IF (Z>9000.0) GO,50,20
IF (9000.0-Z) GO,60,30
GO 40 I=1,9
IF (ALT(I+1)-Z) 40,40,50
CONTINUE
I=10
SSPT=20.046796*SQRT(TM(I)+UTUZ(I)*((Z-ALT(I))))
RETURN
SSPT=209.44
RETURN
END
QUANTA 2398
QUANTA 2399
QUANTA 2400
QUANTA 2401
QUANTA 2402
QUANTA 2403
QUANTA 2404
QUANTA 2405
QUANTA 2406
QUANTA 2407
QUANTA 2408
QUANTA 2409
QUANTA 2410
QUANTA 2411
QUANTA 2412
QUANTA 2413
QUANTA 2414
QUANTA 2415
QUANTA 2416
QUANTA 2417
QUANTA 2418
QUANTA 2419
QUANTA 2420
QUANTA 2421
QUANTA 2422
QUANTA 2423
QUANTA 2424
QUANTA 2425
QUANTA 2426
QUANTA 2427
QUANTA 2428
QUANTA 2429
QUANTA 2430
QUANTA 2431
QUANTA 2432
QUANTA 2433

```



```

2433 C FUNCTION AUSEC (AV,X,Y,NAY)
2434 C
2435 C INTERPOLATES A TABLE OF NAY X,Y POINTS AT ENTRY POINT, AV, USING
2436 C FIRST-ORDER HERMITE, OR OSCILLATORY, INTERPOLATION.
2437 C
2438 C ALGORITHM --- EVALUATE A POLYNOMIAL WHICH PASSES THROUGH A PAIR
2439 C OF POINTS, A2,Y2, AND A3,Y3, AND WHICH HAS A GIVEN FIRST DERIVA-
2440 C TIVE AT EACH POINT. IN THIS CASE, THE DERIVATIVE AT POINT 2 IS
2441 C THE MEAN OF THE SLOPES 1-2 AND 2-3, WHILE THE DERIVATIVE AT POINT
2442 C 3 IS THE MEAN OF THE SLOPES 2-3 AND 3-4.
2443 C
2444 C ROUTINE BASED ON //HERMITE INTERPOLATION//, CAM ALGORITHM 211,
2445 C BY G.M. SCHUBERT. (COMM. ACM, OCT 1963.)
2446 C
2447 C NOTE -- THE X-ARRAY MUST MONOTONICALLY INCREASE IN VALUE.
2448 C
2449 C ROUTINE WRITTEN BY HARRY M. MURPHY, AFML/DTM, 4 JAN 1977.
2450 C
2451 C DIMENSION A(NAY), Y(NAY)
2452 C LEVEL 2, XAY
2453 C
2454 C LOGICAL ERROR
2455 C IF (AVALT.AINAY) GO TO 1
2456 C AUSEC(Y,NAY)
2457 C GO TO 3
2458 C
2459 C START. MAKE AV AND NAY LOCAL VARIABLES.
2460 C
2461 C
2462 C CHECK TABLE LENGTH, NAY.
2463 C
2464 C ERROR=EM.L1+2
2465 C IF (ERROR) WRITE (6,*)
2466 C IF (ERROR) GO TO 3
2467 C
2468 C L=(L+M)/2
2469 C IF (X0.GT.X(1)) L=1
2470 C IF (X0.LE.X(1)) M=1
2471 C L=(L+M)/2
2472 C IF (L.LT.1) GO TO 2
2473 C
2474 C WE HAVE THE ENTRY POINT. COMPUTE X2, A3, Y2, AND
2475 C Y3 AS LOCAL VARIABLES.
2476 C
2477 C AC=X(1)
2478 C AJ=X(1+1)
2479 C YC=Y(1)
2480 C YJ=Y(1+1)
2481 C
2482 C SC3=(YJ-YC)/(AJ-AC)
2483 C IF (SC3.LE. .01) GO TO 5
2484 C SIZE=SC3

```

PAGE 75

```

1403 IF (1.0/1.1) 512=(Y(1)-Y(1-1))/(X(1)-X(1-1))
1404 534=523
1405 IF (1.0/1.1) 534=(Y(1+2)-Y(1+1))/(X(1+2)-X(1+1))
1406 C DEFINE SLOPES AT POINTS 2 AND 3.
1407 52=(512+523)/2.0
1408 53=(523+534)/2.0
1409 C PERFORM HERMITE INTERPOLATION AT X0.
1410 AUSC=((X3-X0)*52*(X2-X0)*(Y2*2.0/(X2-X3)-52)+Y2)*(X3-
1411 X0)*(Y3*2.0/(X3-X2)-53)+Y3)/(X3-X2)*52
1412 C RETURN.
1413 3 RETURN
1414 5 AUSC=523*(X0-X2) + Y2
1415 C RETURN
1416 4 FORMAT (1X/40H FUNCTION AUSC ERROR. TABLE LENGTH LESS THAN 2.0/1X)
1417 C
1418 C
1419 C
1420 C
1421 C
1422 C
1423 C
1424 C
1425 C
1426 C
1427 C
1428 C
1429 C
1430 C
1431 C
1432 C
1433 C
1434 C
1435 C
1436 C
1437 C
1438 C
1439 C
1440 C
1441 C
1442 C
1443 C
1444 C
1445 C
1446 C
1447 C
1448 C
1449 C
1450 C
1451 C
1452 C
1453 C
1454 C
1455 C
1456 C
1457 C
1458 C
1459 C
1460 C
1461 C
1462 C
1463 C
1464 C
1465 C
1466 C
1467 C
1468 C
1469 C
1470 C
1471 C
1472 C
1473 C
1474 C
1475 C
1476 C
1477 C
1478 C
1479 C
1480 C
1481 C
1482 C
1483 C
1484 C
1485 C
1486 C
1487 C
1488 C
1489 C
1490 C
1491 C
1492 C
1493 C
1494 C
1495 C
1496 C
1497 C
1498 C
1499 C
1500 C

```

```

1 SUBROUTINE NUCLEUM(SUBR,TEMPUR)
2
3
4
5
6
7
8
9
10
11
12
13
14
15
16
17
18
19
20

```

```

20  C
21  C
22  C
23  C
24  C
25  C
26  C
27  C
28  C
29  C
30  C
31  C
32  C
33  C
34  C
35  C
36  C
37  C
38  C
39  C
40  C
41  C
42  C
43  C
44  C
45  C
46  C
47  C
48  C
49  C
50  C
51  C
52  C
53  C
54  C
55  C
56  C
57  C
58  C
59  C
60  C
61  C
62  C
63  C
64  C
65  C
66  C
67  C
68  C
69  C

SUBROUTINE ATMOS(Z, TM, SIGMA, RHU, THE, TA, DELTA, CA, AMU, K)
  CALLING SEQUENCE
  CALL ATMOS(Z, TM, SIGMA, RHU, THE, TA, DELTA, CA, AMU, K)
  Z = GEOMETRIC ALTITUDE (FT)
  TM = MOLECULAR SCALE TEMPERATURE (DEGREES FARRINHE)
  SIGMA = RATIO OF DENSITY TO THAT AT SEA LEVEL
  RHU = DENSITY (SLUGS/CCU FT)
  THE = RATIO OF TEMPERATURE TO THAT AT SEA LEVEL
  DELTA = RATIO OF PRESSURE TO THAT AT SEA LEVEL
  CA = SPEED OF SOUND (FT/SEC)
  AMU = VISCOSITY COEFFICIENT (LB-SEC/FT**2)
  K = 1 NORMAL
      = 2 ALTITUDE GREATER THAN 30000 FT.
      = 3 ALTITUDE NEGATIVE
  DIMENSION PPM(11), TMB(11), SIGMA(11), ALM(11)
  DATA PPM/0.0, 0.3609, 0.2370, 0.020, 0.797, 1.54199, 4.00, 17.3004, 3.10,
    1.55196, 3.58, 2.55275, 0.90, 3.54444, 1.00, 3.24934, 3.00, 35.7742, 1.0, 0.5561, 1.0, 0.5561,
    2.10, 0.514, 6.08, 3.09, 9.88, 3.09, 3.00, 5.00, 7.00, 5.00, 7.00, 3.00, 1.00, 2.00, 1.00,
    3.45, 1.00, 2.38, 1.00, 2.00, 1.00, 2.38, 1.00, 2.00, 1.00, 2.38, 1.00, 2.00, 1.00, 2.38, 1.00,
    4.3, 2.66, 5.75, 1.0, 0.2, 1.17, 0.70, 0.3, 0.5, 0.67, 0.31, 0.4, 1.0, 0.32, 0.35, 0.5,
    51.7, 92.8, 95.2, 10.0, 0.9, 3.92, 1.51, 0.5, 0.8, 7.6, 5.5, 9.3, 1.0, 5.0, 0.32, 0.48, 7.2, 1.0,
    62.5, 7.2, 7.7, 1.0, 0.7, 0.6, 0.7, 0.6, 0.7, 0.6, 0.7, 0.6, 0.7, 0.6, 0.7, 0.6, 0.7, 0.6,
    7.0, 0.62, 1.4, 0.5, 0.0, 1.0, 0.7, 0.6, 0.7, 0.6, 0.7, 0.6, 0.7, 0.6, 0.7, 0.6, 0.7, 0.6,
    DATA C/0.0, 0.18, 0.17, 0.16, 0.15, 0.14, 0.13, 0.12, 0.11, 0.10, 0.09, 0.08, 0.07,
    1.00, 0.7, 0.3, 0.2, 0.1, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0,
    K=1
    IF (Z) 1, 3, 2
  1 K=3
  RETURN
  C IF (Z.GT.30000.0) K=K+1
  3 PPM=PPM/(K**2)**2
  20 4 PPM=1
  IF (PPM-PPM(M)) 5, 6, 11
  5 CONTINUE
  6 PPM=1
  7 MEM=1
  8 IF (ALM(M)) 7, 8, 7
  7 THE=THE*(M)*ALM(M)**(PPM-PPM(M))
  SIGMA=EXP((1.0*(J/ALM(M)))*ALOG(TMB(M)/TM))**SIGMA(M)
  GO TO 9
  9 THE=TM(M)
  SIGMA=SIGMA*(M)*EXP(-(1.0*(PPM-PPM(M)))/TMB(M))
  7 PPM=PPM/2**SIGMA
  THE=THE/TMB
  DELTA=SIGMA*THE*TA
  CA=49.0217*SQRT(TM)
  AMU=AMU*SQRT(THE*TA**3)*((TM/5)/(TM*5))
  RETURN
  END

```

69		SUBROUTINE INT1 (X, A, AT, Y, M)	70	NUCMMU
70	C	SUBROUTINE INT1 IS A LINEAR INTERPOLATION ROUTINE.	71	NUCMMU
71	C	GIVEN M VALUE A, INT1 RETURNS THE CORRESPONDING VALUE Y.	72	NUCMMU
72	C	JA = DIMENSION OF X-TABLE AND Y-TABLE IN CALLING PROGRAM.	73	NUCMMU
73	C	AT = TABLE OF X-VALUES IN CALLING PROGRAM.	74	NUCMMU
74	C	YI = TABLE OF Y-VALUES IN CALLING PROGRAM.	75	NUCMMU
75	C	M = RETURN VALUE Y.	76	NUCMMU
76		DIMENSION AT (JA), YI (JA)	77	NUCMMU
77	C		78	NUCMMU
78		IF (X-AT(1)) 1,0,2	79	NUCMMU
79		M=YI(1)	80	NUCMMU
80		CALL NUCMM (BM1, INT1, 1)	81	NUCMMU
81	C	IF (X-AT(JA)) 4,0,3	82	NUCMMU
82	C	M=YI(JA)	83	NUCMMU
83		CALL NUCMM (BM1, INT1, 2)	84	NUCMMU
84		DO 5 I=2,JA	85	NUCMMU
85		IF (X-AT(I)) 1,0,5	86	NUCMMU
86		CONTINUE	87	NUCMMU
87	C	M=YI(I)	88	NUCMMU
88		RETURN	89	NUCMMU
89		M=YI(1-1)*(X-AT(1-1))*(YI(1)-YI(1-1))/(AT(1)-AT(1-1))	90	NUCMMU
90			91	NUCMMU
91		RETURN	92	NUCMMU
92		M=YI(1)	93	NUCMMU
93		RETURN	94	NUCMMU
94		M=YI(JA)	95	NUCMMU
95		RETURN	96	NUCMMU
96		END		

```

96      SUBROUTINE I612(A,Y,DX,NY,XI,YT,OFF,INT)
97      DIMENSION P(INT),AT(NX),Y1(INT)
98      IF (A-AT(1)) 35*5,5
99      5  00 10 I=2,NA
100      IF (A-AT(I)) 45*15,10
101      10  00,11*02
102      00 10 35
103      15 IA=I-1
104      IF (Y-YT(1)) 40*20,20
105      20  00 25 I=2,NY
106      IF (Y-YT(I)) 30*30,25
107      25  00,11*02
108      00 15 40
109      30 1Y=I-1
110      11I=(IA-1)*NY+IY
111      11Z=11*I
112      1C1=11*NY
113      1C2=12*I+1
114      F11=F(111)
115      F12=F(112)
116      F21=F(121)
117      F22=F(122)
118      UY=YT(1Y*I)-YT(1Y)
119      UY1=YT(1Y)-Y/UY
120      UY2=YT(1Y+1)-Y/UY
121      F1=UY2*F11-UY1*F12
122      F2=UY2*F21-UY1*F22
123      UX=XT(1X*I)-AT(1X)
124      UX1=AT(1X)-A/UX
125      UX2=AT(1X+1)-A/UX
126      F1=UX2*F1-UY1*F2
127      RETURN
128      35 CALL NUCEPH(BMINI2 ,1)
129      40 CALL NUCEPH(BMINI2 ,2)
130      END

```

```

NUCEPH 97
NUCEPH 98
NUCEPH 99
NUCEPH 100
NUCEPH 101
NUCEPH 102
NUCEPH 103
NUCEPH 104
NUCEPH 105
NUCEPH 106
NUCEPH 107
NUCEPH 108
NUCEPH 109
NUCEPH 110
NUCEPH 111
NUCEPH 112
NUCEPH 113
NUCEPH 114
NUCEPH 115
NUCEPH 116
NUCEPH 117
NUCEPH 118
NUCEPH 119
NUCEPH 120
NUCEPH 121
NUCEPH 122
NUCEPH 123
NUCEPH 124
NUCEPH 125
NUCEPH 126
NUCEPH 127
NUCEPH 128
NUCEPH 129
NUCEPH 130
NUCEPH 31

```

4.52 5

131  
132  
133  
134  
135  
136  
137  
138

FOURTYE EXP(SHE)  
JWEASION, SHM11(6), EXP(6)  
DATA SHM11/0.0025, 5.1, 5.1, 5.500, /  
DATA EXP1/5625, 537, 5642, 575, 500, 500, /  
CALL IN11(SHE, SHM11, EXP1, E)  
EXIT=0  
RETURN  
END

132  
133  
134  
135  
136  
137  
138  
139

132  
133  
134  
135  
136  
137  
138  
139

PAGE 6

```
139 SUBROUTINE SPLITC  
140 COMMON/PLTCLN/MT,SP (3),SRE,00,CTH,S (3),SOUTP,SALT,SHBT,SP T  
141 SAVE=SP (1)  
142 SP (1)=S (1)  
143 S (1)=SAVE  
144 SAVE=SP (2)  
145 SP (2)=S (2)  
146 S (2)=SAVE  
147 SAVE=SP (3)  
148 SP (3)=S (3)  
149 S (3)=SAVE  
150 RETURN  
151 END  
140  
141  
142  
143  
144  
145  
146  
147  
148  
149  
150  
151  
152
```



100 1

```

152 SUBROUTINE UELIM(ALT,MB,MAU,0.01,TR,DEL,DEL,PM)
153 COMMON/ELIM/MAU(50),SMB,0.001,TR(5),SOUT,PSALF,SMOT,SP1
154 SP=SUMI(ALT-MB)*0.2*0.002
155 PUA=SP(5)*0.005
156 UEL IMAGE MUST SLANT RANGE IN FREE AIR POINT
157 SMB = SUMI(ALT-MB)*0.2*0.002
158 FIVE MAJOR SHOCK STRENGTH AT TOP
159 A05=SUMI(SMB*0.2*0.002)
160 IF (A05.LT.0.0) GO TO 50
161 CALL TRINT(-MB,SMB,0.01)
162 CALL ATMOD(MI,0.001,0.002,0.003,0.004,0.005,0.006,0.007)
163 S11=(MI/5(5))**0.1/3.0
164 S12=S11**0.110.40/C
165 CALL SWITCH
166 CALL UELTPP(MI,MB,ATP,SMOT,TR,PM,0.01)
167 CALL SWITCH
168 PUF=S(2)*0.005
169 UEL REFLECTED SHOCK OVERPRESSURE
170 UEL SHOCK STRENGTH IF REFLECTED SHOCK AT TOP
171 UEL TOWN-DUP1
172 UEL IMAGE MUST OVERPRESSURE
173 UEL TOWN-DUP1(SMB)
174 CALL SWITCH
175 UEL TOWN-DUP1(SMB)
176 CALL SWITCH
177 UEL SLANT RANGE OF INCIDENT SHOCK
178 S1=SUMI(MB-MI)*0.2*0.002
179 UEL OVERPRESSURE IN WAKE OF INCIDENT SHOCK
180 TR=WFTR(SM1)
181 KZP = ATZM(TM)
182 PUA=AFPM(TM,KZP)
183 UEL TOWN-DUP1(PUA)
184 IF (SMB.GT.PUA) PUA=SMB*0.000001
185 UEL TOWN-DUP1(PUA)
186 CALCULATE UEL TOWN-DUP1(PUA)
187 PUA=1.0*UPLDUP1(PUA)
188 PUA=AFPM(TM,KZP)
189 UEL TOWN-DUP1(PUA)
190 IF (UPLDUP1(PUA).GT.0.0) GO TO 50
191 IF (UPLDUP1(PUA).LT.0.0) UEL TOWN-DUP1(PUA)
192 SMB=SUMI(PUA/MAU)*0.0025
193 ASUMI(SMB*0.2*0.002)
194 SP=SUMI(ALT-MB)*0.2*0.002
195 GO TO 10
196 RETURN
197 50 S11=ATZM(1.0/3.0)
198 S12=S11
199 S13=1.0
200 PUF=S(5)*0.005
201 CALL SWITCH

```

153  
154  
155  
156  
157  
158  
159  
160  
161  
162  
163  
164  
165  
166  
167  
168  
169  
170  
171  
172  
173  
174  
175  
176  
177  
178  
179  
180  
181  
182  
183  
184  
185  
186  
187  
188  
189  
190  
191  
192  
193  
194  
195  
196  
197  
198  
199  
200  
201  
202

017  
517  
617  
717  
817  
917  
017  
117  
217  
317  
417  
517  
617  
717  
817  
917

```

UP1=UPKUP(SM)
CALL SW1CN
SM=SM/S(1)*0.001
CALL CPMX(SM,PM)
S(1)=S(1)*PM-1.0
S(2)=S(1)
CALL SW1CN
PM=UPKUP(SM)
CALL SW1CN
UP2=UPM-UP1
UPM=UP1+UP(SM)
SM=SM*UP1
SM=SM*UP1
UP=UP
END

```

203	100CMU
204	100CMU
205	100CMU
206	100CMU
207	100CMU
208	100CMU
209	100CMU
210	100CMU
211	100CMU
212	100CMU
213	100CMU
214	100CMU
215	100CMU
216	100CMU
217	100CMU

```

217 SUBROUTINE CMFM(S,M,KFM)
218 DIMENSION KMK(6),SMT(6)
219
220 C
221 C
222 C
223 C
224 C
225 C
226 C
227 C
228 C
229 C
230 C
231 C
232 C
233 C
234 C
235 C
236 C
237 C
238 C
239 C
240 C
241 C
242 C
243 C
244 C
245 C
246 C
247 C
248 C
249 C
250 C
251 C
252 C
253 C
254 C
255 C
256 C
257 C
258 C
259 C
260 C
261 C
262 C
263 C
264 C
265 C
266 C
267 C
268 C
269 C
270 C
271 C
272 C
273 C
274 C
275 C
276 C
277 C
278 C
279 C
280 C
281 C
282 C
283 C
284 C
285 C
286 C
287 C
288 C
289 C
290 C
291 C
292 C
293 C
294 C
295 C
296 C
297 C
298 C
299 C
300 C
301 C
302 C
303 C
304 C
305 C
306 C
307 C
308 C
309 C
310 C
311 C
312 C
313 C
314 C
315 C
316 C
317 C
318 C
319 C
320 C
321 C
322 C
323 C
324 C
325 C
326 C
327 C
328 C
329 C
330 C
331 C
332 C
333 C
334 C
335 C
336 C
337 C
338 C
339 C
340 C
341 C
342 C
343 C
344 C
345 C
346 C
347 C
348 C
349 C
350 C
351 C
352 C
353 C
354 C
355 C
356 C
357 C
358 C
359 C
360 C
361 C
362 C
363 C
364 C
365 C
366 C
367 C
368 C
369 C
370 C
371 C
372 C
373 C
374 C
375 C
376 C
377 C
378 C
379 C
380 C
381 C
382 C
383 C
384 C
385 C
386 C
387 C
388 C
389 C
390 C
391 C
392 C
393 C
394 C
395 C
396 C
397 C
398 C
399 C
400 C
401 C
402 C
403 C
404 C
405 C
406 C
407 C
408 C
409 C
410 C
411 C
412 C
413 C
414 C
415 C
416 C
417 C
418 C
419 C
420 C
421 C
422 C
423 C
424 C
425 C
426 C
427 C
428 C
429 C
430 C
431 C
432 C
433 C
434 C
435 C
436 C
437 C
438 C
439 C
440 C
441 C
442 C
443 C
444 C
445 C
446 C
447 C
448 C
449 C
450 C
451 C
452 C
453 C
454 C
455 C
456 C
457 C
458 C
459 C
460 C
461 C
462 C
463 C
464 C
465 C
466 C
467 C
468 C
469 C
470 C
471 C
472 C
473 C
474 C
475 C
476 C
477 C
478 C
479 C
480 C
481 C
482 C
483 C
484 C
485 C
486 C
487 C
488 C
489 C
490 C
491 C
492 C
493 C
494 C
495 C
496 C
497 C
498 C
499 C
500 C
501 C
502 C
503 C
504 C
505 C
506 C
507 C
508 C
509 C
510 C
511 C
512 C
513 C
514 C
515 C
516 C
517 C
518 C
519 C
520 C
521 C
522 C
523 C
524 C
525 C
526 C
527 C
528 C
529 C
530 C
531 C
532 C
533 C
534 C
535 C
536 C
537 C
538 C
539 C
540 C
541 C
542 C
543 C
544 C
545 C
546 C
547 C
548 C
549 C
550 C
551 C
552 C
553 C
554 C
555 C
556 C
557 C
558 C
559 C
560 C
561 C
562 C
563 C
564 C
565 C
566 C
567 C
568 C
569 C
570 C
571 C
572 C
573 C
574 C
575 C
576 C
577 C
578 C
579 C
580 C
581 C
582 C
583 C
584 C
585 C
586 C
587 C
588 C
589 C
590 C
591 C
592 C
593 C
594 C
595 C
596 C
597 C
598 C
599 C
600 C
601 C
602 C
603 C
604 C
605 C
606 C
607 C
608 C
609 C
610 C
611 C
612 C
613 C
614 C
615 C
616 C
617 C
618 C
619 C
620 C
621 C
622 C
623 C
624 C
625 C
626 C
627 C
628 C
629 C
630 C
631 C
632 C
633 C
634 C
635 C
636 C
637 C
638 C
639 C
640 C
641 C
642 C
643 C
644 C
645 C
646 C
647 C
648 C
649 C
650 C
651 C
652 C
653 C
654 C
655 C
656 C
657 C
658 C
659 C
660 C
661 C
662 C
663 C
664 C
665 C
666 C
667 C
668 C
669 C
670 C
671 C
672 C
673 C
674 C
675 C
676 C
677 C
678 C
679 C
680 C
681 C
682 C
683 C
684 C
685 C
686 C
687 C
688 C
689 C
690 C
691 C
692 C
693 C
694 C
695 C
696 C
697 C
698 C
699 C
700 C
701 C
702 C
703 C
704 C
705 C
706 C
707 C
708 C
709 C
710 C
711 C
712 C
713 C
714 C
715 C
716 C
717 C
718 C
719 C
720 C
721 C
722 C
723 C
724 C
725 C
726 C
727 C
728 C
729 C
730 C
731 C
732 C
733 C
734 C
735 C
736 C
737 C
738 C
739 C
740 C
741 C
742 C
743 C
744 C
745 C
746 C
747 C
748 C
749 C
750 C
751 C
752 C
753 C
754 C
755 C
756 C
757 C
758 C
759 C
760 C
761 C
762 C
763 C
764 C
765 C
766 C
767 C
768 C
769 C
770 C
771 C
772 C
773 C
774 C
775 C
776 C
777 C
778 C
779 C
780 C
781 C
782 C
783 C
784 C
785 C
786 C
787 C
788 C
789 C
790 C
791 C
792 C
793 C
794 C
795 C
796 C
797 C
798 C
799 C
800 C
801 C
802 C
803 C
804 C
805 C
806 C
807 C
808 C
809 C
810 C
811 C
812 C
813 C
814 C
815 C
816 C
817 C
818 C
819 C
820 C
821 C
822 C
823 C
824 C
825 C
826 C
827 C
828 C
829 C
830 C
831 C
832 C
833 C
834 C
835 C
836 C
837 C
838 C
839 C
840 C
841 C
842 C
843 C
844 C
845 C
846 C
847 C
848 C
849 C
850 C
851 C
852 C
853 C
854 C
855 C
856 C
857 C
858 C
859 C
860 C
861 C
862 C
863 C
864 C
865 C
866 C
867 C
868 C
869 C
870 C
871 C
872 C
873 C
874 C
875 C
876 C
877 C
878 C
879 C
880 C
881 C
882 C
883 C
884 C
885 C
886 C
887 C
888 C
889 C
890 C
891 C
892 C
893 C
894 C
895 C
896 C
897 C
898 C
899 C
900 C
901 C
902 C
903 C
904 C
905 C
906 C
907 C
908 C
909 C
910 C
911 C
912 C
913 C
914 C
915 C
916 C
917 C
918 C
919 C
920 C
921 C
922 C
923 C
924 C
925 C
926 C
927 C
928 C
929 C
930 C
931 C
932 C
933 C
934 C
935 C
936 C
937 C
938 C
939 C
940 C
941 C
942 C
943 C
944 C
945 C
946 C
947 C
948 C
949 C
950 C
951 C
952 C
953 C
954 C
955 C
956 C
957 C
958 C
959 C
960 C
961 C
962 C
963 C
964 C
965 C
966 C
967 C
968 C
969 C
970 C
971 C
972 C
973 C
974 C
975 C
976 C
977 C
978 C
979 C
980 C
981 C
982 C
983 C
984 C
985 C
986 C
987 C
988 C
989 C
990 C
991 C
992 C
993 C
994 C
995 C
996 C
997 C
998 C
999 C
1000 C

```

[illegible]

CALCULATES THE WAVEFORM MAJUS AT ZERO OVERPRESSURE, (WZRO). (I.E., THE MAJUS SEPARATING THE NEGATIVE AND POSITIVE PHASE PORTIONS OF THE WAVEFORM, AT THE SPECIFIED TIME (T)).

```

1 - TIME (SEC)
MP/K - RADIUS (CM)

```

CUMMINS/ELLER/MT,ST(3),SMB/GU,CTP,S(3),SGUTP,SALT,SMBT,ST 1  
 DATA B/O.03217,C/-1.056/C/33597.07,BZ/8490.0/  
 T = 11/ST(2)

```

wfZM=0.0
10 (T,LT,0.0) CALL NUCELM(4,MFZM,1)
10 (T,UT,0.0) wfZM=(1.0-UT)*WC*(LZ*10BZ)
END
END

```

231	NUCMMU
232	NUCMMU
233	NUCMMU
234	NUCMMU
235	NUCMMU
236	NUCMMU
237	NUCMMU
238	NUCMMU
239	NUCMMU
240	NUCMMU
241	NUCMMU
242	NUCMMU
243	NUCMMU
244	NUCMMU
245	NUCMMU
246	NUCMMU
247	NUCMMU
248	NUCMMU
249	NUCMMU
250	NUCMMU
251	NUCMMU
252	NUCMMU
253	NUCMMU
254	NUCMMU
255	NUCMMU
256	NUCMMU

P 02 11

```

256      FUNCTION WPM (I, J, K)
257
258      C
259      C
260      C
261      C
262      C
263      C
264      C
265      C
266      C
267      C
268      C
269      C
270      C
271      C
272      C
273      C
274      C
275      C
276      C
277      C
278      C
279      C
280      C
281      C
282      C
283      C
284      C
285      C
286      C
287      C
288      C
289      C
290      C

```

CALCULATES THE WAVEFORM MAJUS AT PEAK OVERPRESSURE (WPM), 1.0...  
 THE MAJUS OF THE SHOCK FRONT, AT THE SPECIFIED TIME (T).

T = TIME (SEC)  
 WPM = MAJUS (T)

THIS MAJUS IS PART OF THE AFWL INT STANDARD BY NEEDHAM ET AL.

COMMON/PLICA/PA1, SF(13), SMO, SOUTP, S(13), SOUTP, SALT, SMO, T, SFT  
 DATA TASF, C0, C05, TPAW1/0.317, TPAW2/0.79,

I = T/ST(2)  
 IF (T.LT.0.) CALL NUCERR(WPM, TPAW1)

IF (T.EQ.0.) GO TO 2  
 CALCULATE MAJUS EXPLICITLY.  
 EARLY TIME FORM.

IF (T.LT.0.20) WPM = C0210.0 \* TPAW1 \* (1.0 \* (1.23 \* T + 0.123)) \*  
 (1.0 - EXP(TASF \* TPAW1))

IF (T.LT.0.1) GO TO 2  
 LATE TIME FORM.

ALI = ALUS(1)  
 ALF = ALI \* 3.39162  
 WPM = KZ \* (1.0 \* C05 \* C015E \* ALI \* (9.03 / ALF \* T - 0.083) / ALF \* T  
 INTERPOLATE TIME INTERPOLATION.

IF (T.LT.0.20) WPM = (WPM \* (T - 0.1) \* AFPM \* (0.20 - T)) / 0.10  
 WPM = WPM

WPM = WPM \* SF(1) / 30.40  
 RETURN  
 END

```

290      FUNCTION APRMT(T1,M1,PK1,UP1,MZP)
291      C
292      C
293      C
294      C
295      C
296      C
297      C
298      C
299      C
300      C
301      C
302      C
303      C
304      C
305      C
306      C
307      C
308      C
309      C
310      C
311      C
312      C
313      C
314      C
315      C
316      C
317      C
318      C
319      C
320      C
321      C
322      C
323      C
324      C
325      C
326      C
327      C
328      C
329      C
330      C
331      C
332      C
333      C
334      C
335      C
336      C
337      C
338      C
339      C
340      C

```

THIS ROUTINE IS PART OF THE AFML-1-1 STANDARD BY NEEDHAM, ET AL.  
 COMMON/FLICK/MT,SP(3),SME,OU,CTP,S(3),SUOTP,SALT,SHBT,SP1  
 DATA TTULU/0.0/  
 T=TI/SP(2)  
 K=M1\*30.48/SP(1)  
 PMAD=PK1\*30.48/SP(1)  
 UPK=UP1/SP(3)/1.45038E-5  
 MPR=PMAD  
 IF (T.LT.0.1) GO TO 3  
 MPR=MPR\*1.E-5  
 M=M\*1.E-5  
 IF (T.EU.TTULU) GO TO 2  
 MZ=RZP  
 MN=MZ/-.9.7163E3\*1.E-12115  
 MZ=MZ\*1.E-5  
 MN=MN\*1.E-5  
 UPMN=2.2E4/(1+SURT(T))-0.5\*UPK  
 MEG=HZ-RMN  
 KPLS=PK-KZ  
 MNP=PK-RMN  
 ALN=UPK/RPLS  
 OLN=UPK/RPLS  
 OPMNL=ALPH\*PMN\*BLN  
 PMLT=ABS(OPMN/UPK)  
 OPMNY=OPMN\*PMLT\*(OPMNLN-OPMN)  
 ALPHA=THNP/(OPMNY-UPK)\*MPLS/OPK1/MNEU  
 BETA=-MPLS\*(ALPHA\*1.0/UPK)  
 FNUZ=XP/KPLS  
 UNUM=ALPHA\*KNP+BETA  
 HCMN=1.0-OPMN/(KNP/UNUM\*UPK)  
 CMMNL=ALUO(BL\*RMN)  
 CGZL=(BETA\*(1.0/BL\*RMN)-1.0/BL\*RMN)/((FNUZ\*CHMNL\*BKNP\*(FNUZ-1.0))\*(1.0/BL\*RMN\*OPK\*OUM))  
 CGZ=EXP(CGZL)  
 BUZL=CMNL/CGZ\*(KNP\*FNUZ)  
 BUZ=EXP(BUZL)  
 MNK=MK-K  
 UN=1.0-BUZ\*(CGZ\*(KNP\*(FNUZ))  
 IF (M\*GT.MZ) UN=(MK-K)/MPLS\*GM\*(K-MZ)/MPLS  
 MK=MK/(ALPHA\*KNP\*BETA)\*UPK  
 UPK=UPK\*MK  
 MPR=MPR\*1.E-5

342	NJCMMU
343	NJCMU
344	NJCMMU
345	NJCMMU
346	NJCMMU
347	NJCMMU
348	NJCMMU
349	NJCMMU
350	NJCMMU
351	NJCMMU
352	NJCMMU
353	NJCMMU
354	NJCMMU
355	NJCMMU
356	NJCMMU
357	NJCMMU
358	NJCMMU

```

R=21.03
IF (T.02=0.95) GO TO 5
IF (T.04,TTULL) GO TO 4

A=5.440E5*(1-1.02)-7.135E5*(1-1.04)
IF (T.LT.0.02) C=7.41E-5*(1-0.02)
IF (T.02=0.02) C=ALU0(-A/(UPR-A))/(KZP-KPK)
D=(UPR-A)*EAP*(-C*KPK)

#LT=A+0.02*AP(C*K)
IF (T.LT.0.1) UPR=#LT
IF (T.02=0.1) UPR=(#LT*(0.95-T)+0.05*(T-0.1))/0.85

TTULL=T
#PRMT=UPR*1.0203BE-5*SF(3)
KTLUK,
NJU

```

359 SUBROUTINE SPARK ( NCASE, W, MS, AL, MU, 359  
 360 \*A, IABOB, WELP, TSA, 360  
 361 \*POINTS, AFA, ATPP, AMS, IFA, TTP, TMS) 361  
 362 SUBROUTINE SPARK AND ITS ASSOCIATED SUBROUTINES HAVE BEEN ADAPTED 362  
 363 BY CAPT DON CARPENT, AFML/AFM, FROM PROGRAM SPARK FURNISHED BY 363  
 364 AFML/AFM. LAST PROGRAM SPARK UPDATE EVENT = JULY 1977. 364  
 365 365  
 366 366  
 367 367  
 368 368  
 369 369  
 370 370  
 371 371  
 372 372  
 373 373  
 374 374  
 375 375  
 376 376  
 377 377  
 378 378  
 379 379  
 380 380  
 381 381  
 382 382  
 383 383  
 384 384  
 385 385  
 386 386  
 387 387  
 388 388  
 389 389  
 390 390  
 391 391  
 392 392  
 393 393  
 394 394  
 395 395  
 396 396  
 397 397  
 398 398  
 399 399  
 400 400  
 401 401  
 402 402  
 403 403  
 404 404  
 405 405  
 406 406  
 407 407  
 408 408

PARAMETERS

THE FOLLOWING INPUT PARAMETERS APPLY TO ALL SPARK CALLS-  
 NCASE = 1 INDICATES OVERPRESSURE AND TSA SOLUTION DESIRED  
 = 2 INDICATES RANGE AND TSA SOLUTIONS DESIRED  
 W = THE WEAPON FIELD IN KILOTONS.  
 MS = THE HEIGHT OF BURST ABOVE THE GROUND IN FEET.  
 AL = THE RECEIVER ALTITUDE ABOVE THE GROUND IN FEET.  
 MU = THE ALTITUDE OF THE GROUND IN FEET ABOVE SEA LEVEL.

THE FOLLOWING PARAMETERS APPLY ONLY WHEN NCASE=1

INPUT-  
 A = THE HORIZONTAL RANGE IN FEET FROM BURST TO RECEIVER  
 OUTPUT-  
 IABOB = 0 INDICATES RECEIVER INTERCEPTED BY FREE AIR SHOCK.  
 = 1 INDICATES RECEIVER INTERCEPTED BY MACH SHOCK  
 WELP = PEAK OVERPRESSURE AT THE RECEIVER IN PSI.  
 TSA = TIME OF SHOCK ARRIVAL AT THE RECEIVER IN SECONDS.  
 THE FOLLOWING PARAMETERS APPLY ONLY WHEN NCASE=2

INPUT-  
 HAMU = THE PEAK OVERPRESSURE IN PSI OF INTEREST AT RECEIVER.  
 OUTPUT-  
 POINTS = A FLAG INDICATING THE HULL OF AREAS IN THE  
 RECEIVER'S ALTITUDE PLANE WHERE THE PEAK OVERPRESSURE  
 EXCEEDS HAMU  
 = 1 INDICATES CIRCLE OF RADIUS AFA.  
 = 2 INDICATES CIRCLE OF RADIUS AMS.  
 = 3 INDICATES CIRCLE OF RADIUS AFA SURROUNDED BY AN  
 ANNULUS OF MAJOR RADIUS AMS AND MINOR RADIUS ATPP.  
 = 0 INDICATES NO AREA.  
 AFA = HORIZONTAL RANGE IN FEET TO POINT AT WHICH FREE AIR  
 PEAK OVERPRESSURE EQUALS HAMU.  
 ATPP = HORIZONTAL RANGE IN FEET TO INTERSECTION OF TRIPLE  
 POINT PATH  
 AMS = HORIZONTAL RANGE IN FEET TO POINT AT WHICH MACH  
 REGION PEAK OVERPRESSURE EQUALS HAMU.  
 TFA = TIME OF FREE AIR SHOCK ARRIVAL AT AFA IN SECONDS.  
 TTP = TIME OF TRIPLE POINT PATH SHOCK ARRIVAL AT ATPP (SEC)  
 TMS = TIME OF MACH SHOCK ARRIVAL AT AMS IN SECONDS.

LOGICAL VALID  
 INITIALIZE REAST AND ATMOSPHERIC PARAMETERS  
 MUSENG=MS  
 KGRU=1



PAGE 15

```

408      ACAL=AL1*MO
409      CALL ELINIT(MOB,*,ACAL1,MO,KOBU)
410      C
411      C
412      C
413      C
414      C
415      C
416      C
417      C
418      C
419      C
420      C
421      C
422      C
423      C
424      C
425      C
426      C
427      C
428      C
429      C
430      C
431      C
432      C
433      C
434      C
435      C

```

ACAL=AL1\*MO  
 CALL ELINIT(MOB,\*,ACAL1,MO,KOBU)  
 IF KCASE=1 FIND DELP AND TSA AT RECEIVER  
 IF KCASE=2 FIND RANGE AND TSA SOLUTIONS AT ALT  
 GET INTERSECTION WITH TRIPLE POINT PATH. TPP  
 IF KGMU.CW.0.00 TO 20  
 CALL GETTPP(ALT,ME,XTPP,SWTPP,TPP,UPP,UPK)  
 IF DPH.LI.MAMU) GO TO 20  
 CALL GETMSIALI,MB,MAKU,AMS,SWTPP,TPP,UPP,UPK  
 POINTS=2.  
 RETURN  
 POINTS=1. OR 0.  
 20 CALL GETTPP(ALT,MB,MAKU,ATP,TPP,VALIU)  
 POINTS=1.  
 IF NOT.VALIU) POINTS=0.  
 IF KGMU.CW.0.0) GO TO 25  
 CALL GETTPP(ALT,MB,MAKU,ATP,TPP,UPP,UPK)  
 25 RETURN  
 END

1. The first of these is the fact that the

2. second is the fact that the

3. third is the fact that the

4. fourth is the fact that the

5. fifth is the fact that the

6. sixth is the fact that the

7. seventh is the fact that the

8. eighth is the fact that the

9. ninth is the fact that the

10. tenth is the fact that the

11. eleventh is the fact that the

12. twelfth is the fact that the

```

485  NODU=0
486  SP(1) = 1.205P(1)
487  SP(2) = 1.205P(2)
488  C  INITIALIZE TRIPLE POINT PARAMETERS IF NECESSARY
489  C  IF (KMOD(NODU,10)EQ0)
490  C  SET MONITORIAL VALUE TO TRIPLE POINT PATH (TTP) ORIGIN (00.)
491  IF (SMPL(2,4)EQ 1, 40)
492  SMPL=SMPL+2+43
493  NODU=SMPL+2+1000.
494  GO TO 50
495  C  CALL INIT(SMPL,14,SMPL+CSOUTP,CSOUTP)
496  CS=SMPL+3P+1000.
497  C  SET SCALED TTP "STRESS" FACTOR(CTP)
498  IF (SMPL(1,1)EQ 10 TO 60)
499  CT=0.04
500  GO TO 70
501  C  CALL INIT(SMPL,10,SMPL+CLTP+CTO)
502  SMPL=SMPL(SMPL+2+SMPL+2)
503  IF (SMPL(2,2)EQ 4) GO TO 80
504  CALL INIT(SMPL+6,SMPL+FMML+CFMML)
505  GO TO 90
506  C  FMML = 1.03+0.40/SMPL+
507  M = SMPL/CI
508  C  S(1) = CFMML*SF(1)
509  S(2) = CFMML*SF(2)
510  TP = SFMPL(M)
511  RETURN
512  END

```

20.4 81

```
513  
514  
515  
516  
517  
518  
519  
520  
521  
522  
523  
524  
525  
526  
527  
528  
529  
530  
531  
532  
533  
534  
535  
536  
537  
538  
539  
540  
541  
542  
543  
544  
545  
546  
547  
548  
549  
550  
551  
552  
553  
554  
555  
556  
557  
558  
559  
560  
561  
562  
563  
564  
565  
566  
567  
568  
569  
570  
571  
572  
573  
574  
575  
576  
577  
578  
579  
580  
581  
582  
583  
584  
585  
586  
587  
588  
589  
590  
591  
592  
593  
594  
595  
596  
597  
598  
599  
600  
601  
602  
603  
604  
605  
606  
607  
608  
609  
610  
611  
612  
613  
614  
615  
616  
617  
618  
619  
620  
621  
622  
623  
624  
625  
626  
627  
628  
629  
630  
631  
632  
633  
634  
635  
636  
637  
638  
639  
640  
641  
642  
643  
644  
645  
646  
647  
648  
649  
650  
651  
652  
653  
654  
655  
656  
657  
658  
659  
660  
661  
662  
663  
664  
665  
666  
667  
668  
669  
670  
671  
672  
673  
674  
675  
676  
677  
678  
679  
680  
681  
682  
683  
684  
685  
686  
687  
688  
689  
690  
691  
692  
693  
694  
695  
696  
697  
698  
699  
700  
701  
702  
703  
704  
705  
706  
707  
708  
709  
710  
711  
712  
713  
714  
715  
716  
717  
718  
719  
720  
721  
722  
723  
724  
725  
726  
727  
728  
729  
730  
731  
732  
733  
734  
735  
736  
737  
738  
739  
740  
741  
742  
743  
744  
745  
746  
747  
748  
749  
750  
751  
752  
753  
754  
755  
756  
757  
758  
759  
760  
761  
762  
763  
764  
765  
766  
767  
768  
769  
770  
771  
772  
773  
774  
775  
776  
777  
778  
779  
780  
781  
782  
783  
784  
785  
786  
787  
788  
789  
790  
791  
792  
793  
794  
795  
796  
797  
798  
799  
800  
801  
802  
803  
804  
805  
806  
807  
808  
809  
810  
811  
812  
813  
814  
815  
816  
817  
818  
819  
820  
821  
822  
823  
824  
825  
826  
827  
828  
829  
830  
831  
832  
833  
834  
835  
836  
837  
838  
839  
840  
841  
842  
843  
844  
845  
846  
847  
848  
849  
850  
851  
852  
853  
854  
855  
856  
857  
858  
859  
860  
861  
862  
863  
864  
865  
866  
867  
868  
869  
870  
871  
872  
873  
874  
875  
876  
877  
878  
879  
880  
881  
882  
883  
884  
885  
886  
887  
888  
889  
890  
891  
892  
893  
894  
895  
896  
897  
898  
899  
900  
901  
902  
903  
904  
905  
906  
907  
908  
909  
910  
911  
912  
913  
914  
915  
916  
917  
918  
919  
920  
921  
922  
923  
924  
925  
926  
927  
928  
929  
930  
931  
932  
933  
934  
935  
936  
937  
938  
939  
940  
941  
942  
943  
944  
945  
946  
947  
948  
949  
950  
951  
952  
953  
954  
955  
956  
957  
958  
959  
960  
961  
962  
963  
964  
965  
966  
967  
968  
969  
970  
971  
972  
973  
974  
975  
976  
977  
978  
979  
980  
981  
982  
983  
984  
985  
986  
987  
988  
989  
990  
991  
992  
993  
994  
995  
996  
997  
998  
999  
1000
```

```

524 SUBROUTINE BLAST(X,Z,SH,MB,ROU,LAB,ST,OUT)
525 COMMON/BLAST/MT,ST(3),SH,MB,CT,PS(3),SUCTP,SALT,SMBT,SFT
526 IF (IGNORING GROUND REFLECTANCE GET FREE AIR SHOCK
527 IF (GROUND,ROU,OUT) TO 10
528 IF HORIZONTAL RANGE LESS THAN RANGE TO TYP ORIGIN IGNORE
529 REFLECTANCE
530 IF (X,CT,OUT) TO 10
531 GET HEIGHT OF TYP AT HORIZONTAL RANGE
532 HTP=ROU*CTP/(X,OUT-1.0)*1.0
533 IF RECEIVER ABOVE TYP HEIGHT IGNORE GROUND REFLECTANCE
534 IF (Z,ROU,OUT) TO 10
535 GET MATCH SHOCK
536 LAB=ST
537 GET SLANT RANGE FROM GROUND ZERO TO RECEIVER
538 SMOZ=SM/(LAB*Z/ROU)
539 GET OVERPRESSURE
540 OUT=TPROU/(SMOZ*OINT,MINI)
541 GET SLANT RANGE FROM BURST TO INTERSECTION POINT
542 MT=SM/(OINT*OZ*(MINI-MB)*OZ)
543 GET TIME OF SHOCK ARRIVAL (T)
544 T=MT*(MT)
545 RETURN
546 GET FREE AIR SHOCK
547 LAB=ST
548 GET TIME OF SHOCK ARRIVAL (T)
549 T=MT*(MT)
550 IF (LAB,ST,OUT) TO 10
551 IF (LAB,ST,OUT) TO 10
552 IF (LAB,ST,OUT) TO 10
553 IF (LAB,ST,OUT) TO 10
554 IF (LAB,ST,OUT) TO 10
555 IF (LAB,ST,OUT) TO 10
556 IF (LAB,ST,OUT) TO 10
557 IF (LAB,ST,OUT) TO 10
558 IF (LAB,ST,OUT) TO 10
559 IF (LAB,ST,OUT) TO 10
560 IF (LAB,ST,OUT) TO 10
561 IF (LAB,ST,OUT) TO 10

```

PAGE 20

561	SUBROUTINE GETIP(ALT,ME,X,SMGZ,T,UPR,MUDU)	NUCMUD	562
562	COMMON/ELICK/ARL,SP(3)*SMO,DU,CLP*5(3)*SUGIP*SALT*SMOT,SPT	NUCMUD	563
563	GET HORIZONTAL RANGE TO INTERSECTION OF IMPLE POINT PATH	NUCMUD	564
564	CELT(SMT)	NUCMUD	565
565	X=DU*((ALT/CLP/50)**2+1.)	NUCMUD	566
566	GET TIME OF SHOCK ARRIVAL AT INTERSECTION	NUCMUD	567
567	SHESMT=((ALT-MB)**2*X**2)	NUCMUD	568
568	TEFTU(SM)	NUCMUD	569
569	GET FREE AIM SHOCK AT INTERSECTION	NUCMUD	570
570	UPID=APPROX(SM)	NUCMUD	571
571	GET MAGN SHOCK AT INTERSECTION	NUCMUD	572
572	SMGZ=SUPT(ALT**2*X**2)	NUCMUD	573
573	UPMETPROX(SMGZ,SINT,HINT)	NUCMUD	574
574	RETURN	NUCMUD	575
575	END	NUCMUD	576

PAGE 21

```
576 SUBROUTINE DELTA(TIME,MARK,XX,T,VALUE)
577 LOGICAL VALUE
578 Z=ALTIME
579 SP=ABS(Z)*.01
580 VALUE=.TRUE.
581 C ITERATE TO FIND SLANT RANGE TO MARK
582 10 X=SP**2-2*ZC
583 IF (X<0.0) GO TO 20
584 DELTA=PRGNT(SK)
585 IF (ABS(DELTA-MARK)/.01>.01) MARK=GO TO 30
586 SP=SP*(DELTA/MARK)**.25
587 GO TO 10
588 C NO SOLUTION
589 VALUE=.FALSE.
590 X=0.0
591 T=0.0
592 RETURN
593 C SOLUTION FOUND
594 X=SUMT(X)
595 T=FTPT(SK)
596 RETURN
597 END
```

```
NUCMOD 577
NUCMOD 578
NUCMOD 579
NUCMOD 580
NUCMOD 581
NUCMOD 582
NUCMOD 583
NUCMOD 584
NUCMOD 585
NUCMOD 586
NUCMOD 587
NUCMOD 588
NUCMOD 589
NUCMOD 590
NUCMOD 591
NUCMOD 592
NUCMOD 593
NUCMOD 594
NUCMOD 595
NUCMOD 596
NUCMOD 597
NUCMOD 598
```

PAGE 22

```

590 SUBROUTINE GETMS(CALTIME,MAMU,X,SKIP,PT)
591 CUMMU=PT*CUK/RT*SF (3)*SM*100,CIP,S(3)*SOUTP*SALT*SM*1*SF I
592 SMZ=SM*TP
593 IF (ABS(DELCP-MAMU).LT..01)*MAMU)100 TO 30
594 SMZ=SMZ*(DELCP/MAMU)**25
595 IF (SMZ*.LT*.SKIP)100 TO 20
596 GO TO 10
597 NO SOLUTION
598 20 CALL NUCLEK(CMU,IMS,1)
599 SOLUTION FOUND
600 A=SGRT(SMZ**2-ALT**2)
601 GET TSA
602 SM=SGRT(CU*INT**2*(1-MO-MI*1)**2)
603 T=FT*P(SM)
604 RETURN
605 END

```

```

599 NUCMOD
600 NUCMOD
601 NUCMOD
602 NUCMOD
603 NUCMOD
604 NUCMOD
605 NUCMOD
606 NUCMOD
607 NUCMOD
608 NUCMOD
609 NUCMOD
610 NUCMOD
611 NUCMOD
612 NUCMOD
613 NUCMOD
614 NUCMOD
615 NUCMOD

```



[illegible]

PAGE 24

```

641 C
642 C
643 C
644 C
645 C
646 C
647 C
648 C
649 C
650 C
651 C
652 C
653 C
654 C
655 C
656 C
657 C
658 C
659 C
660 C
661 C

FUNCTION WFTP(WFT)
  R = MAJUS (FEET)
  WFTP = TIME AT PEAK (SEC)
  COMMON/FLICK/WAL,SF(3),SMB,GG,CIP,S(3),SOUTP,SALT,SMOT,SPT
  CONVERT FROM FEET TO METERS
  R=WFT*.3048/SF(1)
  IF (WALT.57.0)GO TO 10
  A=SQRT(R)
  Y=SQRT(X)
  WFTP=.0029551*R-.06348*Y-.50446/X+.28741/(R**(.2+.3))-263.5/(X**Y)
  GO TO 20
10 WFTP=X*(1.7455/E-4+R*(-2.0)16E-5+R*(1.3371E-6+R*(-3.6325E-8+R*
  *(4.5554E-10+R*(-2.0)1633E-12))))
20 CONTINUE
  WFTP=WFTP*SF(2)
  IF (WFTP.LT.0.)CALL NUCLERM(OM*WFTP ,1)
  RETURN
END

```

NUCMUU 642  
 NUCMUU 643  
 NUCMUU 644  
 NUCMUU 645  
 NUCMUU 646  
 NUCMUU 647  
 NUCMUU 648  
 NUCMUU 649  
 NUCMUU 650  
 NUCMUU 651  
 NUCMUU 652  
 NUCMUU 653  
 NUCMUU 654  
 NUCMUU 655  
 NUCMUU 656  
 NUCMUU 657  
 NUCMUU 658  
 NUCMUU 659  
 NUCMUU 660  
 NUCMUU 661

```

0601 C
0602 C
0603 C
0604 C
0605 C
0606 C
0607 C
0608 C
0609 C
0610 C
0611 C
0612 C
0613 C
0614 C
0615 C
0616 C
0617 C
0618 C
0619 C
0620 C
0621 C
0622 C
0623 C
0624 C
0625 C
0626 C
0627 C
0628 C
0629 C
0630 C
0631 C
0632 C
0633 C
0634 C
0635 C
0636 C
0637 C
0638 C
0639 C
0640 C
0641 C
0642 C
0643 C
0644 C
0645 C
0646 C
0647 C
0648 C
0649 C
0650 C
0651 C
0652 C
0653 C
0654 C
0655 C
0656 C
0657 C
0658 C
0659 C
0660 C
0661 C
0662 C
0663 C
0664 C
0665 C
0666 C
0667 C
0668 C
0669 C
0670 C
0671 C
0672 C
0673 C
0674 C
0675 C
0676 C
0677 C
0678 C
0679 C
0680 C
0681 C
0682 C
0683 C
0684 C
0685 C
0686 C
0687 C
0688 C
0689 C
0690 C
0691 C
0692 C
0693 C
0694 C
0695 C
0696 C
0697 C
0698 C
0699 C
0700 C
0701 C
0702 C
0703 C
0704 C
0705 C
0706 C
0707 C
0708 C
0709 C
0710 C
0711 C
0712 C
0713 C
0714 C
0715 C
0716 C
0717 C
0718 C
0719 C
0720 C
0721 C
0722 C
0723 C
0724 C
0725 C
0726 C
0727 C
0728 C
0729 C
0730 C
0731 C
0732 C
0733 C
0734 C
0735 C
0736 C
0737 C
0738 C
0739 C
0740 C
0741 C
0742 C
0743 C
0744 C
0745 C
0746 C
0747 C
0748 C
0749 C
0750 C
0751 C
0752 C
0753 C
0754 C
0755 C
0756 C
0757 C
0758 C
0759 C
0760 C
0761 C
0762 C
0763 C
0764 C
0765 C
0766 C
0767 C
0768 C
0769 C
0770 C
0771 C
0772 C
0773 C
0774 C
0775 C
0776 C
0777 C
0778 C
0779 C
0780 C
0781 C
0782 C
0783 C
0784 C
0785 C
0786 C
0787 C
0788 C
0789 C
0790 C
0791 C
0792 C
0793 C
0794 C
0795 C
0796 C
0797 C
0798 C
0799 C
0800 C
0801 C
0802 C
0803 C
0804 C
0805 C
0806 C
0807 C
0808 C
0809 C
0810 C
0811 C
0812 C
0813 C
0814 C
0815 C
0816 C
0817 C
0818 C
0819 C
0820 C
0821 C
0822 C
0823 C
0824 C
0825 C
0826 C
0827 C
0828 C
0829 C
0830 C
0831 C
0832 C
0833 C
0834 C
0835 C
0836 C
0837 C
0838 C
0839 C
0840 C
0841 C
0842 C
0843 C
0844 C
0845 C
0846 C
0847 C
0848 C
0849 C
0850 C
0851 C
0852 C
0853 C
0854 C
0855 C
0856 C
0857 C
0858 C
0859 C
0860 C
0861 C
0862 C
0863 C
0864 C
0865 C
0866 C
0867 C
0868 C
0869 C
0870 C
0871 C
0872 C
0873 C
0874 C
0875 C
0876 C
0877 C
0878 C
0879 C
0880 C
0881 C
0882 C
0883 C
0884 C
0885 C
0886 C
0887 C
0888 C
0889 C
0890 C
0891 C
0892 C
0893 C
0894 C
0895 C
0896 C
0897 C
0898 C
0899 C
0900 C
0901 C
0902 C
0903 C
0904 C
0905 C
0906 C
0907 C
0908 C
0909 C
0910 C
0911 C
0912 C
0913 C
0914 C
0915 C
0916 C
0917 C
0918 C
0919 C
0920 C
0921 C
0922 C
0923 C
0924 C
0925 C
0926 C
0927 C
0928 C
0929 C
0930 C
0931 C
0932 C
0933 C
0934 C
0935 C
0936 C
0937 C
0938 C
0939 C
0940 C
0941 C
0942 C
0943 C
0944 C
0945 C
0946 C
0947 C
0948 C
0949 C
0950 C
0951 C
0952 C
0953 C
0954 C
0955 C
0956 C
0957 C
0958 C
0959 C
0960 C
0961 C
0962 C
0963 C
0964 C
0965 C
0966 C
0967 C
0968 C
0969 C
0970 C
0971 C
0972 C
0973 C
0974 C
0975 C
0976 C
0977 C
0978 C
0979 C
0980 C
0981 C
0982 C
0983 C
0984 C
0985 C
0986 C
0987 C
0988 C
0989 C
0990 C
0991 C
0992 C
0993 C
0994 C
0995 C
0996 C
0997 C
0998 C
0999 C
1000 C

```

```

686 C SUBROUTINE TPI(M,M1,U1)
687 C GIVEN M, M1, U1, SUBROUTINE TPI RETURNS M1 AND U1.
688 C M IS THE HEIGHT OF THE CENTER OF THE CIRCLE
689 C M1 IS THE HEIGHT OF THE CENTER OF THE CIRCLE
690 C M1 IS THE HEIGHT OF THE CENTER OF THE CIRCLE
691 C M1 IS THE HEIGHT OF THE CENTER OF THE CIRCLE
692 C M1 IS THE HEIGHT OF THE CENTER OF THE CIRCLE
693 C M1 IS THE HEIGHT OF THE CENTER OF THE CIRCLE
694 C M1 IS THE HEIGHT OF THE CENTER OF THE CIRCLE
695 C M1 IS THE HEIGHT OF THE CENTER OF THE CIRCLE
696 C M1 IS THE HEIGHT OF THE CENTER OF THE CIRCLE
697 C M1 IS THE HEIGHT OF THE CENTER OF THE CIRCLE
698 C M1 IS THE HEIGHT OF THE CENTER OF THE CIRCLE
699 C M1 IS THE HEIGHT OF THE CENTER OF THE CIRCLE
700 C M1 IS THE HEIGHT OF THE CENTER OF THE CIRCLE
701 C M1 IS THE HEIGHT OF THE CENTER OF THE CIRCLE
702 C M1 IS THE HEIGHT OF THE CENTER OF THE CIRCLE
703 C M1 IS THE HEIGHT OF THE CENTER OF THE CIRCLE
704 C M1 IS THE HEIGHT OF THE CENTER OF THE CIRCLE
705 C M1 IS THE HEIGHT OF THE CENTER OF THE CIRCLE
706 C M1 IS THE HEIGHT OF THE CENTER OF THE CIRCLE
707 C M1 IS THE HEIGHT OF THE CENTER OF THE CIRCLE
708 C M1 IS THE HEIGHT OF THE CENTER OF THE CIRCLE
709 C M1 IS THE HEIGHT OF THE CENTER OF THE CIRCLE
710 C M1 IS THE HEIGHT OF THE CENTER OF THE CIRCLE
711 C M1 IS THE HEIGHT OF THE CENTER OF THE CIRCLE
712 C M1 IS THE HEIGHT OF THE CENTER OF THE CIRCLE
713 C M1 IS THE HEIGHT OF THE CENTER OF THE CIRCLE
714 C M1 IS THE HEIGHT OF THE CENTER OF THE CIRCLE
715 C M1 IS THE HEIGHT OF THE CENTER OF THE CIRCLE

```

```

NUCMU 687
NUCMU 688
NUCMU 689
NUCMU 690
NUCMU 691
NUCMU 692
NUCMU 693
NUCMU 694
NUCMU 695
NUCMU 696
NUCMU 697
NUCMU 698
NUCMU 699
NUCMU 700
NUCMU 701
NUCMU 702
NUCMU 703
NUCMU 704
NUCMU 705
NUCMU 706
NUCMU 707
NUCMU 708
NUCMU 709
NUCMU 710
NUCMU 711
NUCMU 712
NUCMU 713
NUCMU 714
NUCMU 715

```

715	C	SUBROUTINE SNAME( MM,	ACALT,	ACVEL,	HANGLE,	VAROFL,	NUCMU
716	C	BANGLE, YIELD,	MOB,	TERMT,	ALBEDU,	VISIOL,	NUCMU
717	C	VAPUR, CLUALT,	CLUUA,	CLUOUT,	UC,	UU,	NUCMU
718	C	UM,	CL,	VALU,	NOTNEW,	WRTFLG,	NUCMU
719	C	SUBROUTINE SNAME AND ITS ASSOCIATED SUBROUTINES HAVE BEEN ADAPTED					NUCMU
720	C	BY CAPT S.D. GARRETT, AFWL/OTVM, FROM PROGRAM SNAME FURNISHED BY					NUCMU
721	C	AFWL/OTVM.					NUCMU
722	C						NUCMU
723	C						NUCMU
724	C						NUCMU
725	C						NUCMU
726	C						NUCMU
727	C						NUCMU
728	C						NUCMU
729	C						NUCMU
730	C						NUCMU
731	C						NUCMU
732	C						NUCMU
733	C						NUCMU
734	C						NUCMU
735	C						NUCMU
736	C						NUCMU
737	C						NUCMU
738	C						NUCMU
739	C						NUCMU
740	C						NUCMU
741	C						NUCMU
742	C						NUCMU
743	C						NUCMU
744	C						NUCMU
745	C						NUCMU
746	C						NUCMU
747	C						NUCMU
748	C						NUCMU
749	C						NUCMU
750	C						NUCMU
751	C						NUCMU
752	C						NUCMU
753	C						NUCMU
754	C						NUCMU
755	C						NUCMU
756	C						NUCMU
757	C						NUCMU
758	C						NUCMU
759	C						NUCMU
760	C						NUCMU
761	C						NUCMU
762	C						NUCMU
763	C						NUCMU
764	C						NUCMU

INPUT PARAMETERS

MM = THE HORIZONTAL RANGE IN FEET FROM BURST TO RECEIVER.

ACALT = THE RECEIVER ALTITUDE ABOVE THE GROUND IN FEET.

ALVEL = THE RECEIVER VELOCITY IN FEET/SEC RELATIVE TO THE BURST.

HANGLE = THE HORIZONTAL ANGLE IN DEGREES CLOCKWISE THAT THE RECEIVER PANEL IS ROTATED FROM PERPENDICULAR TO THE BURST.

VAROFL = THE VERTICAL ANGLE IN DEGREES THAT THE RECEIVER PANEL IS ROTATED FROM PERPENDICULAR TO THE BURST. POSITIVE WHEN NORMAL TO PANEL POINTS ABOVE THE BURST.

BANGLE = THE HORIZONTAL ANGLE IN DEGREES FROM THE NOSE OF THE RECEIVER CLOCKWISE TO THE BURST.

YIELD = THE WEAPON YIELD IN KILOTONS.

MUB = THE HEIGHT OF BURST ABOVE THE GROUND IN FEET.

TERMT = THE ALTITUDE OF THE GROUND IN FEET ABOVE SEA LEVEL.

ALBEDU = GROUND REFLECTANCE (.23 FOR SAC NORMAL DAY).

VISIBL = VISIBILITY IN STATUTE MILES (10. FOR SAC NORMAL DAY).

VAPUR = SEA LEVEL WATER VAPOR PRESSURE (MM HG) (5. FOR SAC NORMAL DAY).

CLUALT = ALTITUDE OF CLOUD LAYER ABOVE THE GROUND IN FEET.

CLUUA = ALBEDU OF THE CLOUD.

CLUOUT = TRANSMISSIVITY OF THE CLOUD.

ROUTNE = A LOGICAL VARIABLE WHICH IF .TRUE. INDICATES THAT THE SOLUTION SLANT RANGE FOUND FOR THE PREVIOUS PROBLEM SHOULD BE USED AS THE INITIAL ESTIMATE FOR THIS RANGE SOLUTION PROBLEM.

WRTFLG = A LOGICAL VARIABLE WHICH IF .TRUE. CAUSES A MESSAGE TO BE WRITTEN WHENEVER THE RECEIVER ENTERS THE FIREBALL AND HENCE A CALORY LEVEL OF 10000 CAL/CM2 IS RETURNED.

OUTPUT PARAMETERS

UC = TOTAL THERMAL RADIATION INCIDENT ON RECEIVER PANEL IN CAL/CM2.

UU = DIRECT THERMAL RADIATION INCIDENT ON RECEIVER PANEL IN CAL/CM2.

UM = REFLECTED THERMAL RADIATION INCIDENT ON RECEIVER PANEL IN CAL/CM2.

CAL = IF POSITIVE FLGS THAT THE HORIZONTAL RANGE TO THE POINT IN THE ACALT PLANE AT WHICH CAL CAL/CM2 OF THERMAL RADIATION IS INCIDENT ON THE RECEIVER PANEL IS DESIRED.

IF NEGATIVE FLGS THAT THE THERMAL RADIATION INCIDENT ON

PAGE 20

```

705 C THE RECEIVER PANEL AT THE RECEIVER LOCATION SPECIFIED BY NUCMUU
706 C NR AND ACALIT IS DESIRED. NUCMUU
707 C = THE HORIZONTAL RANGE IN FEET TO THE POINT AT WHICH THERMAL NUCMUU
708 C RADIATION INCIDENT ON THE RECEIVER PANEL EQUALS CAL. NUCMUU
709 C VALUE = A LOGICAL VARIABLE WHICH FLIPS HIGH=0.50 WHEN FALSE. NUCMUU
710 C NUCMUU
711 C NUCMUU
712 C NUCMUU
713 C NUCMUU
714 C NUCMUU
715 C NUCMUU
716 C NUCMUU
717 C NUCMUU
718 C NUCMUU
719 C NUCMUU
720 C NUCMUU
721 C NUCMUU
722 C NUCMUU
723 C NUCMUU
724 C NUCMUU
725 C NUCMUU
726 C NUCMUU
727 C NUCMUU
728 C NUCMUU
729 C NUCMUU
730 C NUCMUU
731 C NUCMUU
732 C NUCMUU
733 C NUCMUU
734 C NUCMUU
735 C NUCMUU
736 C NUCMUU
737 C NUCMUU
738 C NUCMUU
739 C NUCMUU
740 C NUCMUU
741 C NUCMUU
742 C NUCMUU
743 C NUCMUU
744 C NUCMUU
745 C NUCMUU
746 C NUCMUU
747 C NUCMUU
748 C NUCMUU
749 C NUCMUU
750 C NUCMUU
751 C NUCMUU
752 C NUCMUU
753 C NUCMUU
754 C NUCMUU
755 C NUCMUU
756 C NUCMUU
757 C NUCMUU
758 C NUCMUU
759 C NUCMUU
760 C NUCMUU
761 C NUCMUU
762 C NUCMUU
763 C NUCMUU
764 C NUCMUU
765 C NUCMUU
766 C NUCMUU
767 C NUCMUU
768 C NUCMUU
769 C NUCMUU
770 C NUCMUU
771 C NUCMUU
772 C NUCMUU
773 C NUCMUU
774 C NUCMUU
775 C NUCMUU
776 C NUCMUU
777 C NUCMUU
778 C NUCMUU
779 C NUCMUU
780 C NUCMUU
781 C NUCMUU
782 C NUCMUU
783 C NUCMUU
784 C NUCMUU
785 C NUCMUU
786 C NUCMUU
787 C NUCMUU
788 C NUCMUU
789 C NUCMUU
790 C NUCMUU
791 C NUCMUU
792 C NUCMUU
793 C NUCMUU
794 C NUCMUU
795 C NUCMUU
796 C NUCMUU
797 C NUCMUU
798 C NUCMUU
799 C NUCMUU
800 C NUCMUU
801 C NUCMUU
802 C NUCMUU
803 C NUCMUU
804 C NUCMUU
805 C NUCMUU
806 C NUCMUU
807 C NUCMUU
808 C NUCMUU
809 C NUCMUU
810 C NUCMUU
811 C NUCMUU
812 C NUCMUU
813 C NUCMUU
814 C NUCMUU
815 C NUCMUU

```



PAGE 30

```

805 C
806 C
807 C
808 C
809 C
810 C
811 C
812 C
813 C
814 C
815 C
816 C
817 C
818 C
819 C
820 C
821 C
822 C
823 C
824 C
825 C
826 C
827 C
828 C
829 C
830 C
831 C
832 C
833 C
834 C
835 C
836 C
837 C
838 C
839 C
840 C
841 C
842 C
843 C
844 C
845 C
846 C
847 C
848 C
849 C
850 C
851 C
852 C
853 C
854 C
855 C
856 C
857 C
858 C
859 C
860 C
861 C
862 C
863 C
864 C
865 C
866 C
867 C
868 C
869 C
870 C
871 C
872 C
873 C
874 C
875 C
876 C
877 C
878 C
879 C
880 C
881 C
882 C
883 C
884 C
885 C
886 C
887 C
888 C
889 C
890 C
891 C
892 C
893 C
894 C
895 C
896 C
897 C
898 C
899 C
900 C
901 C
902 C
903 C
904 C
905 C
906 C
907 C
908 C
909 C
910 C
911 C
912 C
913 C
914 C
915 C

14 MURE=SUMT(MREST*REST-DIFALT*DIFALT)
15 BVANG=ATANG(MUR*DIFALT)
16 IF (BVANG.LE.0.) BVANG=BVANG*PI
17 AF=HUB*CUS(BVANG)
18 YP=HUB*RSIN(BVANG)
19 ZP=DIFALT
20 PHANG=BHANG*HANGLE*HANGU
21 PVANG=BVANG*VANGLE*HANGU
22 AN=RSIN(PVANG)*CUS(PHANG)
23 YN=RSIN(PVANG)*SIN(PHANG)
24 ZN=ECUS(PVANG)
25 C
26 C INITIALIZE THE THERMAL RADIATION VARIABLES
27 C
28 C
29 C
30 C
31 C
32 C
33 C
34 C
35 C
36 C
37 C
38 C
39 C
40 C
41 C
42 C
43 C
44 C
45 C
46 C
47 C
48 C
49 C
50 C
51 C
52 C
53 C
54 C
55 C
56 C
57 C
58 C
59 C
60 C
61 C
62 C
63 C
64 C
65 C
66 C
67 C
68 C
69 C
70 C
71 C
72 C
73 C
74 C
75 C
76 C
77 C
78 C
79 C
80 C
81 C
82 C
83 C
84 C
85 C
86 C
87 C
88 C
89 C
90 C
91 C
92 C
93 C
94 C
95 C
96 C
97 C
98 C
99 C
100 C
101 C
102 C
103 C
104 C
105 C
106 C
107 C
108 C
109 C
110 C
111 C
112 C
113 C
114 C
115 C

116 C
117 C
118 C
119 C
120 C
121 C
122 C
123 C
124 C
125 C
126 C
127 C
128 C
129 C
130 C
131 C
132 C
133 C
134 C
135 C
136 C
137 C
138 C
139 C
140 C
141 C
142 C
143 C
144 C
145 C
146 C
147 C
148 C
149 C
150 C
151 C
152 C
153 C
154 C
155 C
156 C
157 C
158 C
159 C
160 C
161 C
162 C
163 C
164 C
165 C
166 C
167 C
168 C
169 C
170 C
171 C
172 C
173 C
174 C
175 C
176 C
177 C
178 C
179 C
180 C
181 C
182 C
183 C
184 C
185 C
186 C
187 C
188 C
189 C
190 C
191 C
192 C
193 C
194 C
195 C
196 C
197 C
198 C
199 C
200 C
201 C
202 C
203 C
204 C
205 C
206 C
207 C
208 C
209 C
210 C
211 C
212 C
213 C
214 C
215 C
216 C
217 C
218 C
219 C
220 C
221 C
222 C
223 C
224 C
225 C
226 C
227 C
228 C
229 C
230 C
231 C
232 C
233 C
234 C
235 C
236 C
237 C
238 C
239 C
240 C
241 C
242 C
243 C
244 C
245 C
246 C
247 C
248 C
249 C
250 C
251 C
252 C
253 C
254 C
255 C
256 C
257 C
258 C
259 C
260 C
261 C
262 C
263 C
264 C
265 C
266 C
267 C
268 C
269 C
270 C
271 C
272 C
273 C
274 C
275 C
276 C
277 C
278 C
279 C
280 C
281 C
282 C
283 C
284 C
285 C
286 C
287 C
288 C
289 C
290 C
291 C
292 C
293 C
294 C
295 C
296 C
297 C
298 C
299 C
300 C
301 C
302 C
303 C
304 C
305 C
306 C
307 C
308 C
309 C
310 C
311 C
312 C
313 C
314 C
315 C
316 C
317 C
318 C
319 C
320 C
321 C
322 C
323 C
324 C
325 C
326 C
327 C
328 C
329 C
330 C
331 C
332 C
333 C
334 C
335 C
336 C
337 C
338 C
339 C
340 C
341 C
342 C
343 C
344 C
345 C
346 C
347 C
348 C
349 C
350 C
351 C
352 C
353 C
354 C
355 C
356 C
357 C
358 C
359 C
360 C
361 C
362 C
363 C
364 C
365 C
366 C
367 C
368 C
369 C
370 C
371 C
372 C
373 C
374 C
375 C
376 C
377 C
378 C
379 C
380 C
381 C
382 C
383 C
384 C
385 C
386 C
387 C
388 C
389 C
390 C
391 C
392 C
393 C
394 C
395 C
396 C
397 C
398 C
399 C
400 C
401 C
402 C
403 C
404 C
405 C
406 C
407 C
408 C
409 C
410 C
411 C
412 C
413 C
414 C
415 C
416 C
417 C
418 C
419 C
420 C
421 C
422 C
423 C
424 C
425 C
426 C
427 C
428 C
429 C
430 C
431 C
432 C
433 C
434 C
435 C
436 C
437 C
438 C
439 C
440 C
441 C
442 C
443 C
444 C
445 C
446 C
447 C
448 C
449 C
450 C
451 C
452 C
453 C
454 C
455 C
456 C
457 C
458 C
459 C
460 C
461 C
462 C
463 C
464 C
465 C
466 C
467 C
468 C
469 C
470 C
471 C
472 C
473 C
474 C
475 C
476 C
477 C
478 C
479 C
480 C
481 C
482 C
483 C
484 C
485 C
486 C
487 C
488 C
489 C
490 C
491 C
492 C
493 C
494 C
495 C
496 C
497 C
498 C
499 C
500 C
501 C
502 C
503 C
504 C
505 C
506 C
507 C
508 C
509 C
510 C
511 C
512 C
513 C
514 C
515 C
516 C
517 C
518 C
519 C
520 C
521 C
522 C
523 C
524 C
525 C
526 C
527 C
528 C
529 C
530 C
531 C
532 C
533 C
534 C
535 C
536 C
537 C
538 C
539 C
540 C
541 C
542 C
543 C
544 C
545 C
546 C
547 C
548 C
549 C
550 C
551 C
552 C
553 C
554 C
555 C
556 C
557 C
558 C
559 C
560 C
561 C
562 C
563 C
564 C
565 C
566 C
567 C
568 C
569 C
570 C
571 C
572 C
573 C
574 C
575 C
576 C
577 C
578 C
579 C
580 C
581 C
582 C
583 C
584 C
585 C
586 C
587 C
588 C
589 C
590 C
591 C
592 C
593 C
594 C
595 C
596 C
597 C
598 C
599 C
600 C
601 C
602 C
603 C
604 C
605 C
606 C
607 C
608 C
609 C
610 C
611 C
612 C
613 C
614 C
615 C
616 C
617 C
618 C
619 C
620 C
621 C
622 C
623 C
624 C
625 C
626 C
627 C
628 C
629 C
630 C
631 C
632 C
633 C
634 C
635 C
636 C
637 C
638 C
639 C
640 C
641 C
642 C
643 C
644 C
645 C
646 C
647 C
648 C
649 C
650 C
651 C
652 C
653 C
654 C
655 C
656 C
657 C
658 C
659 C
660 C
661 C
662 C
663 C
664 C
665 C
666 C
667 C
668 C
669 C
670 C
671 C
672 C
673 C
674 C
675 C
676 C
677 C
678 C
679 C
680 C
681 C
682 C
683 C
684 C
685 C
686 C
687 C
688 C
689 C
690 C
691 C
692 C
693 C
694 C
695 C
696 C
697 C
698 C
699 C
700 C
701 C
702 C
703 C
704 C
705 C
706 C
707 C
708 C
709 C
710 C
711 C
712 C
713 C
714 C
715 C
716 C
717 C
718 C
719 C
720 C
721 C
722 C
723 C
724 C
725 C
726 C
727 C
728 C
729 C
730 C
731 C
732 C
733 C
734 C
735 C
736 C
737 C
738 C
739 C
740 C
741 C
742 C
743 C
744 C
745 C
746 C
747 C
748 C
749 C
750 C
751 C
752 C
753 C
754 C
755 C
756 C
757 C
758 C
759 C
760 C
761 C
762 C
763 C
764 C
765 C
766 C
767 C
768 C
769 C
770 C
771 C
772 C
773 C
774 C
775 C
776 C
777 C
778 C
779 C
780 C
781 C
782 C
783 C
784 C
785 C
786 C
787 C
788 C
789 C
790 C
791 C
792 C
793 C
794 C
795 C
796 C
797 C
798 C
799 C
800 C
801 C
802 C
803 C
804 C
805 C
806 C
807 C
808 C
809 C
810 C
811 C
812 C
813 C
814 C
815 C
816 C
817 C
818 C
819 C
820 C
821 C
822 C
823 C
824 C
825 C
826 C
827 C
828 C
829 C
830 C
831 C
832 C
833 C
834 C
835 C
836 C
837 C
838 C
839 C
840 C
841 C
842 C
843 C
844 C
845 C
846 C
847 C
848 C
849 C
850 C
851 C
852 C
853 C
854 C
855 C
856 C
857 C
858 C
859 C
860 C
861 C
862 C
863 C
864 C
865 C
866 C
867 C
868 C
869 C
870 C
871 C
872 C
873 C
874 C
875 C
876 C
877 C
878 C
879 C
880 C
881 C
882 C
883 C
884 C
885 C
886 C
887 C
888 C
889 C
890 C
891 C
892 C
893 C
894 C
895 C
896 C
897 C
898 C
899 C
900 C
901 C
902 C
903 C
904 C
905 C
906 C
907 C
908 C
909 C
910 C
911 C
912 C
913 C
914 C
915 C
916 C
917 C
918 C
919 C
920 C
921 C
922 C
923 C
924 C
925 C
926 C
927 C
928 C
929 C
930 C
931 C
932 C
933 C
934 C
935 C
936 C
937 C
938 C
939 C
940 C
941 C
942 C
943 C
944 C
945 C
946 C
947 C
948 C
949 C
950 C
951 C
952 C
953 C
954 C
955 C
956 C
957 C
958 C
959 C
960 C
961 C
962 C
963 C
964 C
965 C
966 C
967 C
968 C
969 C
970 C
971 C
972 C
973 C
974 C
975 C
976 C
977 C
978 C
979 C
980 C
981 C
982 C
983 C
984 C
985 C
986 C
987 C
988 C
989 C
990 C
991 C
992 C
993 C
994 C
995 C
996 C
997 C
998 C
999 C

```



```

915 20 CALL AHEAD(IMEALS,SNIP,POFLAG)
916 IF (PFLAG.EQ.1.)GO TO 45
917 UU = 39.0577 * U
918 WKATE = UU / UELTIM
919 UC = UU * UC
920 UV = UU / VF
921 UV = UU + UV * AA
922 WK = WK + UV * AB
923 IF (TIME .LT. IMAX) GO TO 20
924 IF (WKATE .GE. U.027) GO TO 20
925 CALL UMM(BALTIM,MMK,REST,UC,UU,WK)
926
927 C IF LEVEL SOLUTION ONLY DESIRED, RETURN
928
929 C
930 IF (CAL.LT.U.U)RETURN
931
932 C SEE IF U NEAR CAL. IF NOT, CHANGE TARGET POSITION, AND REPEAT
933
934 IF (ABS(U-CAL).LT.0.01)CALIRETURN
935 IF (JJJ.GT.10)GO TO 40
936 REST=GUESN(JJJ,CAL,UC,WKATE)
937 IF (REST.GT.AMB) AND (REST.GT.ABS(DIFFERENCE) TO 14
938 PFLAG=1.
939 REST=AMAX1(MFB*.01,(ABS(DIFFAL)*.01))
940 GO TO 14
941
942 C ABNORMAL RETURNS
943
944 C
945 C
946 C
947 C
948 C
949 C
950 C
951 C
952 C
953 C
954 C
955 C
956 C
957 C
958 C
959 C
960 C
961 C
962 C
963 C
964 C
965 C
966 C
967 C
968 C
969 C
970 C
971 C
972 C
973 C
974 C
975 C
976 C
977 C
978 C
979 C
980 C
981 C
982 C
983 C
984 C
985 C
986 C
987 C
988 C
989 C
990 C
991 C
992 C
993 C
994 C
995 C
996 C
997 C
998 C
999 C
1000 C
1001 C
1002 C
1003 C
1004 C
1005 C
1006 C
1007 C
1008 C
1009 C
1010 C
1011 C
1012 C
1013 C
1014 C
1015 C
1016 C
1017 C
1018 C
1019 C
1020 C
1021 C
1022 C
1023 C
1024 C
1025 C
1026 C
1027 C
1028 C
1029 C
1030 C
1031 C
1032 C
1033 C
1034 C
1035 C
1036 C
1037 C
1038 C
1039 C
1040 C
1041 C
1042 C
1043 C
1044 C
1045 C
1046 C
1047 C
1048 C
1049 C
1050 C
1051 C
1052 C
1053 C
1054 C
1055 C
1056 C
1057 C
1058 C
1059 C
1060 C
1061 C
1062 C
1063 C
1064 C
1065 C
1066 C
1067 C
1068 C
1069 C
1070 C
1071 C
1072 C
1073 C
1074 C
1075 C
1076 C
1077 C
1078 C
1079 C
1080 C
1081 C
1082 C
1083 C
1084 C
1085 C
1086 C
1087 C
1088 C
1089 C
1090 C
1091 C
1092 C
1093 C
1094 C
1095 C
1096 C
1097 C
1098 C
1099 C
1100 C
1101 C
1102 C
1103 C
1104 C
1105 C
1106 C
1107 C
1108 C
1109 C
1110 C
1111 C
1112 C
1113 C
1114 C
1115 C
1116 C
1117 C
1118 C
1119 C
1120 C
1121 C
1122 C
1123 C
1124 C
1125 C
1126 C
1127 C
1128 C
1129 C
1130 C
1131 C
1132 C
1133 C
1134 C
1135 C
1136 C
1137 C
1138 C
1139 C
1140 C
1141 C
1142 C
1143 C
1144 C
1145 C
1146 C
1147 C
1148 C
1149 C
1150 C
1151 C
1152 C
1153 C
1154 C
1155 C
1156 C
1157 C
1158 C
1159 C
1160 C
1161 C
1162 C
1163 C
1164 C
1165 C
1166 C
1167 C
1168 C
1169 C
1170 C
1171 C
1172 C
1173 C
1174 C
1175 C
1176 C
1177 C
1178 C
1179 C
1180 C
1181 C
1182 C
1183 C
1184 C
1185 C
1186 C
1187 C
1188 C
1189 C
1190 C
1191 C
1192 C
1193 C
1194 C
1195 C
1196 C
1197 C
1198 C
1199 C
1200 C
1201 C
1202 C
1203 C
1204 C
1205 C
1206 C
1207 C
1208 C
1209 C
1210 C
1211 C
1212 C
1213 C
1214 C
1215 C
1216 C
1217 C
1218 C
1219 C
1220 C
1221 C
1222 C
1223 C
1224 C
1225 C
1226 C
1227 C
1228 C
1229 C
1230 C
1231 C
1232 C
1233 C
1234 C
1235 C
1236 C
1237 C
1238 C
1239 C
1240 C
1241 C
1242 C
1243 C
1244 C
1245 C
1246 C
1247 C
1248 C
1249 C
1250 C
1251 C
1252 C
1253 C
1254 C
1255 C
1256 C
1257 C
1258 C
1259 C
1260 C
1261 C
1262 C
1263 C
1264 C
1265 C
1266 C
1267 C
1268 C
1269 C
1270 C
1271 C
1272 C
1273 C
1274 C
1275 C
1276 C
1277 C
1278 C
1279 C
1280 C
1281 C
1282 C
1283 C
1284 C
1285 C
1286 C
1287 C
1288 C
1289 C
1290 C
1291 C
1292 C
1293 C
1294 C
1295 C
1296 C
1297 C
1298 C
1299 C
1300 C
1301 C
1302 C
1303 C
1304 C
1305 C
1306 C
1307 C
1308 C
1309 C
1310 C
1311 C
1312 C
1313 C
1314 C
1315 C
1316 C
1317 C
1318 C
1319 C
1320 C
1321 C
1322 C
1323 C
1324 C
1325 C
1326 C
1327 C
1328 C
1329 C
1330 C
1331 C
1332 C
1333 C
1334 C
1335 C
1336 C
1337 C
1338 C
1339 C
1340 C
1341 C
1342 C
1343 C
1344 C
1345 C
1346 C
1347 C
1348 C
1349 C
1350 C
1351 C
1352 C
1353 C
1354 C
1355 C
1356 C
1357 C
1358 C
1359 C
1360 C
1361 C
1362 C
1363 C
1364 C
1365 C
1366 C
1367 C
1368 C
1369 C
1370 C
1371 C
1372 C
1373 C
1374 C
1375 C
1376 C
1377 C
1378 C
1379 C
1380 C
1381 C
1382 C
1383 C
1384 C
1385 C
1386 C
1387 C
1388 C
1389 C
1390 C
1391 C
1392 C
1393 C
1394 C
1395 C
1396 C
1397 C
1398 C
1399 C
1400 C
1401 C
1402 C
1403 C
1404 C
1405 C
1406 C
1407 C
1408 C
1409 C
1410 C
1411 C
1412 C
1413 C
1414 C
1415 C
1416 C
1417 C
1418 C
1419 C
1420 C
1421 C
1422 C
1423 C
1424 C
1425 C
1426 C
1427 C
1428 C
1429 C
1430 C
1431 C
1432 C
1433 C
1434 C
1435 C
1436 C
1437 C
1438 C
1439 C
1440 C
1441 C
1442 C
1443 C
1444 C
1445 C
1446 C
1447 C
1448 C
1449 C
1450 C
1451 C
1452 C
1453 C
1454 C
1455 C
1456 C
1457 C
1458 C
1459 C
1460 C
1461 C
1462 C
1463 C
1464 C
1465 C
1466 C
1467 C
1468 C
1469 C
1470 C
1471 C
1472 C
1473 C
1474 C
1475 C
1476 C
1477 C
1478 C
1479 C
1480 C
1481 C
1482 C
1483 C
1484 C
1485 C
1486 C
1487 C
1488 C
1489 C
1490 C
1491 C
1492 C
1493 C
1494 C
1495 C
1496 C
1497 C
1498 C
1499 C
1500 C
1501 C
1502 C
1503 C
1504 C
1505 C
1506 C
1507 C
1508 C
1509 C
1510 C
1511 C
1512 C
1513 C
1514 C
1515 C
1516 C
1517 C
1518 C
1519 C
1520 C
1521 C
1522 C
1523 C
1524 C
1525 C
1526 C
1527 C
1528 C
1529 C
1530 C
1531 C
1532 C
1533 C
1534 C
1535 C
1536 C
1537 C
1538 C
1539 C
1540 C
1541 C
1542 C
1543 C
1544 C
1545 C
1546 C
1547 C
1548 C
1549 C
1550 C
1551 C
1552 C
1553 C
1554 C
1555 C
1556 C
1557 C
1558 C
1559 C
1560 C
1561 C
1562 C
1563 C
1564 C
1565 C
1566 C
1567 C
1568 C
1569 C
1570 C
1571 C

```

```

957 C      SUMMU(1:10) = AREAT(IHEATS,SKIP,FBFLAG)
958 C
959 C      COMMON /SNCM/
960 C      AA, CALI, AP, AC,
961 C      AAR, CHEFL, OFB,
962 C      IIC, HF, ICLUD, NML,
963 C      HFB, TC, TRAU, VF,
964 C      ZFB, XNA, ZNA
965 C
966 C      LUMMU /SNCM/
967 C      AURCAV(14), URM,
968 C      TCU(14), TUZ(14),
969 C      TRATW(14), WCUZ, WIN(16)
970 C
971 C      LOGICAL SKIP
972 C
973 C      DIMENSION URAUWL(14)
974 C      DIMENSION HEATS(400)
975 C
976 C      DATA P1/3.14159265359/
977 C
978 C      W=0
979 C      IF (CHEFL.EQ.1.) CALL VIEWF(VVVF,FBFLAG)
980 C      IF (FBFLAG.EQ.1.) RETURN
981 C      VF = VVVF
982 C      AA=VF
983 C      IF (CHEFL.EQ.1.) CALL IHEATS(14)
984 C      IF (SKIP) GO TO 1
985 C      IHEATS=IHEATS+1
986 C      URAU=PUREN(TRAU)
987 C      HEATS(IHEATS)=URAU
988 C      MAAT=IHEATS
989 C      GO TO 2
990 C
991 C      1 IHEATS=IHEATS+1
992 C      IF (IHEATS.GT.MAAT) GO TO 3
993 C      URAU=HEATS(IHEATS)
994 C      MAAT=IHEATS
995 C      GO TO 2
996 C
997 C      2 CONTINUE
998 C      IF (CHEFL.EQ.0.) GO TO 12
999 C
1000 C      CALCULATE EFFECTIVE ALBEDOS AND GEOMETRIES
1001 C
1002 C      IF (ICLUUD.EQ.1) GO TO 6
1003 C      AUE=AU
1004 C      ACE=0.0
1005 C      GO TO 10
1006 C
1007 C      IF (ALTI.GT.CALI) GO TO 8
1008 C      IF (FBALTI.GT.CALI) GO TO 7
1009 C      AUE=AG*(1.0+AL)
1010 C      ACE=AC*(1.0+AU)
1011 C      GO TO 10
1012 C
1013 C      7 AUE=AG*TC
1014 C      ACE=TC
1015 C
1016 C

```

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

NUCMU

958

959

960

961

962

963

964

965

966

967

968

969

970

971

972

973

974

975

976

977

978

979

980

981

982

983

984

985

986

987

988

989

990

991

992

993

994

995

996

997

998

999

1000

1001

1002

1003

1004

1005

1006

1007

ALF,

GALI,

UHM(14),

YFE,

AG,

FBALI,

W,

XFB,

SIGAVE(14),

TRWL(14),

AC,

OFB,

NML,

VF,

ZNA

URM,

TUZ(14),

WIN(16)

AA,

CALI,

CHEFL,

OFB,

ICLUUD,

NML,

VF,

IC,

TRAU,

YNA,

ZNA

URM,

TUZ(14),

WIN(16)

WCUZ,

WIN(16)

WCUZ,

WIN(16)

WCUZ,

WIN(16)

WCUZ,

WIN(16)

WCUZ,

WIN(16)

WCUZ,

WIN(16)



PAGE 34

1057  
1058

RETURN  
END

NUCMOD 1058  
NUCMOD 1059

```

1059 FUNCTION QUESN(JJJ,WANT,UC,REST)
1060 DIMENSION TRY(10),CALC(10)
1061 CALC(JJJ)=UC
1062 TRY(JJJ)=REST
1063 IF (JJJ.EQ.1) GO TO 4
1064 A1=0.
1065 A2=0.
1066 A3=0.
1067 A4=0.
1068 ZN=0.
1069 DO 2 I=1,JJJ
1070 Z=1./((WANT-CALC(I))*2
1071 A=ALOG(TRY(I))
1072 C=ALOG(CALC(I))
1073 ZN=ZN+Z
1074 A1=A1+A*Z
1075 AC=A2+A*Z
1076 A3=A3+A*C*Z
1077 A4=A4+C*Z
1078 YVAL=(AC*A3-A1*A4)/(A2*AC-A1*ZN)
1079 SLOPE=(A3-YVAL)/A1
1080 A=EXP(YVAL)
1081 B=SLOPE
1082 QUESN=(WANT/A)**(1./B)
1083 RETURN
1084 B=-Z.
1085 A=CALC(1)+TRY(1)*2
1086 GO TO 3
1087 END

```

```

NUCMU 1060
NUCMU 1061
NUCMU 1062
NUCMU 1063
NUCMU 1064
NUCMU 1065
NUCMU 1066
NUCMU 1067
NUCMU 1068
NUCMU 1069
NUCMU 1070
NUCMU 1071
NUCMU 1072
NUCMU 1073
NUCMU 1074
NUCMU 1075
NUCMU 1076
NUCMU 1077
NUCMU 1078
NUCMU 1079
NUCMU 1080
NUCMU 1081
NUCMU 1082
NUCMU 1083
NUCMU 1084
NUCMU 1085
NUCMU 1086
NUCMU 1087
NUCMU 1088

```

P. 62 36

```

1088 SUBROUTINE UMM(BURST,WM,HUMF,MEST,UC,UU,UR)
1089 IF (W.GT.500.0) GO TO 20
1090 SHUB=BURST/(W*(1.73.1))
1091 IF (SHUB.GT.369.0) GO TO 20
1092 IF (SHUB.GE.177.0.AND.SHUB.LE.369.0) THSU=6.21*1.0E+06*(W/BURST**3)
1093 I=(2.0E-08)
1094 IF (SHUB.LT.177.0) THSU=1.0
1095 IF (SHUB.GT.369.0) THSU=0.0
1096 TSU=1.0-THSU
1097 IF (SHUB.LE.183.0) FMW=(3.41E-3*SHUB)*1.0
1098 IF (SHUB.GT.183.0) FMW=1.63
1099 SINT=(HUMF/MEST)
1100 THETA1=(2.0/3.0)*ASIN(SINT)
1101 THETA=COS(THETA1)
1102 FACTOR=((TSU)*(THSU*FMW*THETA))
1103 UC=UC*FACTOR
1104 UR=UR*FACTOR
1105 UU=UU*FACTOR
1106 GO TO 21
1107 UC=UC
1108 UR=UR
1109 UU=UU
1110 CONTINUE
1111 RETURN
1112 END
1089 NUCMOD
1090 NUCMOD
1091 NUCMOD
1092 NUCMOD
1093 NUCMOD
1094 NUCMOD
1095 NUCMOD
1096 NUCMOD
1097 NUCMOD
1098 NUCMOD
1099 NUCMOD
1100 NUCMOD
1101 NUCMOD
1102 NUCMOD
1103 NUCMOD
1104 NUCMOD
1105 NUCMOD
1106 NUCMOD
1107 NUCMOD
1108 NUCMOD
1109 NUCMOD
1110 NUCMOD
1111 NUCMOD
1112 NUCMOD
1113 NUCMOD

```

```

1113 C SUBROUTINE AINT (ZF1,ZF2,WAVEL,V,IMUN,PAVE,WIN,SIGAVE,AUACAV,WCUZ)
1114 C
1115 C COMPUTES REQUIRED ALTITUDE INTEGRALS
1116 C ZF1 AND ZF2 ARE SOURCE AND RECEIVER ALTITUDES IN FEET.
1117 C WAVEL IS THE CENTER WAVE LENGTH IN MICRONS.
1118 C V IS THE SURFACE VISUAL RANGE IN MILES.
1119 C IMUN IS ATMOSPHERE CODE - 1 = WET ATMOSPHERE
1120 C 2 = DRY ATMOSPHERE
1121 C PAVE IS THE RETURNED AVERAGE PRESSURE IN MM-HG.
1122 C WIN IS THE RETURNED WATER INTEGRAL FOR EIGHT DIFFERENT
1123 C VALUES OF EXPONENTS OF PRESSURE.
1124 C
1125 C IF ZF1=ZF2, VALUE OF INTEGRAND IS RETURNED IN WIN.
1126 C SIGAVE IS THE RETURNED AVERAGE SCATTERING COEFFICIENT IN KM-1.
1127 C AUACAV IS THE RETURNED AVERAGE ATMOSPHERIC OZONE ABSORPTION
1128 C COEFFICIENT IN KM-1.
1129 C WCUZ IS THE RETURNED CARBON DIOXIDE CONCENTRATION IN ATMOS-CM/KM.
1130 C
1131 C DIMENSION WIN(8), EX(8), WAVEL(14), SIGAVE(14), AUACAV(4), AUA(4)
1132 C
1133 C DATA EX/0.0,0.43,0.52,0.54,0.60,0.61,0.62,0.64/
1134 C
1135 C IF (ABS(ZF1-ZF2).GT.33.0) GO TO 3
1136 C CALL ATMUS(ZF1,TM,X2X,MHU,THETA,PAVE,CA,AMU,K)
1137 C PAVE=760.0*PAVE
1138 C CALL WATMHU (ZF1,IMUN,RHUH)
1139 C
1140 C DO 1 I=1,8
1141 C WIN(I)=PAVE*EX(I)*MHU
1142 C
1143 C DO 2 J=AND=1,14
1144 C ALAM=WAVEL (IDAND)
1145 C CALL SCAT (ZF1,ALAM,V,SIG)
1146 C SIGAVE (IDAND)=SIG
1147 C CALL OZAL (ZF1,AUACAV)
1148 C CALL WCUZP (ZF1,WCUZ*U)
1149 C WCUZ=-WCUZ
1150 C RETURN
1151 C
1152 C UZ=ABS(ZF1-ZF2)/20.0
1153 C Z=AMIN1(ZF1,ZF2)-UZ/Z.0
1154 C PAVE=0.0
1155 C DO 4 I=1,8
1156 C WIN(I)=0.0
1157 C
1158 C DO 5 IDAND=1,14
1159 C SIGAVE (IDAND)=0.0
1160 C
1161 C DO 6 J=1,14
1162 C AUACAV (J)=0.0
1163 C
1164 C DO 10 J=1,20
1165 C Z=Z*U/
1166 C CALL ATMUS (Z,TM,X2X,MHU,THETA,P,CA,AMU,K)
1167 C P=760.0*P
1168 C PAVE=PAVE*P
1169 C
1170 C
1171 C
1172 C
1173 C
1174 C
1175 C
1176 C
1177 C
1178 C
1179 C
1180 C
1181 C
1182 C
1183 C
1184 C
1185 C
1186 C
1187 C
1188 C
1189 C
1190 C
1191 C
1192 C
1193 C
1194 C
1195 C
1196 C
1197 C
1198 C
1199 C
1200 C
1201 C
1202 C
1203 C
1204 C
1205 C
1206 C
1207 C
1208 C
1209 C
1210 C
1211 C
1212 C
1213 C
1214 C
1215 C
1216 C
1217 C
1218 C
1219 C
1220 C
1221 C
1222 C
1223 C
1224 C
1225 C
1226 C
1227 C
1228 C
1229 C
1230 C
1231 C
1232 C
1233 C
1234 C
1235 C
1236 C
1237 C
1238 C
1239 C
1240 C
1241 C
1242 C
1243 C
1244 C
1245 C
1246 C
1247 C
1248 C
1249 C
1250 C
1251 C
1252 C
1253 C
1254 C
1255 C
1256 C
1257 C
1258 C
1259 C
1260 C
1261 C
1262 C
1263 C
1264 C
1265 C
1266 C
1267 C
1268 C
1269 C
1270 C
1271 C
1272 C
1273 C
1274 C
1275 C
1276 C
1277 C
1278 C
1279 C
1280 C
1281 C
1282 C
1283 C
1284 C
1285 C
1286 C
1287 C
1288 C
1289 C
1290 C
1291 C
1292 C
1293 C
1294 C
1295 C
1296 C
1297 C
1298 C
1299 C
1300 C
1301 C
1302 C
1303 C
1304 C
1305 C
1306 C
1307 C
1308 C
1309 C
1310 C
1311 C
1312 C
1313 C
1314 C
1315 C
1316 C
1317 C
1318 C
1319 C
1320 C
1321 C
1322 C
1323 C
1324 C
1325 C
1326 C
1327 C
1328 C
1329 C
1330 C
1331 C
1332 C
1333 C
1334 C
1335 C
1336 C
1337 C
1338 C
1339 C
1340 C
1341 C
1342 C
1343 C
1344 C
1345 C
1346 C
1347 C
1348 C
1349 C
1350 C
1351 C
1352 C
1353 C
1354 C
1355 C
1356 C
1357 C
1358 C
1359 C
1360 C
1361 C
1362 C
1363 C
1364 C
1365 C
1366 C
1367 C
1368 C
1369 C
1370 C
1371 C
1372 C
1373 C
1374 C
1375 C
1376 C
1377 C
1378 C
1379 C
1380 C
1381 C
1382 C
1383 C
1384 C
1385 C
1386 C
1387 C
1388 C
1389 C
1390 C
1391 C
1392 C
1393 C
1394 C
1395 C
1396 C
1397 C
1398 C
1399 C
1400 C
1401 C
1402 C
1403 C
1404 C
1405 C
1406 C
1407 C
1408 C
1409 C
1410 C
1411 C
1412 C
1413 C
1414 C
1415 C
1416 C
1417 C
1418 C
1419 C
1420 C
1421 C
1422 C
1423 C
1424 C
1425 C
1426 C
1427 C
1428 C
1429 C
1430 C
1431 C
1432 C
1433 C
1434 C
1435 C
1436 C
1437 C
1438 C
1439 C
1440 C
1441 C
1442 C
1443 C
1444 C
1445 C
1446 C
1447 C
1448 C
1449 C
1450 C
1451 C
1452 C
1453 C
1454 C
1455 C
1456 C
1457 C
1458 C
1459 C
1460 C
1461 C
1462 C
1463 C
1464 C
1465 C
1466 C
1467 C
1468 C
1469 C
1470 C
1471 C
1472 C
1473 C
1474 C
1475 C
1476 C
1477 C
1478 C
1479 C
1480 C
1481 C
1482 C
1483 C
1484 C
1485 C
1486 C
1487 C
1488 C
1489 C
1490 C
1491 C
1492 C
1493 C
1494 C
1495 C
1496 C
1497 C
1498 C
1499 C
1500 C
1501 C
1502 C
1503 C
1504 C
1505 C
1506 C
1507 C
1508 C
1509 C
1510 C
1511 C
1512 C
1513 C
1514 C
1515 C
1516 C
1517 C
1518 C
1519 C
1520 C
1521 C
1522 C
1523 C
1524 C
1525 C
1526 C
1527 C
1528 C
1529 C
1530 C
1531 C
1532 C
1533 C
1534 C
1535 C
1536 C
1537 C
1538 C
1539 C
1540 C
1541 C
1542 C
1543 C
1544 C
1545 C
1546 C
1547 C
1548 C
1549 C
1550 C
1551 C
1552 C
1553 C
1554 C
1555 C
1556 C
1557 C
1558 C
1559 C
1560 C
1561 C
1562 C
1563 C
1564 C
1565 C
1566 C
1567 C
1568 C
1569 C
1570 C
1571 C
1572 C
1573 C
1574 C
1575 C
1576 C
1577 C
1578 C
1579 C
1580 C
1581 C
1582 C
1583 C
1584 C
1585 C
1586 C
1587 C
1588 C
1589 C
1590 C
1591 C
1592 C
1593 C
1594 C
1595 C
1596 C
1597 C
1598 C
1599 C
1600 C
1601 C
1602 C
1603 C
1604 C
1605 C
1606 C
1607 C
1608 C
1609 C
1610 C
1611 C
1612 C
1613 C
1614 C
1615 C
1616 C
1617 C
1618 C
1619 C
1620 C
1621 C
1622 C
1623 C
1624 C
1625 C
1626 C
1627 C
1628 C
1629 C
1630 C
1631 C
1632 C
1633 C
1634 C
1635 C
1636 C
1637 C
1638 C
1639 C
1640 C
1641 C
1642 C
1643 C
1644 C
1645 C
1646 C
1647 C
1648 C
1649 C
1650 C
1651 C
1652 C
1653 C
1654 C
1655 C
1656 C
1657 C
1658 C
1659 C
1660 C
1661 C
1662 C
1663 C
1664 C
1665 C
1666 C
1667 C
1668 C
1669 C
1670 C
1671 C
1672 C
1673 C
1674 C
1675 C
1676 C
1677 C
1678 C
1679 C
1680 C
1681 C
1682 C
1683 C
1684 C
1685 C
1686 C
1687 C
1688 C
1689 C
1690 C
1691 C
1692 C
1693 C
1694 C
1695 C
1696 C
1697 C
1698 C
1699 C
1700 C
1701 C
1702 C
1703 C
1704 C
1705 C
1706 C
1707 C
1708 C
1709 C
1710 C
1711 C
1712 C
1713 C
1714 C
1715 C
1716 C
1717 C
1718 C
1719 C
1720 C
1721 C
1722 C
1723 C
1724 C
1725 C
1726 C
1727 C
1728 C
1729 C
1730 C
1731 C
1732 C
1733 C
1734 C
1735 C
1736 C
1737 C
1738 C
1739 C
1740 C
1741 C
1742 C
1743 C
1744 C
1745 C
1746 C
1747 C
1748 C
1749 C
1750 C
1751 C
1752 C
1753 C
1754 C
1755 C
1756 C
1757 C
1758 C
1759 C
1760 C
1761 C
1762 C
1763 C
1764 C
1765 C
1766 C
1767 C
1768 C
1769 C
1770 C
1771 C
1772 C
1773 C
1774 C
1775 C
1776 C
1777 C
1778 C
1779 C
1780 C
1781 C
1782 C
1783 C
1784 C
1785 C
1786 C
1787 C
1788 C
1789 C
1790 C
1791 C
1792 C
1793 C
1794 C
1795 C
1796 C
1797 C
1798 C
1799 C
1800 C
1801 C
1802 C
1803 C
1804 C
1805 C
1806 C
1807 C
1808 C
1809 C
1810 C
1811 C
1812 C
1813 C
1814 C
1815 C
1816 C
1817 C
1818 C
1819 C
1820 C
1821 C
1822 C
1823 C
1824 C
1825 C
1826 C
1827 C
1828 C
1829 C
1830 C
1831 C
1832 C
1833 C
1834 C
1835 C
1836 C
1837 C
1838 C
1839 C
1840 C
1841 C
1842 C
1843 C
1844 C
1845 C
1846 C
1847 C
1848 C
1849 C
1850 C
1851 C
1852 C
1853 C
1854 C
1855 C
1856 C
1857 C
1858 C
1859 C
1860 C
1861 C
1862 C
1863 C
1864 C
1865 C
1866 C
1867 C
1868 C
1869 C
1870 C
1871 C
1872 C
1873 C
1874 C
1875 C
1876 C
1877 C
1878 C
1879 C
1880 C
1881 C
1882 C
1883 C
1884 C
1885 C
1886 C
1887 C
1888 C
1889 C
1890 C
1891 C
1892 C
1893 C
1894 C
1895 C
1896 C
1897 C
1898 C
1899 C
1900 C
1901 C
1902 C
1903 C
1904 C
1905 C
1906 C
1907 C
1908 C
1909 C
1910 C
1911 C
1912 C
1913 C
1914 C
1915 C
1916 C
1917 C
1918 C
1919 C
1920 C
1921 C
1922 C
1923 C
1924 C
1925 C
1926 C
1927 C
1928 C
1929 C
1930 C
1931 C
1932 C
1933 C
1934 C
1935 C
1936 C
1937 C
1938 C
1939 C
1940 C
1941 C
1942 C
1943 C
1944 C
1945 C
1946 C
1947 C
1948 C
1949 C
1950 C
1951 C
1952 C
1953 C
1954 C
1955 C
1956 C
1957 C
1958 C
1959 C
1960 C
1961 C
1962 C
1963 C
1964 C
1965 C
1966 C
1967 C
1968 C
1969 C
1970 C
1971 C
1972 C
1973 C
1974 C
1975 C
1976 C
1977 C
1978 C
1979 C
1980 C
1981 C
1982 C
1983 C
1984 C
1985 C
1986 C
1987 C
1988 C
1989 C
1990 C
1991 C
1992 C
1993 C
1994 C
1995 C
1996 C
1997 C
1998 C
1999 C
2000 C

```

1163	CALL WATRHU (Z*IWUN*MMUW)	NUCMUW	1164
1164	UU 7 I=1*8	NUCMUW	1165
1165	WIN(I)=WIN(I)+P*EX(I)*MMUW	NUCMUW	1166
1166	UU 8 IBAND=1*14	NUCMUW	1167
1167	ALAM=WAVEL(IBAND)	NUCMUW	1168
1168	CALL SCAT (Z*ALAM*V*SIG)	NUCMUW	1169
1169	SIGAVE(IBAND)=SIGAVE(IBAND)*SIG	NUCMUW	1170
1170	CALL UZAL (Z*AUAC)	NUCMUW	1171
1171	UU 9 I=1*4	NUCMUW	1172
1172	AUACAV(I)=AUACAV(I)*AUAC(I)	NUCMUW	1173
1173	CONTINUE	NUCMUW	1174
1174	CALL WCO2P (ZF1*ARG1*1)	NUCMUW	1175
1175	CALL WCO2P (ZF2*ARG2*1)	NUCMUW	1176
1176	WCO2=(ARG2-ARG1)/((ZF1-ZF2)*0.0005048)	NUCMUW	1177
1177	PAVE=PAVE/Z0*0	NUCMUW	1178
1178	UU 11 I=1*8	NUCMUW	1179
1179	W1*1(I)=WIN(I)/Z0*0	NUCMUW	1180
1180	UU 12 IBAND=1*14	NUCMUW	1181
1181	SIGAVE(IBAND)=SIGAVE(IBAND)/Z0*0	NUCMUW	1182
1182	UU 13 I=1*4	NUCMUW	1183
1183	AUACAV(I)=AUACAV(I)/Z0*0	NUCMUW	1184
1184	RETURN	NUCMUW	1185
1185	END	NUCMUW	1186



```

1186 FUNCTION FLUA(TT,IMARK)
1187
1188 *****
1189 *****
1190 *****
1191 *****
1192 *****
1193 *****
1194 *****
1195 *****
1196 *****
1197 *****
1198 *****
1199 *****
1200 *****
1201 *****
1202 *****
1203 *****
1204 *****
1205 *****
1206 *****
1207 *****
1208 *****
1209 *****
1210 *****
1211 *****
1212 *****
1213 *****
1214 *****
1215 *****
1216 *****
1217 *****
1218 *****
1219 *****
1220 *****
1221 *****
1222 *****
1223 *****
1224 *****
1225 *****
1226 *****
1227 *****
1228 *****
1229 *****
1230 *****
1231 *****
1232 *****
1233 *****
1234 *****
1235 *****
1236 *****

```

AFEL INTERNAL POWER TIME HISTORY FUNCTION

CALLING SEQUENCE

FLUA(=SIGMA,TT,IMST)

#YIELD (KILOTONS)

SIGMA=DENSITY RATIO AT BURST ALTITUDE (NHUA/NHUSL)

TT=TIME WHERE POWER IS DESIRED (SEC)

FLUA=POWER (WATTS)

ROUTINE BY ALFRED L. SHARP - 7 NOVEMBER 1972.

\*\*\*\*\*

COMMON /SNCM3/ UT, N, SIGMA, TMAX

IF (IMARK,UT,0) GO TO 30

IF (SIGMA,LT,0.0008) GO TO 90

S=1.75995\*SIGMA\*\*(-.0432)

PSCM=.17214\*SIGMA\*\*(-.6244)\*#\*\*53

SIGLOG=ALOG(SIGMA)

TSEM=(1.6828E-4\*SIGLOG\*(-1.62326E-6\*SIGLOG\*(-3.72132E-6-SIGLOG

+1.51933E-7)))\*#\*\*3123

BHM=2.\*SIGMA\*\*1008

BML=SIGMA\*\*1109

TMAX=.036\*#\*\*44\*SIGMA\*\*(.36)

TMIN=.00256\*#\*\*39\*SIGMA\*\*(-.062)

UT=(TMAX/TMIN)\*\*.01

IF (TMIN\*.61\*.99\*TMAX) TMIN=.99\*TMAX

PMAX=1.49E13\*#\*\*59\*SIGMA\*\*(-.45)

PMIN=6.82E11\*#\*\*54\*SIGMA\*\*(-1.02)

IF (PMIN\*.6E\*.99\*PMAX) PMIN=.99\*PMAX

BSEM=PSCM/PMIN-1.

BHR=3.4071\*SIGMA\*\*17827

BHL=9.83382\*SIGLOG\*(-.45\*SIGLOG\*(-.207-SIGLOG\*.007741))

BTIME=1.523\*SIGMA\*\*(-.0752)\*TMAX

BHITE=1./(.8\*SIGMA\*\*3372)-1.

C=(ALOG(TMAX)-ALOG(TMIN))\*TMAX/(TMAX-TMIN)

B=5\*EXP(C)/C

TM=TMIN/TMAX

HINTMR=PMIN/(TM\*\*(-5)\*EXP(-B\*EXP(-C\*TR)))

PAGE 40

```

1236 MINITMA=PMAX/(EXP(-B*EXP(-C)))
1237 ALPH=-.0209***.3209+1.023***(-.0013979)
1238 C
1239 30 TSMAX=TT/TMAX
1240 IF (TT.EU.0.) GO TO 100
1241 IF (TT.LT.TMIN) GO TO 50
1242 IF (TSMAX-1.) 40+60*60
1243 TETA=(1.-ALOU(1./TSMAX))/ALOU(1./TH)
1244 TETAB=3.14159265359*TETA
1245 MINT=MINTMX*(MINTMN-MINTMX)*((1.-COS(TETAB))/2.)*ALPH
1246 GO TO 70
1247 50 FAC=2.*BHITC/((BTIME/TT)*BNL*(TT/BTIME)*BNK)
1248 PFAC=1./(FAC*1.)
1249 FACM=(2.*BSEM/((TSEM/TT)*BNL*(TT/TSEM)*BNK))*1.
1250 FLUX=PMIN*FAC*FACM
1251 GO TO 80
1252 60 MINT=MINTMX
1253 FAC=2.*BHITC/((BTIME/TT)*BNL*(TT/BTIME)*BNK)
1254 PFAC=1./(FAC*1.)
1255 FACM=(2.*BSEM/((TSEM/TT)*BNL*(TT/TSEM)*BNK))*1.
1256 FLUX=MINT*(TSMAX**(-5)*EXP(-B*EXP(-C*TSMAX)))*PFAC*FACM
1257 RETURN
1258 C
1259 90 CALL NUCENR(BFLUX *1)
1260 RETURN
1261 C
1262 100 FLUX=PMIN
1263 RETURN
1264 END

```

NUCMUU 1237  
 NUCMUU 1238  
 NUCMUU 1239  
 NUCMUU 1240  
 NUCMUU 1241  
 NUCMUU 1242  
 NUCMUU 1243  
 NUCMUU 1244  
 NUCMUU 1245  
 NUCMUU 1246  
 NUCMUU 1247  
 NUCMUU 1248  
 NUCMUU 1249  
 NUCMUU 1250  
 NUCMUU 1251  
 NUCMUU 1252  
 NUCMUU 1253  
 NUCMUU 1254  
 NUCMUU 1255  
 NUCMUU 1256  
 NUCMUU 1257  
 NUCMUU 1258  
 NUCMUU 1259  
 NUCMUU 1260  
 NUCMUU 1261  
 NUCMUU 1262  
 NUCMUU 1263  
 NUCMUU 1264  
 NUCMUU 1265

1265	C	SUBROUTINE UZAC (ZP, AUAC)	NUCMUO	1266
1266	C	COMPUTES OZONE ABSORPTION COEFFICIENT IN KM-1	NUCMUO	1267
1267	C	ZP IS ALTITUDE IN FEET.	NUCMUO	1268
1268	C	AUAC IS THE RETURNED ATMOSPHERIC OZONE ABSORPTION COEFFICIENT.	NUCMUO	1269
1269	C		NUCMUO	1270
1270	C		NUCMUO	1271
1271	C	DIMENSION AUAC(4), A(4), MU(26), UT(26)	NUCMUO	1272
1272	C		NUCMUO	1273
1273	C	DATA A/210.0,101.0,0.0,0.34,0.0177,MU/0.0,0.4,0.6,0.8,0.10,0.0,11.0,0.12,0.0,	NUCMUO	1274
1274	C	113.0,14.0,0.15,0.16,0.17,0.18,0.21,0.22,0.23,0.24,0.25,0.30,0.32,0.3	NUCMUO	1275
1275	C	24.0,0.38,0.42,0.44,0.47,0.50,0.017,0.03356,0.00226,0.00216,0.00228,0	NUCMUO	1276
1276	C	3.0035,0.0046,0.00621,0.00845,0.00957,0.00994,0.0103,0.0111,0.0122,	NUCMUO	1277
1277	C	40.0184,0.0197,0.0198,0.0193,0.0180,0.00903,0.00682,0.00465,0.00253	NUCMUO	1278
1278	C	5.0,0.00126,0.000919,0.000798,0.000667	NUCMUO	1279
1279	C		NUCMUO	1280
1280	C	Z=ZF*0.00030*0	NUCMUO	1281
1281	C	CALL INT1 (Z,26,MU,UT,U)	NUCMUO	1282
1282	C	DO 1 I=1,4	NUCMUO	1283
1283	C	AUAC(I)=U*A(I)	NUCMUO	1284
1284	C	RETURN	NUCMUO	1285
1285	C	END	NUCMUO	1286

LINE	NO	STATEMENT	ADDRESS	DISC	REL	DATE
1286	C	FUNCTION=POWER(TIME*IMARK)	1287			
1287	C	COMMON, /SACM, /	1288			
1288	C	DATA 4/1.0E-6/	1289			
1289	C	IF (IMARK.GT.0.0) GO TO 10	1290			
1290	C	PI = 3.141592653589793	1291			
1291	C	ALUT=ALUT(IUT)	1292			
1292	C	POWER=DE-0PMU	1293			
1293	C	POWER=0.	1294			
1294	C	I=1	1295			
1295	C	ISTEP=TIME/C.	1296			
1296	C	RETURN	1297			
1297	C	IF (I-1) 1,1,0	1298			
1298	C	POWER=POWER	1299			
1299	C	PLAST=PI	1300			
1300	C	ISTART=A	1301			
1301	C	I=2	1302			
1302	C	GO TO 3	1303			
1303	C	POWER=0.	1304			
1304	C	ISTART=ISTART	1305			
1305	C	PLUG=ALUT(ISTART/ISTART)	1306			
1306	C	ALUT=ALUT	1307			
1307	C	IF (N*LT.1) N=1	1308			
1308	C	ALUT=EXP(PLUG/PLUG(N))	1309			
1309	C	PLAST=ISTART	1310			
1310	C	GO 4 J=1,N	1311			
1311	C	T=PLAST*AMULT	1312			
1312	C	POWER=POWER*(P+PLAST)*(T-PLAST)	1313			
1313	C	PLAST=T	1314			
1314	C	PLAST=PI	1315			
1315	C	POWER=POWER	1316			
1316	C	PLAST=PI	1317			
1317	C	POWER=POWER	1318			
1318	C	PLAST=PI	1319			
1319	C	POWER=POWER	1320			
1320	C	PLAST=PI	1321			
1321	C	POWER=POWER	1322			
1322	C	PLAST=PI	1323			
1323	C	POWER=POWER	1324			
1324	C	PLAST=PI	1325			
1325	C	POWER=POWER	1326			
1326	C	PLAST=PI	1327			
1327	C	POWER=POWER	1328			
1328	C	PLAST=PI	1329			
1329	C	POWER=POWER	1330			
1330	C	PLAST=PI	1331			
1331	C	POWER=POWER	1332			
1332	C	PLAST=PI	1333			
1333	C	POWER=POWER	1334			
1334	C	PLAST=PI	1335			
1335	C	POWER=POWER	1336			
1336	C	PLAST=PI	1337			
1337	C	POWER=POWER	1338			
1338	C	PLAST=PI	1339			
1339	C	POWER=POWER	1340			
1340	C	PLAST=PI	1341			
1341	C	POWER=POWER	1342			
1342	C	PLAST=PI	1343			
1343	C	POWER=POWER	1344			
1344	C	PLAST=PI	1345			
1345	C	POWER=POWER	1346			
1346	C	PLAST=PI	1347			
1347	C	POWER=POWER	1348			
1348	C	PLAST=PI	1349			
1349	C	POWER=POWER	1350			
1350	C	PLAST=PI	1351			
1351	C	POWER=POWER	1352			
1352	C	PLAST=PI	1353			
1353	C	POWER=POWER	1354			
1354	C	PLAST=PI	1355			
1355	C	POWER=POWER	1356			
1356	C	PLAST=PI	1357			
1357	C	POWER=POWER	1358			
1358	C	PLAST=PI	1359			
1359	C	POWER=POWER	1360			
1360	C	PLAST=PI	1361			
1361	C	POWER=POWER	1362			
1362	C	PLAST=PI	1363			
1363	C	POWER=POWER	1364			
1364	C	PLAST=PI	1365			
1365	C	POWER				

1329	DATA AAAA/	1.00000E+00	2.00000E+00	3.00000E+00	4.00000E+00	NUCMUU	1329
1330	DATA AAAA/	5.00000E+00	6.00000E+00	7.00000E+00	8.00000E+00	NUCMUU	1330
1331	DATA AAAA/	1.00000E+01	1.50000E+01	2.00000E+01	2.50000E+01	NUCMUU	1331
1332	DATA AAAA/	3.00000E+01	3.50000E+01	4.00000E+01	4.50000E+01	NUCMUU	1332
1333	DATA AAAA/	6.00000E+01	6.50000E+01	7.00000E+01	7.50000E+01	NUCMUU	1333
1334	DATA AAAA/	1.00000E+02	1.50000E+02	2.00000E+02	2.50000E+02	NUCMUU	1334
1335	DATA AAAA/	5.00000E+02	5.50000E+02	6.00000E+02	6.50000E+02	NUCMUU	1335
1336	DATA AAAA/	1.00000E+03	1.50000E+03	2.00000E+03	2.50000E+03	NUCMUU	1336
1337	DATA AAAA/	3.00000E+03	3.50000E+03	4.00000E+03	4.50000E+03	NUCMUU	1337
1338	DATA AAAA/	6.00000E+03	6.50000E+03	7.00000E+03	7.50000E+03	NUCMUU	1338
1339	DATA AAAA/	1.00000E+04	1.50000E+04	2.00000E+04	2.50000E+04	NUCMUU	1339
1340	DATA AAAA/	3.00000E+04	3.50000E+04	4.00000E+04	4.50000E+04	NUCMUU	1340
1341	DATA AAAA/	6.00000E+04	6.50000E+04	7.00000E+04	7.50000E+04	NUCMUU	1341
1342	DATA AAAA/	1.00000E+05	1.50000E+05	2.00000E+05	2.50000E+05	NUCMUU	1342
1343	DATA AAAA/	3.00000E+05	3.50000E+05	4.00000E+05	4.50000E+05	NUCMUU	1343
1344	DATA AAAA/	6.00000E+05	6.50000E+05	7.00000E+05	7.50000E+05	NUCMUU	1344
1345	DATA AAAA/	1.00000E+06	1.50000E+06	2.00000E+06	2.50000E+06	NUCMUU	1345
1346	DATA AAAA/	3.00000E+06	3.50000E+06	4.00000E+06	4.50000E+06	NUCMUU	1346
1347	DATA AAAA/	6.00000E+06	6.50000E+06	7.00000E+06	7.50000E+06	NUCMUU	1347
1348	DATA AAAA/	1.00000E+07	1.50000E+07	2.00000E+07	2.50000E+07	NUCMUU	1348
1349	DATA AAAA/	3.00000E+07	3.50000E+07	4.00000E+07	4.50000E+07	NUCMUU	1349
1350	DATA AAAA/	6.00000E+07	6.50000E+07	7.00000E+07	7.50000E+07	NUCMUU	1350
1351	DATA AAAA/	1.00000E+08	1.50000E+08	2.00000E+08	2.50000E+08	NUCMUU	1351
1352	DATA AAAA/	3.00000E+08	3.50000E+08	4.00000E+08	4.50000E+08	NUCMUU	1352
1353	DATA AAAA/	6.00000E+08	6.50000E+08	7.00000E+08	7.50000E+08	NUCMUU	1353
1354	DATA AAAA/	1.00000E+09	1.50000E+09	2.00000E+09	2.50000E+09	NUCMUU	1354
1355	DATA AAAA/	3.00000E+09	3.50000E+09	4.00000E+09	4.50000E+09	NUCMUU	1355
1356	DATA AAAA/	6.00000E+09	6.50000E+09	7.00000E+09	7.50000E+09	NUCMUU	1356
1357	DATA AAAA/	1.00000E+10	1.50000E+10	2.00000E+10	2.50000E+10	NUCMUU	1357
1358	DATA AAAA/	3.00000E+10	3.50000E+10	4.00000E+10	4.50000E+10	NUCMUU	1358
1359	DATA AAAA/	6.00000E+10	6.50000E+10	7.00000E+10	7.50000E+10	NUCMUU	1359
1360	DATA AAAA/	1.00000E+11	1.50000E+11	2.00000E+11	2.50000E+11	NUCMUU	1360
1361	DATA AAAA/	3.00000E+11	3.50000E+11	4.00000E+11	4.50000E+11	NUCMUU	1361
1362	DATA AAAA/	6.00000E+11	6.50000E+11	7.00000E+11	7.50000E+11	NUCMUU	1362
1363	DATA AAAA/	1.00000E+12	1.50000E+12	2.00000E+12	2.50000E+12	NUCMUU	1363
1364	DATA AAAA/	3.00000E+12	3.50000E+12	4.00000E+12	4.50000E+12	NUCMUU	1364
1365	DATA AAAA/	6.00000E+12	6.50000E+12	7.00000E+12	7.50000E+12	NUCMUU	1365
1366	DATA AAAA/	1.00000E+13	1.50000E+13	2.00000E+13	2.50000E+13	NUCMUU	1366
1367	DATA AAAA/	3.00000E+13	3.50000E+13	4.00000E+13	4.50000E+13	NUCMUU	1367
1368	DATA AAAA/	6.00000E+13	6.50000E+13	7.00000E+13	7.50000E+13	NUCMUU	1368
1369	DATA AAAA/	1.00000E+14	1.50000E+14	2.00000E+14	2.50000E+14	NUCMUU	1369
1370	DATA AAAA/	3.00000E+14	3.50000E+14	4.00000E+14	4.50000E+14	NUCMUU	1370
1371	DATA AAAA/	6.00000E+14	6.50000E+14	7.00000E+14	7.50000E+14	NUCMUU	1371
1372	DATA AAAA/	1.00000E+15	1.50000E+15	2.00000E+15	2.50000E+15	NUCMUU	1372
1373	DATA AAAA/	3.00000E+15	3.50000E+15	4.00000E+15	4.50000E+15	NUCMUU	1373
1374	DATA AAAA/	6.00000E+15	6.50000E+15	7.00000E+15	7.50000E+15	NUCMUU	1374
1375	DATA AAAA/	1.00000E+16	1.50000E+16	2.00000E+16	2.50000E+16	NUCMUU	1375
1376	DATA AAAA/	3.00000E+16	3.50000E+16	4.00000E+16	4.50000E+16	NUCMUU	1376
1377	DATA AAAA/	6.00000E+16	6.50000E+16	7.00000E+16	7.50000E+16	NUCMUU	1377

1376	3	1.24900E-01	1.24900E-01	1.34900E-01	1.44600E-01	1.54900E-01	NUL
1379	3	1.76500E-01	2.4900E-01	3.44600E-01	4.55000E-01	5.67400E-01	NUL
1380	3	6.32770E-01	1.0660E+00	1.13300E+00	1.24400E+00	1.40900E+00	NUL
1381	DATA(1222(1),1)=163.2417						
1382	3	1.52000E+00	1.6000E+00	1.66300E+00	1.72100E+00	1.76000E+00	NUL
1383	3	1.76600E+00					NUL
1384	3	7.75000E-02	1.0000E-01	1.09500E-01	1.15000E-01	1.23700E-01	NUL
1385	3	1.44500E-01	1.82000E-01	2.62000E-01	3.53600E-01	5.45700E-01	NUL
1386	3	7.2790E-01	8.94100E-01	1.02200E+00	1.14000E+00	1.32100E+00	NUL
1387	3	1.44100E+00	1.54700E+00	1.62100E+00	1.69900E+00	1.73500E+00	NUL
1388	3	1.74500E+00					NUL
1389	3	8.30000E-02	8.9000E-02	9.10000E-02	1.00000E-01	1.00000E-01	NUL
1390	3	1.17000E-01	1.43000E-01	2.05000E-01	2.78000E-01	4.41000E-01	NUL
1391	3	8.10000E-01	7.84000E-01	9.08000E-01	1.02800E+00	1.22800E+00	NUL
1392	3	1.37600E+00	1.47800E+00	1.56200E+00	1.64900E+00	1.70100E+00	NUL
1393	3	7.12000E-02	7.60000E-02	8.00000E-02	8.40000E-02	8.40000E-02	NUL
1394	3	5.217300E-01	6.65400E-01	8.00000E-01	9.24400E-01	1.13100E+00	NUL
1395	3	1.24800E+00	1.46100E+00	1.50300E+00	1.60000E+00	1.66300E+00	NUL
1396	3	1.663E+00					NUL
1397	3	6.24000E-02	7.80000E-02	9.50000E-02	1.18500E-01	1.20000E-01	NUL
1398	3	5.17300E-01	6.65400E-01	8.00000E-01	9.24400E-01	1.13100E+00	NUL
1399	DATA(1222(1),1)=242.32017						
1400	3	4.39000E-01	5.71000E-01	7.08000E-01	8.33000E-01	1.04900E+00	NUL
1401	3	1.20300E+00	1.32900E+00	1.43200E+00	1.54300E+00	1.61700E+00	NUL
1402	3	5.56000E-02	6.38000E-02	7.15300E-01	8.55800E-01	2.60000E-01	NUL
1403	3	3.74500E-01	4.98000E-01	5.20600E-01	7.38300E-01	9.46700E-01	NUL
1404	3	1.12000E+00	1.25200E+00	1.37000E+00	1.48100E+00	1.56700E+00	NUL
1405	3	1.56700E+00					NUL
1406	3	4.75000E-02	7.25000E-02	9.90000E-02	1.31000E-01	2.19000E-01	NUL
1407	3	3.21000E-02	4.32000E-01	5.50000E-01	6.76000E-01	8.61000E-01	NUL
1408	3	1.04000E+00	1.18100E+00	1.30000E+00	1.43700E+00	1.51600E+00	NUL
1409	3	1.51600E+00					NUL
1410	3	4.54000E-02	6.46000E-02	8.62000E-02	1.14800E-01	1.89500E-01	NUL
1411	3	2.79900E-01	3.80200E-01	4.88000E-01	5.89800E-01	7.87400E-01	NUL
1412	3	1.11800E-01	1.23300E+00	1.35900E+00	1.48300E+00	1.48300E+00	NUL
1413	3	4.54000E-02	6.46000E-02	8.62000E-02	1.14800E-01	1.89500E-01	NUL
1414	3	2.79900E-01	3.80200E-01	4.88000E-01	5.89800E-01	7.87400E-01	NUL
1415	3	1.11800E-01	1.23300E+00	1.35900E+00	1.48300E+00	1.48300E+00	NUL
1416	3	4.54000E-02	6.46000E-02	8.62000E-02	1.14800E-01	1.89500E-01	NUL
1417	3	2.79900E-01	3.80200E-01	4.88000E-01	5.89800E-01	7.87400E-01	NUL
1418	3	1.11800E-01	1.23300E+00	1.35900E+00	1.48300E+00	1.48300E+00	NUL
1419	3	4.54000E-02	6.46000E-02	8.62000E-02	1.14800E-01	1.89500E-01	NUL
1420	3	3.84000E-02	3.90000E-02	4.06000E-02	4.10000E-02	4.30000E-02	NUL
1421	DATA(1222(1),1)=321.40317						
1422	3	4.60000E-02	5.60000E-02	6.70000E-02	8.90000E-02	1.42000E-01	NUL
1423	3	2.18000E-01	2.99000E-01	3.88000E-01	4.82000E-01	6.52000E-01	NUL
1424	3	8.26000E-01	9.53000E-01	1.09000E+00	1.23800E+00	1.32600E+00	NUL
1425	3	1.35200E+00					NUL
1426	3	3.33000E-02	4.37000E-02	5.58000E-02	7.17000E-02	1.15600E-01	NUL
1427	3	3.93000E-02	5.00000E-02	6.30000E-02	7.90000E-02	1.15600E-01	NUL

PAGE 42

```
1429 1.71400E-01, 2.37200E-01, 3.08000E-01, 3.88100E-01, 5.48500E-01, 1429
1429 7.04200E-01, 8.22000E-01, 9.81500E-01, 1.12300E+00, 1.24100E+00, 1430
1430 1.24100E+00, 2.88000E-02, 2.88000E-02, 2.88000E-02, 2.90000E-02, 1432
1432 2.88000E-02, 3.86000E-02, 4.10000E-02, 5.80000E-02, 9.00000E-02, 1433
1433 3.30000E-02, 1.90000E-01, 2.52000E-01, 3.18000E-01, 4.57000E-01, 1434
1434 1.32000E-01, 1.90000E-01, 2.52000E-01, 3.18000E-01, 4.57000E-01, 1435
1435 6.03000E-01, 7.23000E-01, 8.48000E-01, 9.95000E-01, 1.11000E+00, 1436
1436 1.11000E+00, 2.50000E-02, 2.50000E-02, 2.50000E-02, 2.50000E-02, 1437
1437 2.50000E-02, 3.08000E-02, 3.76000E-02, 4.70000E-02, 7.24000E-02, 1438
1438 3.08000E-02, 1.47700E-01, 1.92000E-01, 2.47900E-01, 3.63000E-01, 1439
1439 1.08900E-01, 6.09000E-01, 7.29300E-01, 8.70000E-01, 1.00100E+00, 1440
1440 4.85500E-01, 1.00100E+00, 2.50000E-02, 2.50000E-02, 2.50000E-02, 1441
1441 1.00100E+00, 2.50000E-02, 2.50000E-02, 2.50000E-02, 2.50000E-02, 1442
1442 2.50000E-02, 3.08000E-02, 3.76000E-02, 4.70000E-02, 7.24000E-02, 1443
1443 3.08000E-02, 1.47700E-01, 1.92000E-01, 2.47900E-01, 3.63000E-01, 1444
1444 1.08900E-01, 6.09000E-01, 7.29300E-01, 8.70000E-01, 1.00100E+00, 1445
1445 4.85500E-01, 1.00100E+00, 2.50000E-02, 2.50000E-02, 2.50000E-02, 1446
1446 1.00100E+00, 2.50000E-02, 2.50000E-02, 2.50000E-02, 2.50000E-02, 1447
1447 2.50000E-02, 3.08000E-02, 3.76000E-02, 4.70000E-02, 7.24000E-02, 1448
1448 3.08000E-02, 1.47700E-01, 1.92000E-01, 2.47900E-01, 3.63000E-01, 1449
1449 1.08900E-01, 6.09000E-01, 7.29300E-01, 8.70000E-01, 1.00100E+00, 1450
1450 4.85500E-01, 1.00100E+00, 2.50000E-02, 2.50000E-02, 2.50000E-02, 1451
1451 1.00100E+00, 2.50000E-02, 2.50000E-02, 2.50000E-02, 2.50000E-02, 1452
1452 2.50000E-02, 3.08000E-02, 3.76000E-02, 4.70000E-02, 7.24000E-02, 1453
1453 3.08000E-02, 1.47700E-01, 1.92000E-01, 2.47900E-01, 3.63000E-01, 1454
1454 1.08900E-01, 6.09000E-01, 7.29300E-01, 8.70000E-01, 1.00100E+00, 1455
1455 4.85500E-01, 1.00100E+00, 2.50000E-02, 2.50000E-02, 2.50000E-02, 1456
1456 1.00100E+00, 2.50000E-02, 2.50000E-02, 2.50000E-02, 2.50000E-02, 1457
1457 2.50000E-02, 3.08000E-02, 3.76000E-02, 4.70000E-02, 7.24000E-02, 1458
1458 3.08000E-02, 1.47700E-01, 1.92000E-01, 2.47900E-01, 3.63000E-01, 1459
1459 1.08900E-01, 6.09000E-01, 7.29300E-01, 8.70000E-01, 1.00100E+00, 1460
```

```
DATA(1:222(1),1)=404.420/
2.61000E-02,
2.61000E-02,
2.61000E-02,
1.00100E+00,
1.00100E+00/

X1=0
IF (X1.GT.1.0) X1=1.0
IF (X1.LT.0.0) X1=-1.0
AC=M
IF (X2.GT.1.0) X2=1.0
IF (X2.LT.0.0) X2=-1.0
CALL UNIT(XXXX,YYYY,ZZZ,Z1,Z2,X1,X2,MM)
WRITE(1)
END
```

1459 46

```

1459 C SUBROUTINE DIM1 (XX,YY,ZZ,M,N,AA,Y,Z)
1460 C LINEAR 2 DIMENSIONAL INTERPOLATION
1461 C EXAMPLE-GIVEN THE FOLLOWING TABLE AND A AND Y VALUES,WE CAN
1462 C INTERPOLATE FOR APPROPRIATE Z VALUE
1463 C XX AND YY MUST BE IN INCREASING ORDER
1464 C X1 X2 X3
1465 C Y1 Z1 Z2 Z3
1466 C Y2 Z4 Z5 Z6
1467 C Y3 Z7 Z8 Z9
1468 C DIMENSION AA(N), YY(M), ZZ(M,N)
1469 C IF ((X-XT.XX(1)).OR.(X-XT.XX(N)).OR.((Y-LT.YY(1)).OR.(Y-UT.YY(M)
1470 C 1))) GO TO 70
1471 C WHEN=1
1472 C WHEN=1
1473 C GO TO 1=1,MM
1474 C IF ((YY(1).LE.Y).AND.(YY(1+1).GT.Y)) GO TO 10
1475 C GO TO 20
1476 C C1=(Y-YY(1))/(YY(1+1)-YY(1))
1477 C I1=1
1478 C I2=1+1
1479 C GO TO 30
1480 C CONTINUE
1481 C GO 50 J=1,NN
1482 C IF ((XX(J).LE.X).AND.(XX(J+1).GT.X)) GO TO 40
1483 C GO TO 50
1484 C C2=(X-XX(J))/(XX(J+1)-XX(J))
1485 C J1=J
1486 C J2=J+1
1487 C GO TO 60
1488 C CONTINUE
1489 C CONTINUE
1490 C Z1=ZZ(I1+J1)*C1*(ZZ(I2+J1)-ZZ(I1+J1))
1491 C Z2=ZZ(I1+J2)*C1*(ZZ(I2+J2)-ZZ(I1+J2))
1492 C Z=Z1+C2*(Z2-Z1)
1493 C RETURN
1494 C WRITE (6,Y0) A,Y
1495 C CALL NUCHEM(OMU,INT ,1)
1496 C RETURN
1497 C
1498 C
1499 C
1500 C FORMAT (1H1,COMPARAMETER OUTSIDE RANGE,X=E15.8,ZX,ZHY=E15.8)
1501 C ENU

```

1460 NUCMOD  
 1461 NUCMOD  
 1462 NUCMOD  
 1463 NUCMOD  
 1464 NUCMOD  
 1465 NUCMOD  
 1466 NUCMOD  
 1467 NUCMOD  
 1468 NUCMOD  
 1469 NUCMOD  
 1470 NUCMOD  
 1471 NUCMOD  
 1472 NUCMOD  
 1473 NUCMOD  
 1474 NUCMOD  
 1475 NUCMOD  
 1476 NUCMOD  
 1477 NUCMOD  
 1478 NUCMOD  
 1479 NUCMOD  
 1480 NUCMOD  
 1481 NUCMOD  
 1482 NUCMOD  
 1483 NUCMOD  
 1484 NUCMOD  
 1485 NUCMOD  
 1486 NUCMOD  
 1487 NUCMOD  
 1488 NUCMOD  
 1489 NUCMOD  
 1490 NUCMOD  
 1491 NUCMOD  
 1492 NUCMOD  
 1493 NUCMOD  
 1494 NUCMOD  
 1495 NUCMOD  
 1496 NUCMOD  
 1497 NUCMOD  
 1498 NUCMOD  
 1499 NUCMOD  
 1500 NUCMOD  
 1501 NUCMOD  
 1502 NUCMOD



```

1502 C SUBROUTINE SCAT (ZF,ALAM,V,SIG)
1503 C
1504 C SUBROUTINE SCAT COMPUTES THE SCATTERING COEFFICIENT, KM-1.
1505 C ZF IS THE ALTITUDE IN FEET.
1506 C ALAM IS THE WAVELENGTH IN MICRONS.
1507 C V IS THE SURFACE VISUAL RANGE IN MILES.
1508 C SIG IS THE RETURNED SCATTERING COEFFICIENT, KM-1.
1509 C
1510 C DIMENSION AS(4), AL(4), ES(4), EL(4), VIS(4)
1511 C
1512 C DATA AS/1.22*0.244*0.0486*0.0132/
1513 C DATA AL/0.168*0.0777*0.0361*0.0132/
1514 C DATA ES/-0.033*-0.324*-0.221*-0.0920/
1515 C DATA EL/-0.173*-0.147*-0.122*-0.0920/
1516 C DATA VIS/2.0*10.0*50.0*100.0/
1517 C
1518 C V=MAX1(V,2.0)
1519 C V=MIN1(V,100.0)
1520 C Z=ZF*0.003048
1521 C AM=0.11*Z*0.70
1522 C AMU=(0.55/ALAM)*AM
1523 C DO I=1,4
1524 C IF (V*EL*VIS(I)*1) GO TO 2
1525 C GO TO 3
1526 C I=3
1527 C IF (Z*3.0) GO TO 3
1528 C SIG1=AS(I)*AMU*EXP(ES(I)*Z)
1529 C SIG2=AS(I)*AMU*EXP(ES(I)*V*7)
1530 C GO TO 4
1531 C SIG1=AL(I)*AMU*EXP(EL(I)*Z)
1532 C SIG2=AL(I)*AMU*EXP(EL(I)*V*2)
1533 C SIG=SIG1*(SIG2-SIG1)*(V-VIS(I))/(VIS(I)-VIS(I))
1534 C RETURN
1535 C END

```

1503 NUCMOD  
 1504 NUCMOD  
 1505 NUCMOD  
 1506 NUCMOD  
 1507 NUCMOD  
 1508 NUCMOD  
 1509 NUCMOD  
 1510 NUCMOD  
 1511 NUCMOD  
 1512 NUCMOD  
 1513 NUCMOD  
 1514 NUCMOD  
 1515 NUCMOD  
 1516 NUCMOD  
 1517 NUCMOD  
 1518 NUCMOD  
 1519 NUCMOD  
 1520 NUCMOD  
 1521 NUCMOD  
 1522 NUCMOD  
 1523 NUCMOD  
 1524 NUCMOD  
 1525 NUCMOD  
 1526 NUCMOD  
 1527 NUCMOD  
 1528 NUCMOD  
 1529 NUCMOD  
 1530 NUCMOD  
 1531 NUCMOD  
 1532 NUCMOD  
 1533 NUCMOD  
 1534 NUCMOD  
 1535 NUCMOD  
 1536 NUCMOD

PAGE 48

```

1536 C SUBROUTINE TC02(FLAG)
1537 C
1538 C
1539 C
1540 C
1541 C
1542 C
1543 C
1544 C
1545 C
1546 C
1547 C
1548 C
1549 C
1550 C
1551 C
1552 C
1553 C
1554 C
1555 C
1556 C
1557 C
1558 C
1559 C
1560 C
1561 C
1562 C
1563 C
1564 C
1565 C
1566 C
1567 C
1568 C
1569 C
1570 C
1571 C
1572 C
1573 C
1574 C
1575 C
1576 C
1577 C
1578 C
1579 C
1580 C
1581 C
1582 C

```

COMMON /SNLM2/ AGACAV(14), DKM,  
 TCUM(14), TDIF(14), TOZ(14),  
 TWATW(14), WCU2, WIN(B)

COMMON /SNLM4/ PAVE

DIMENSION C(4), IUSE(4), C2(4), C3(4), C4(4), U(4),  
 C1(4), IUSE(4), C2(4), C3(4), C4(4), U(4),  
 UATA IUSE/9.10,11.13,CUNST/.43429440/  
 UATA C/.050.063.0492.3.15/  
 UATA AK/.41.0.38.0.39.0.43/  
 UATA ALIM/3.00.0.50.0.  
 UATA CC/6.0.0.0.536.0.137.0.  
 UATA DELNU/1500.0.550.0.1100.0.1060.0.  
 UATA AKK/0.0.0.0.114.0.62.0.  
 UATA U70.0.0.138.0.77.0.

IF (IFLAG .GT. 0) GO TO 10  
 PALUG=ALUG(PAVE)  
 DO 1 I=1,4  
 C1(I)=C(I)\*EXP(PALUG\*DK(I))  
 C2(I)=C(I)\*CUNST  
 C3(I)=AKK(I)\*CUNST\*PALUG+C1(I)  
 C4(I)=1.0/DELNU(I)  
 CONTINUE  
 RETURN

CONTINUE  
 DO 2 I=1,4  
 AKK=WC02\*DKM  
 WSK=SUMT(WKK)  
 AIN=C1(I)\*WSK  
 IF (AIN.LE.ALIM(I)) GO TO 3  
 IF (C1(I) .GT. 3.0) GO TO 3  
 AIN=C2(I)\*ALUG(WKK)+C3(I)  
 AIN=AMAX1(AIN,ALIM(I))  
 TCU=1.-AIN\*C4(I)  
 IF (TCU) 4,5,5  
 TCU=0.  
 J=IUSE(I)  
 TCUM(J)=TCU  
 CONTINUE  
 RETURN  
 END

```

1583 SUBROUTINE TUIFFS(IFLAG)
1584
1585
1586
1587
1588
1589
1590
1591
1592
1593
1594
1595
1596
1597
1598
1599
1600
1601
1602
1603
1604
1605
1606
1607
1608
1609

```

SUBROUTINE TUIFFS(IFLAG)  
 SUBROUTINE TUIFFS COMPUTES THE DIFFUSE SCATTERING FUNCTION, TUIFF.  
 RF IS THE RANGE FROM THE SOURCE TO THE RECEIVER IN FEET.  
 SIGAVE IS THE SCATTERING COEFFICIENT, KM-1.  
 TUIF IS THE RETURNED DIFFUSE SCATTERING FUNCTION.  
 COMMON /SNCM2/ AUCAV(14), UKM, SIGAVE(14),  
 \* TCOW(14), TUIF(14), TUZ(14), THWL(14),  
 \* TWAIV(14), WCUZ, WJIN(8)  
 DIMENSION SMCBRT(14),P6SURT(14)  
 IF (IFLAG .GT. 0) GO TO 10  
 DO 1 IBAND=1,14  
 S=SIGAVE(IBAND)  
 SMCBRT(IBAND)=S\*S\*.3333333333  
 P6SURT(IBAND)=S\*.6\*SURT(S)  
 RETURN  
 CONTINUE  
 DO 2 IBAND=1,14  
 TUIF(IBAND)=EXP(-SIGAVE(IBAND)\*UKM)\*(1.+P6SURT(IBAND)\*UKM\*EXP(SMCE  
 \*RT(IBAND)\*UKM))  
 RETURN  
 END

1000 50

SUBROUTINE TUZONE

COMPUTES OZONE ABSORPTION FACTOR.  
 IF IS THE RANGE FROM THE SOURCE TO THE RECEIVER IN FEET.  
 AUACAV IS THE OZONE ABSORPTION COEFFICIENT IN KM-1.  
 TLZ IS THE RETURNED OZONE TRANSMITTANCE FACTOR.

COMMON /SRUMCZ/ AUACAV(14), UKM, SIGAVE(14),  
 \* TCOM(14), TUIF(14), THWL(14),  
 \* TATW(14), WJ(18)

DO 1 I=1,4  
 TUZ(I)=EXP(-AUACAV(I)\*UKM)  
 RETURN  
 END

NUCMU 1610  
 NUCMU 1611  
 NUCMU 1612  
 NUCMU 1613  
 NUCMU 1614  
 NUCMU 1615  
 NUCMU 1616  
 NUCMU 1617  
 NUCMU 1618  
 NUCMU 1619  
 NUCMU 1620  
 NUCMU 1621  
 NUCMU 1622  
 NUCMU 1623  
 NUCMU 1624

PAGE 51

```

1624 C SUBROUTINE TRANS(UPB)
1625 C
1626 C SUBROUTINE TRANS CALCULATES THE ATMOSPHERIC
1627 C TRANSMISSION FACTOR AS A FUNCTION OF WAVELENGTH.
1628 C
1629 C COMMON /SNOM2/ AUACAV(14), URM, SIGAVE(14),
1630 C TCUM(14), TUIF(14), TOZ(14), TRWL(14),
1631 C TWATW(14), WCU2, *IN(8)
1632 C
1633 C DATA TOZ,TWATW,TCUM/42*1.0/
1634 C
1635 C URM=0.000304*UPB
1636 C CALL TUIFS(1)
1637 C CALL TWATER(1)
1638 C CALL TCUZ(1)
1639 C CALL TOZONE
1640 C DO 1 I=1,14
1641 C TRWL(I)=TUIF(I)*TWATW(I)*TCUM(I)*TOZ(I)
1642 C CONTINUE
1643 C RETURN
1644 C END

```

```

NUCMU 1625
NUCMU 1626
NUCMU 1627
NUCMU 1628
NUCMU 1629
NUCMU 1630
NUCMU 1631
NUCMU 1632
NUCMU 1633
NUCMU 1634
NUCMU 1635
NUCMU 1636
NUCMU 1637
NUCMU 1638
NUCMU 1639
NUCMU 1640
NUCMU 1641
NUCMU 1642
NUCMU 1643
NUCMU 1644
NUCMU 1645

```

```

1645 SUBROUTINE TWATER(FLAG)
1646 C
1647 COMMON /SINCM2/ AUACAV(14), URM, SIGAVE(14),
1648 TCOW(14), TUIF(14), TRWL(14),
1649 TWATW(14), WCUT, WIN(8)
1650 C
1651 DIMENSION
1652 IELNU(7), U(7), C(7), CC(7), C1(7), C2(7), C3(7), C4(7),
1653 USE(7), ALIM(7), WINW(7), WINS(7), U
1654 C
1655 DATA CONST/0.43429448/.IUSE/4.6.7.9.11.13.14/
1656 DATA ALIM/0.200.200.350.275.200.500./
1657 DATA WINW/WINS/140./
1658 DATA UELNU/0.2240.1000.1500.1100.1000.540./
1659 DATA U/0.0.0.0.460.230.246.0./
1660 DATA C/0.38.31.242.152.316.40.2/
1661 DATA CC/0.0.0.0.202.127.337.0./
1662 C
1663 IF (FLAG .GT. 0) GO TO 10
1664 WINW(2)=WIN(4)
1665 WINW(3)=WIN(3)
1666 WINW(4)=WIN(2)
1667 WINW(5)=WIN(5)
1668 WINW(6)=WIN(6)
1669 WINW(7)=WIN(5)
1670 WINW(4)=WIN(2)
1671 WINS(5)=WIN(7)
1672 WINS(6)=WIN(6)
1673 C1(1)=0.1*WIN(1)
1674 UO 1 I=2.7
1675 C1(1)=C1(1)*SUMT(0.1*WIN(1))
1676 C4(1)=1./UELNU(1)
1677 UO 2 I=4.6
1678 C2(1)=0.1*WINS(1)
1679 C3(1)=U(1)*CONST
1680 RETURN
1681 CONTINUE
1682 USUMT=SQRT(URM)
1683 #=C1(1)*URM
1684 TWATW(4)=AMAX1(0.01,-.02*#)
1685 UO 5 I=2.7
1686 AIN=C1(1)*USUMT
1687 IF (AIN.LE.ALIM(1)) GO TO 4
1688 IF (U(1)) 3,4,3
1689 U=C2(1)*URM
1690 AIN=C1(1)+C3(1)*ALOG(UR)
1691 AIN=AMAX1(ALIM(1),AIN)
1692 TWAT=1.-AIN*U4(1)
1693 TWAT=AMAX1(0.,TWAT)
1694 J=IUSE(1)
1695 TWATW(J)=AMIN1(1.0,TWAT)

```

PL 62 53

1695  
1696

RETURN  
END

NUCMU 1696  
NUCMU 1697

```

1697 SUBROUTINE VIEWF(VVVF,FBFLAG)
1698
1699 C
1700 C VIEWF CALCULATES THE VIEW FACTOR (RATIO OF NORMAL INCIDENT
1701 C RADIATION TO RADIATION INCIDENT UP PLANE NORMAL TO LINE OF SIGHT
1702 C TO POINT SOURCE) FOR EACH SURFACE ELEMENT IN SECTION.
1703 C
1704 C VIEWF ALSO CALCULATES GO AND AAR FOR USE IN CALCULATION OF
1705 C GROUND AND CLOUD REFLECTIONS.
1706 C
1707 C
1708 C COMMON /SNOMI/ AA, AB, AC, AG, ALI,
1709 C AAR, CALT, CRFL, DFB, FBALT, GALT,
1710 C GO, HFB, ICLUD, NML, U, UAR(14),
1711 C MFB, TC, TRAD, VFA, YFB,
1712 C ZFB, XNA, YNA, ZNA
1713 C
1714 C DIMENSION UBT(10),ALFT(19),VFMT(150)
1715 C
1716 DATA ALFT/0.0,5.0,10.0,15.0,20.0,25.0,30.0,35.0,40.0,45.0,50.0,55.0,
1717 10.0,60.0,65.0,70.0,75.0,80.0,85.0,90.0/
1718 DATA UBT/0.1,1.1,1.1,2.1,5.2,10.3,20.0,30.0,40.0,50.0,60.0,70.0,80.0,90.0,100.0,110.0,120.0,130.0,140.0,150.0,160.0,170.0,180.0,190.0,200.0,210.0,220.0,230.0,240.0,250.0,260.0,270.0,280.0,290.0,300.0,310.0,320.0,330.0,340.0,350.0,360.0,370.0,380.0,390.0,400.0,410.0,420.0,430.0,440.0,450.0,460.0,470.0,480.0,490.0,500.0,510.0,520.0,530.0,540.0,550.0,560.0,570.0,580.0,590.0,600.0,610.0,620.0,630.0,640.0,650.0,660.0,670.0,680.0,690.0,700.0,710.0,720.0,730.0,740.0,750.0,760.0,770.0,780.0,790.0,800.0,810.0,820.0,830.0,840.0,850.0,860.0,870.0,880.0,890.0,900.0,910.0,920.0,930.0,940.0,950.0,960.0,970.0,980.0,990.0,1000.0,1010.0,1020.0,1030.0,1040.0,1050.0,1060.0,1070.0,1080.0,1090.0,1100.0,1110.0,1120.0,1130.0,1140.0,1150.0,1160.0,1170.0,1180.0,1190.0,1200.0,1210.0,1220.0,1230.0,1240.0,1250.0,1260.0,1270.0,1280.0,1290.0,1300.0,1310.0,1320.0,1330.0,1340.0,1350.0,1360.0,1370.0,1380.0,1390.0,1400.0,1410.0,1420.0,1430.0,1440.0,1450.0,1460.0,1470.0,1480.0,1490.0,1500.0,1510.0,1520.0,1530.0,1540.0,1550.0,1560.0,1570.0,1580.0,1590.0,1600.0,1610.0,1620.0,1630.0,1640.0,1650.0,1660.0,1670.0,1680.0,1690.0,1700.0,1710.0,1720.0,1730.0,1740.0,1750.0,1760.0,1770.0,1780.0,1790.0,1800.0,1810.0,1820.0,1830.0,1840.0,1850.0,1860.0,1870.0,1880.0,1890.0,1900.0,1910.0,1920.0,1930.0,1940.0,1950.0,1960.0,1970.0,1980.0,1990.0,2000.0,2010.0,2020.0,2030.0,2040.0,2050.0,2060.0,2070.0,2080.0,2090.0,2100.0,2110.0,2120.0,2130.0,2140.0,2150.0,2160.0,2170.0,2180.0,2190.0,2200.0,2210.0,2220.0,2230.0,2240.0,2250.0,2260.0,2270.0,2280.0,2290.0,2300.0,2310.0,2320.0,2330.0,2340.0,2350.0,2360.0,2370.0,2380.0,2390.0,2400.0,2410.0,2420.0,2430.0,2440.0,2450.0,2460.0,2470.0,2480.0,2490.0,2500.0,2510.0,2520.0,2530.0,2540.0,2550.0,2560.0,2570.0,2580.0,2590.0,2600.0,2610.0,2620.0,2630.0,2640.0,2650.0,2660.0,2670.0,2680.0,2690.0,2700.0,2710.0,2720.0,2730.0,2740.0,2750.0,2760.0,2770.0,2780.0,2790.0,2800.0,2810.0,2820.0,2830.0,2840.0,2850.0,2860.0,2870.0,2880.0,2890.0,2900.0,2910.0,2920.0,2930.0,2940.0,2950.0,2960.0,2970.0,2980.0,2990.0,3000.0,3010.0,3020.0,3030.0,3040.0,3050.0,3060.0,3070.0,3080.0,3090.0,3100.0,3110.0,3120.0,3130.0,3140.0,3150.0,3160.0,3170.0,3180.0,3190.0,3200.0,3210.0,3220.0,3230.0,3240.0,3250.0,3260.0,3270.0,3280.0,3290.0,3300.0,3310.0,3320.0,3330.0,3340.0,3350.0,3360.0,3370.0,3380.0,3390.0,3400.0,3410.0,3420.0,3430.0,3440.0,3450.0,3460.0,3470.0,3480.0,3490.0,3500.0,3510.0,3520.0,3530.0,3540.0,3550.0,3560.0,3570.0,3580.0,3590.0,3600.0,3610.0,3620.0,3630.0,3640.0,3650.0,3660.0,3670.0,3680.0,3690.0,3700.0,3710.0,3720.0,3730.0,3740.0,3750.0,3760.0,3770.0,3780.0,3790.0,3800.0,3810.0,3820.0,3830.0,3840.0,3850.0,3860.0,3870.0,3880.0,3890.0,3900.0,3910.0,3920.0,3930.0,3940.0,3950.0,3960.0,3970.0,3980.0,3990.0,4000.0,4010.0,4020.0,4030.0,4040.0,4050.0,4060.0,4070.0,4080.0,4090.0,4100.0,4110.0,4120.0,4130.0,4140.0,4150.0,4160.0,4170.0,4180.0,4190.0,4200.0,4210.0,4220.0,4230.0,4240.0,4250.0,4260.0,4270.0,4280.0,4290.0,4300.0,4310.0,4320.0,4330.0,4340.0,4350.0,4360.0,4370.0,4380.0,4390.0,4400.0,4410.0,4420.0,4430.0,4440.0,4450.0,4460.0,4470.0,4480.0,4490.0,4500.0,4510.0,4520.0,4530.0,4540.0,4550.0,4560.0,4570.0,4580.0,4590.0,4600.0,4610.0,4620.0,4630.0,4640.0,4650.0,4660.0,4670.0,4680.0,4690.0,4700.0,4710.0,4720.0,4730.0,4740.0,4750.0,4760.0,4770.0,4780.0,4790.0,4800.0,4810.0,4820.0,4830.0,4840.0,4850.0,4860.0,4870.0,4880.0,4890.0,4900.0,4910.0,4920.0,4930.0,4940.0,4950.0,4960.0,4970.0,4980.0,4990.0,5000.0,5010.0,5020.0,5030.0,5040.0,5050.0,5060.0,5070.0,5080.0,5090.0,5100.0,5110.0,5120.0,5130.0,5140.0,5150.0,5160.0,5170.0,5180.0,5190.0,5200.0,5210.0,5220.0,5230.0,5240.0,5250.0,5260.0,5270.0,5280.0,5290.0,5300.0,5310.0,5320.0,5330.0,5340.0,5350.0,5360.0,5370.0,5380.0,
```



PAGE 55

```

1747 IF (MFB*LT*HFB) GO TO 3
1748 VFKU=0.5
1749 IF (U2*UC*0.0) GO TO 2
1750 ALFA=ATAN(SUMT(UA**2*UY**2)/((-U2))**57.29576
1751 UBAR=UFB/HFB
1752 CALL INIZ(UBAR*ALFA*NUB*NALE*UBT*ALFT*VFKT*VFKU*190)
1753 VFR=VFKU*(1.0-VFKU)*SIN(PIU2*HFB/HFB)
1754 IF (UFB*0.01*HFB) GO TO 4
1755 FPLAQ=1.
1756 RETURN
1757 SINB=MFB/UFB
1758 COST=UX*NA*UY*YNA*U2*ZNA
1759 IF (COST*LT*-SINB) GO TO 7
1760 IF (COST*LT*SINB) GO TO 5
1761 VF=COST
1762 GO TO 6
1763 COSB=SUMT(1.0-SINB**2)
1764 SINT=SUMT(1.0-COST**2)
1765 VU=COSB*COST/(SINB*SINT)
1766 VV=COSB/SINT
1767 VF=(COST*(PI-ACUS(VU)*VU*SUMT(1.0-VU**2))+(ACUS(VV)-VV*SUMT(1.0-VV
1768 *2)))/SINB**2/PI
1769 VF=VF*VFK
1770 CURTINUE
1771 VVVF=VF
1772 RETURN
1773 END

```

NUCMUU 1748  
 NUCMUU 1749  
 NUCMUU 1750  
 NUCMUU 1751  
 NUCMUU 1752  
 NUCMUU 1753  
 NUCMUU 1754  
 NUCMUU 1755  
 NUCMUU 1756  
 NUCMUU 1757  
 NUCMUU 1758  
 NUCMUU 1759  
 NUCMUU 1760  
 NUCMUU 1761  
 NUCMUU 1762  
 NUCMUU 1763  
 NUCMUU 1764  
 NUCMUU 1765  
 NUCMUU 1766  
 NUCMUU 1767  
 NUCMUU 1768  
 NUCMUU 1769  
 NUCMUU 1770  
 NUCMUU 1771  
 NUCMUU 1772  
 NUCMUU 1773  
 NUCMUU 1774

1774 56

```

1775 C SUBROUTINE WATMD (ZF, JWDN, KHOW)
1776 C SUBROUTINE WATMD COMPUTES WATER VAPOR DENSITY GM/M**3
1777 C ZF IS ALTITUDE IN FEET.
1778 C JWDN IS ATMOSPHERE CODE, 1 = WET ATMOSPHERE.
1779 C KHOW IS RETURNED WATER VAPOR DENSITY, GM/M**3
1780 C
1781 C ZF=0.0003046
1782 C IF (JWDN.EQ.2) GO TO 3
1783 C IF (Z.GT.4.0) GO TO 1
1784 C KHOW=EXP(3.135-0.3277*Z)
1785 C GO TO 6
1786 C IF (Z.GT.16.7) GO TO 2
1787 C KHOW=EXP(3.962-0.534*Z)
1788 C GO TO 6
1789 C KHOW=0.007
1790 C GO TO 6
1791 C IF (Z.GT.5.0) GO TO 4
1792 C KHOW=EXP(-0.408*Z)
1793 C GO TO 6
1794 C IF (Z.GT.15.0) GO TO 5
1795 C KHOW=EXP(0.7403-0.5561*Z)
1796 C GO TO 6
1797 C KHOW=0.0005
1798 C RETURN
1799 C
1800 END

```

1775 NUCMUU  
 1776 NUCMUU  
 1777 NUCMUU  
 1778 NUCMUU  
 1779 NUCMUU  
 1780 NUCMUU  
 1781 NUCMUU  
 1782 NUCMUU  
 1783 NUCMUU  
 1784 NUCMUU  
 1785 NUCMUU  
 1786 NUCMUU  
 1787 NUCMUU  
 1788 NUCMUU  
 1789 NUCMUU  
 1790 NUCMUU  
 1791 NUCMUU  
 1792 NUCMUU  
 1793 NUCMUU  
 1794 NUCMUU  
 1795 NUCMUU  
 1796 NUCMUU  
 1797 NUCMUU  
 1798 NUCMUU  
 1799 NUCMUU  
 1800 NUCMUU

PAGE 51

```

1001 C
1002 C
1003 C
1004 C
1005 C
1006 C
1007 C
1008 C
1009 C
1010 C
1011 C
1012 C
1013 C
1014 C
1015 C
1016 C
1017 C
1018 C
1019 C
1020 C
1021 C
1022 C
1023 C
1024 C

SUBROUTINE WCO2P (ZP,ARG,IMM)
  SUBROUTINE WCO2P COMPUTES CO2 CONCENTRATION.
  ZP IS ALTITUDE IN FEET.
  ARG IS RETURNED VALUE.
  IMM IS CODE: 0, RETURN WCO2 IN ATMOS-CM/MM
              1, RETURN * IN ATMOS-CM

  DIMENSION A(4), B(4), ZC(3)
  DATA A/-0.1313,-0.3009,-0.1327,-0.1774/.0/5.520,7.460,5.285,6.112/
  DATA ZC/11.5,13.0,18.5/

  Z=ZF*0.0003048
  DO 1 I=1,3
    IF (Z.LE.ZC(I)) GO TO 2
    CONTINUE
  I=4
  ARG=EXP(A(I)*Z*B(I))
  IF (IMM.EQ.1) RETURN
  ARG=A(I)*ARG
  RETURN
END

```

APPENDIX B  
QUANTA OUTPUT

PAGE 1

THERE ARE 1 MARVAL MUNS FOR THIS PROBLEM WITH 4 TARGETS, 3 SUB LOCATIONS,  
2 TYPES OF AIRCRAFT (TOTAL OF 20), AND 2 TYPES OF MISSILES.  
THE REQUIRED SIZE FOR THE INDA ARRAY IS 5  
THE SIZE YOU HAVE DESIGNATED IS 5

TARGET	VALUE	LOCATION (DEGREES)	HONWAYS	AIRCRAFT TYPE AND NUMBER
1	100000	13.5833	144.7167	1 1 20000 2 10000 TAKE-OFF SEQUENCE BY TYPE 1 1 2
2	00000	44.0000	68.0333	1 10000 2 30000 TAKE-OFF SEQUENCE BY TYPE 1 2 2
3	0000	33.7167	84.5167	1 40000 2 50000 TAKE-OFF SEQUENCE BY TYPE 1 1 1 2 2 2
4	100000	33.4333	112.1667	1 40000 2 00000 TAKE-OFF SEQUENCE BY TYPE 1 1 1 1

AIRCRAFT TYPE	RELATIVE VALUE	BRAKE DISTANCE	PSI	CAL
1	20000	30000	10000	900000
2	100000	40000	15000	1200000

AIRCRAFT TYPE	TAKE-OFF INTERVALS	MINUTES
1	1	0.2500
1	1	0.5000
1	2	0.5000
1	2	0.5000
2	1	0.1250
2	1	0.2500
2	2	0.2500
2	2	0.2500

SUB LOCATIONS (DEGREES)	SUBS	MISSILES AND TYPE
1 30.7500	74.0000	1 18
2 20.0500	93.4500	3 12
3 45.0500	120.0500	2 10

NUMBER OF SUBS OF TYPE	1	2
1 <td>2</td> <td>5</td>	2	5

MISSILE TYPE	LAUNCH INTERVAL	RELIABILITY	MIN RANGE	MAX RANGE	YIELD	HEIGHT OF BURST	NUMBER MVS/MISSILE
1	0.2500	0.9000	250.000	2250.000	1000.0000	7000.00	2.0
2	0.2500	0.8500	650.000	2000.000	800.0000	6000.00	3.0

MISSILE TYPE	TIME	RANGE
1	3.5000	250.0000
2	5.5000	950.0000

7.5000 1600.0000  
9.5000 2250.0000

PAGE 2

MISSILE TYPE  
2

TIME RANGE  
5.0000 650.0000  
7.5000 1100.0000  
10.0000 1550.0000  
12.5000 2000.0000

THE REQUIRED WORK ARRAY SIZE IS 656  
THE PROVIDED WORK ARRAY SIZE IS 656  
THE REQUIRED WORK ARRAY SIZE IS 656  
THE PROVIDED WORK ARRAY SIZE IS 656  
THE REQUIRED SIZE FOR THE ALLOC AND PLAMB ARRAYS IS 480  
THE SIZE YOU HAVE DESIGNATED IS 480  
THE REQUIRED WORK ARRAY SIZE IS 72  
THE PROVIDED WORK ARRAY SIZE IS 656

## SUBROUTINE PROCESS

AIRCRAFT TYPE 1 OF 2 TYPE(S)

## VULNERABILITY CRITERIA FOR AIRCRAFT TYPE

1.00 PSI 90 CAL/CM<sup>2</sup>

## ATA INPUT FOR AIRCRAFT PROFILE

CARD NUMBER	GROUND RANGE	FLIGHT TIME	AIRCRAFT ALTITUDE	VELOCITY OF SOUND	MACH NUMBER	LEVEL-OFF ACCELERATION
1	0.00000000	0.00000000	0.00000000	1115.43553240	0.000	0.000
2	1500.00000000	7.50000000	5.00000000	1115.41737491	.130	0.000
3	3700.00000000	17.00000000	7.00000000	1115.40971103	.170	0.000
4	5700.00000000	30.00000000	10.00000000	1115.37522727	.200	0.000
5	7000.00000000	40.00000000	75.00000000	1115.14913559	.250	0.000
6	13000.00000000	63.00000000	230.00000000	1115.55494757	.340	0.000
7	20000.00000000	79.00000000	250.00000000	1115.47025509	.450	0.000
8	33000.00000000	105.00000000	500.00000000	1114.51915304	.600	0.000
9	50000.00000000	130.00000000	1250.00000000	1114.630005.3	.750	0.000
10	63000.00000000	150.00000000	2300.00000000	1107.58910112	.800	0.000
11	72000.00000000	160.00000000	2800.00000000	1105.65630093	.900	0.000
12	90000.00000000	180.00000000	4500.00000000	1097.05971240	.900	0.000
13	98000.00000000	195.00000000	5800.00000000	1093.70035753	.900	0.000
14	105000.00000000	200.00000000	7000.00000000	1085.28615092	.900	0.000
15	110000.00000000	205.00000000	9200.00000000	1080.51229753	.900	0.000
16	115000.00000000	210.00000000	10000.00000000	1077.44000000	.900	0.000

INITIAL ALTITUDE OF MAXIMUM MACH 20000 FEET

ATA COMPUTED FOR AIRCRAFT TYPE 1 AT A TERMINAL ALTITUDE OF 10000.0 FEET

VELOCITY OF SOUND: 1077.44 FEET/SECOND  
ACCELERATION COMPONENTS: 0.000 FEET/SEC/SEC

MACH NUMBER: 0.900 TERMINAL 0.900

VELOCITY: 969.70 FEET/SEC FINAL 995.09 FEET/SEC

GROUND RANGE (FEET) FLIGHT TIME (SEC) GROUND RANGE (FT) FLIGHT TIME (MIN)

0.	0.	0.	0.
.150000000E+04	.750000000E+01	.24671053E+00	.125000000E+00
.370000000E+04	.190000000E+02	.6085203E+00	.31666667E+00
.570000000E+04	.300000000E+02	.737500000E+00	.500000000E+00
.700000000E+04	.400000000E+02	.14002032E+01	.800000000E+00
.130000000E+05	.630000000E+02	.21301574E+01	.125000000E+01
.200000000E+05	.795000000E+02	.32894737E+01	.132500000E+01
.330000000E+05	.105000000E+03	.5427631E+01	.175000000E+01
.500000000E+05	.130000000E+03	.82230842E+01	.21666667E+01
.630000000E+05	.150000000E+03	.10361042E+02	.250000000E+01
.720000000E+05	.170000000E+03	.11942105E+02	.28666667E+01





SUBROUTINE PROCESS

AIRCRAFT TYPE 2 OF 2 TYPE(S)

VULNERABILITY CRITERIA FOR AIRCRAFT TYPE

1.50 PSI 120 CAL/CM<sup>2</sup>

DATA INPUT FOR AIRCRAFT PROFILE

CARD NUMBER	GROUND RANGE	FLIGHT TIME	AIRCRAFT ALTITUDE	VELOCITY OF SOUND	MACH NUMBER	LEVEL-OFF ACCELERATION
1	0.00000000	0.00000000	0.00000000	1116.43653240	0.000	0.200
2	2000.00000000	20.00000000	9.00000000	1116.40204669	.140	0.200
3	3900.00000000	30.00000000	30.00000000	1116.32158255	.140	0.200
4	6200.00000000	40.00000000	92.00000000	1116.06398203	.190	0.200
5	9500.00000000	50.00000000	360.00000000	1115.05635218	.250	0.200
6	13400.00000000	60.00000000	500.00000000	1114.51911546	.310	0.200
7	15600.00000000	66.00000000	500.01000000	1114.51873166	.350	0.200
8	55700.00000000	125.00000000	500.11000000	1114.51873166	.680	0.200
9	61000.00000000	132.00000000	1425.00000000	1110.56327981	.700	0.200
10	68000.00000000	140.00000000	3950.00000000	1101.19625459	.720	0.200
11	75500.00000000	146.00000000	5000.00000000	1097.11196555	.730	0.200

INITIAL ALTITUDE OF MAXIMUM MACH 7600.0 FEET

DATA COMPUTED FOR AIRCRAFT TYPE 2 AT A TERMINAL ALTITUDE OF 5000.0 FEET

VELOCITY OF SOUND: 1097.11 FEET/SECOND

ACCELERATION COMPONENTS: 0.200 FEET/SEC/SEC

MACH NUMBER: .730 TERMINAL .849

VELOCITY: 800.89 FEET/SEC FINAL 922.80 FEET/SEC

GROUND RANGE (FEET) FLIGHT TIME (SEC)

GROUND RANGE (FEET)	FLIGHT TIME (SEC)	GROUND RANGE (NM)	FLIGHT TIME (MIN)
0.	0.	0.	0.
.20000000E+04	.20000000E+02	.32894737E+00	.33333333E+00
.39000000E+04	.30000000E+02	.6414737E+00	.50000000E+00
.62000000E+04	.40000000E+02	.1019736E+01	.66666667E+00
.95000000E+04	.50000000E+02	.15625000E+01	.83333333E+00
.13400000E+05	.60000000E+02	.22039474E+01	.10000000E+01
.15600000E+05	.66000000E+02	.25657895E+01	.11000000E+01
.55900000E+05	.12500000E+03	.91940789E+01	.20833333E+01
.61000000E+05	.13200000E+03	.10032695E+02	.22000000E+01
.68000000E+05	.14000000E+03	.11164211E+02	.23333333E+01
.75500000E+05	.14800000E+03	.1241763E+02	.24666667E+01
.77066767E+05	.14996628E+03	.12678744E+02	.24994381E+01
.76647504E+05	.15153257E+03	.12943668E+02	.25322095E+01
.80332212E+05	.15369885E+03	.13212535E+02	.25649809E+01
.81990692E+05	.15586514E+03	.13485344E+02	.25977523E+01
.83673542E+05	.15763142E+03	.13762096E+02	.26305237E+01

PAGE 0

05380163E+05      159/9771E+03      14042/90E+02      06632951E+01

0/1110/53E+05      161/6399E+03      14327427E+02      0960666E+01  
92466350E+05      16/66285E+03      15204993E+02      27943808E+01  
14/0144E+06      22/66285E+03      24311585E+02      3/943608E+01

THERE WILL BE 1 MANUAL RUN(S) FOR THIS CASE.  
THE CUT-OFF VALUES ARE 0.50000

\*\*\*\*\* AIRCRAFT TYPE 1 .VS. MISSILE TYPE 1\*\*\*\*\*

WHEN DETONATION IS	0.0 NM FROM CENTROID, LETHAL AREA =	177.43 SQUARE NM
WHEN DETONATION IS	1.0 NM FROM CENTROID, LETHAL AREA =	149.20 SQUARE NM
WHEN DETONATION IS	2.0 NM FROM CENTROID, LETHAL AREA =	120.01 SQUARE NM
WHEN DETONATION IS	3.0 NM FROM CENTROID, LETHAL AREA =	111.74 SQUARE NM
WHEN DETONATION IS	4.0 NM FROM CENTROID, LETHAL AREA =	103.06 SQUARE NM
WHEN DETONATION IS	5.0 NM FROM CENTROID, LETHAL AREA =	100.15 SQUARE NM
WHEN DETONATION IS	6.0 NM FROM CENTROID, LETHAL AREA =	106.17 SQUARE NM
WHEN DETONATION IS	7.0 NM FROM CENTROID, LETHAL AREA =	108.15 SQUARE NM
WHEN DETONATION IS	8.0 NM FROM CENTROID, LETHAL AREA =	108.75 SQUARE NM
WHEN DETONATION IS	9.0 NM FROM CENTROID, LETHAL AREA =	112.26 SQUARE NM
WHEN DETONATION IS	10.0 NM FROM CENTROID, LETHAL AREA =	114.96 SQUARE NM
WHEN DETONATION IS	11.0 NM FROM CENTROID, LETHAL AREA =	119.49 SQUARE NM
WHEN DETONATION IS	12.0 NM FROM CENTROID, LETHAL AREA =	129.11 SQUARE NM
WHEN DETONATION IS	13.0 NM FROM CENTROID, LETHAL AREA =	133.85 SQUARE NM
WHEN DETONATION IS	14.0 NM FROM CENTROID, LETHAL AREA =	140.41 SQUARE NM
WHEN DETONATION IS	15.0 NM FROM CENTROID, LETHAL AREA =	135.33 SQUARE NM
WHEN DETONATION IS	16.0 NM FROM CENTROID, LETHAL AREA =	139.66 SQUARE NM
WHEN DETONATION IS	17.0 NM FROM CENTROID, LETHAL AREA =	142.79 SQUARE NM
WHEN DETONATION IS	18.0 NM FROM CENTROID, LETHAL AREA =	145.13 SQUARE NM
WHEN DETONATION IS	19.0 NM FROM CENTROID, LETHAL AREA =	140.94 SQUARE NM
WHEN DETONATION IS	20.0 NM FROM CENTROID, LETHAL AREA =	140.39 SQUARE NM
WHEN DETONATION IS	21.0 NM FROM CENTROID, LETHAL AREA =	149.37 SQUARE NM
WHEN DETONATION IS	22.0 NM FROM CENTROID, LETHAL AREA =	150.56 SQUARE NM
WHEN DETONATION IS	23.0 NM FROM CENTROID, LETHAL AREA =	151.39 SQUARE NM
WHEN DETONATION IS	24.0 NM FROM CENTROID, LETHAL AREA =	156.10 SQUARE NM
WHEN DETONATION IS	25.0 NM FROM CENTROID, LETHAL AREA =	156.72 SQUARE NM
WHEN DETONATION IS	26.0 NM FROM CENTROID, LETHAL AREA =	153.26 SQUARE NM
WHEN DETONATION IS	27.0 NM FROM CENTROID, LETHAL AREA =	153.74 SQUARE NM
WHEN DETONATION IS	28.0 NM FROM CENTROID, LETHAL AREA =	154.16 SQUARE NM
WHEN DETONATION IS	29.0 NM FROM CENTROID, LETHAL AREA =	154.54 SQUARE NM

WHEN DETONATION IS	0.0 NM FROM BRAKE RELEASE, KILL LINE IS	0.0 PLUS	4.7 NM
WHEN DETONATION IS	1.0 NM FROM BRAKE RELEASE, KILL LINE IS	1.0 PLUS	4.4 NM
WHEN DETONATION IS	2.0 NM FROM BRAKE RELEASE, KILL LINE IS	2.0 PLUS	4.1 NM
WHEN DETONATION IS	3.0 NM FROM BRAKE RELEASE, KILL LINE IS	3.0 PLUS	3.8 NM
WHEN DETONATION IS	4.0 NM FROM BRAKE RELEASE, KILL LINE IS	4.0 PLUS	3.5 NM
WHEN DETONATION IS	5.0 NM FROM BRAKE RELEASE, KILL LINE IS	5.0 PLUS	3.3 NM
WHEN DETONATION IS	6.0 NM FROM BRAKE RELEASE, KILL LINE IS	6.0 PLUS	3.3 NM
WHEN DETONATION IS	7.0 NM FROM BRAKE RELEASE, KILL LINE IS	7.0 PLUS	3.2 NM
WHEN DETONATION IS	8.0 NM FROM BRAKE RELEASE, KILL LINE IS	8.0 PLUS	3.1 NM
WHEN DETONATION IS	9.0 NM FROM BRAKE RELEASE, KILL LINE IS	9.0 PLUS	2.5 NM
WHEN DETONATION IS	10.0 NM FROM BRAKE RELEASE, KILL LINE IS	10.0 PLUS	2.9 NM
WHEN DETONATION IS	11.0 NM FROM BRAKE RELEASE, KILL LINE IS	11.0 PLUS	2.7 NM
WHEN DETONATION IS	12.0 NM FROM BRAKE RELEASE, KILL LINE IS	11.6 PLUS	2.6 NM

\*\*\*\*\* AIRCRAFT TYPE 1 .VS. MISSILE TYPE \*\*\*\*\*

WHEN DETONATION IS	0.0 NM FROM	CENTROID	LETHAL AREA =	142.39	SQUARE NM
WHEN DETONATION IS	1.0 NM FROM	CENTROID	LETHAL AREA =	110.97	SQUARE NM
WHEN DETONATION IS	2.0 NM FROM	CENTROID	LETHAL AREA =	101.54	SQUARE NM
WHEN DETONATION IS	3.0 NM FROM	CENTROID	LETHAL AREA =	91.57	SQUARE NM
WHEN DETONATION IS	4.0 NM FROM	CENTROID	LETHAL AREA =	85.60	SQUARE NM
WHEN DETONATION IS	5.0 NM FROM	CENTROID	LETHAL AREA =	84.55	SQUARE NM
WHEN DETONATION IS	6.0 NM FROM	CENTROID	LETHAL AREA =	80.04	SQUARE NM
WHEN DETONATION IS	7.0 NM FROM	CENTROID	LETHAL AREA =	93.45	SQUARE NM
WHEN DETONATION IS	8.0 NM FROM	CENTROID	LETHAL AREA =	97.02	SQUARE NM
WHEN DETONATION IS	9.0 NM FROM	CENTROID	LETHAL AREA =	100.59	SQUARE NM
WHEN DETONATION IS	10.0 NM FROM	CENTROID	LETHAL AREA =	102.75	SQUARE NM
WHEN DETONATION IS	11.0 NM FROM	CENTROID	LETHAL AREA =	105.90	SQUARE NM
WHEN DETONATION IS	12.0 NM FROM	CENTROID	LETHAL AREA =	115.19	SQUARE NM
WHEN DETONATION IS	13.0 NM FROM	CENTROID	LETHAL AREA =	119.66	SQUARE NM
WHEN DETONATION IS	14.0 NM FROM	CENTROID	LETHAL AREA =	110.19	SQUARE NM
WHEN DETONATION IS	15.0 NM FROM	CENTROID	LETHAL AREA =	121.85	SQUARE NM
WHEN DETONATION IS	16.0 NM FROM	CENTROID	LETHAL AREA =	125.41	SQUARE NM
WHEN DETONATION IS	17.0 NM FROM	CENTROID	LETHAL AREA =	127.99	SQUARE NM
WHEN DETONATION IS	18.0 NM FROM	CENTROID	LETHAL AREA =	129.92	SQUARE NM
WHEN DETONATION IS	19.0 NM FROM	CENTROID	LETHAL AREA =	131.41	SQUARE NM
WHEN DETONATION IS	20.0 NM FROM	CENTROID	LETHAL AREA =	132.61	SQUARE NM
WHEN DETONATION IS	21.0 NM FROM	CENTROID	LETHAL AREA =	133.58	SQUARE NM
WHEN DETONATION IS	22.0 NM FROM	CENTROID	LETHAL AREA =	134.39	SQUARE NM
WHEN DETONATION IS	23.0 NM FROM	CENTROID	LETHAL AREA =	135.06	SQUARE NM
WHEN DETONATION IS	24.0 NM FROM	CENTROID	LETHAL AREA =	135.67	SQUARE NM
WHEN DETONATION IS	25.0 NM FROM	CENTROID	LETHAL AREA =	136.18	SQUARE NM
WHEN DETONATION IS	26.0 NM FROM	CENTROID	LETHAL AREA =	136.62	SQUARE NM
WHEN DETONATION IS	27.0 NM FROM	CENTROID	LETHAL AREA =	137.01	SQUARE NM
WHEN DETONATION IS	28.0 NM FROM	CENTROID	LETHAL AREA =	137.36	SQUARE NM
WHEN DETONATION IS	29.0 NM FROM	CENTROID	LETHAL AREA =	137.68	SQUARE NM

WHEN DETONATION IS	0.0 NM FROM	BRAKE	RELEASE	KILL LINE IS	0.0 PLUS	4.4 NM
WHEN DETONATION IS	1.0 NM FROM	BRAKE	RELEASE	KILL LINE IS	1.0 PLUS	4.2 NM
WHEN DETONATION IS	2.0 NM FROM	BRAKE	RELEASE	KILL LINE IS	2.0 PLUS	4.0 NM
WHEN DETONATION IS	3.0 NM FROM	BRAKE	RELEASE	KILL LINE IS	3.0 PLUS	3.7 NM
WHEN DETONATION IS	4.0 NM FROM	BRAKE	RELEASE	KILL LINE IS	4.0 PLUS	3.4 NM
WHEN DETONATION IS	5.0 NM FROM	BRAKE	RELEASE	KILL LINE IS	5.0 PLUS	3.1 NM
WHEN DETONATION IS	6.0 NM FROM	BRAKE	RELEASE	KILL LINE IS	6.0 PLUS	2.9 NM
WHEN DETONATION IS	7.0 NM FROM	BRAKE	RELEASE	KILL LINE IS	7.0 PLUS	2.9 NM
WHEN DETONATION IS	8.0 NM FROM	BRAKE	RELEASE	KILL LINE IS	8.0 PLUS	3.2 NM
WHEN DETONATION IS	9.0 NM FROM	BRAKE	RELEASE	KILL LINE IS	9.0 PLUS	2.8 NM
WHEN DETONATION IS	10.0 NM FROM	BRAKE	RELEASE	KILL LINE IS	10.0 PLUS	2.4 NM
WHEN DETONATION IS	11.0 NM FROM	BRAKE	RELEASE	KILL LINE IS	10.5 PLUS	2.7 NM
WHEN DETONATION IS	12.0 NM FROM	BRAKE	RELEASE	KILL LINE IS	11.0 PLUS	2.4 NM

\*\*\*\*\* AIRCRAFT TYPE C.VS. MISSILE TYPE \*\*\*\*\*

WHEN DETONATION IS	0.0 NM FROM CENTRIGU, LETHAL AREA =	59.54 SQUARE NM
WHEN DETONATION IS	1.0 NM FROM CENTRIGU, LETHAL AREA =	40.39 SQUARE NM
WHEN DETONATION IS	2.0 NM FROM CENTRIGU, LETHAL AREA =	44.55 SQUARE NM
WHEN DETONATION IS	3.0 NM FROM CENTRIGU, LETHAL AREA =	45.22 SQUARE NM
WHEN DETONATION IS	4.0 NM FROM CENTRIGU, LETHAL AREA =	50.53 SQUARE NM
WHEN DETONATION IS	5.0 NM FROM CENTRIGU, LETHAL AREA =	54.52 SQUARE NM
WHEN DETONATION IS	6.0 NM FROM CENTRIGU, LETHAL AREA =	50.61 SQUARE NM
WHEN DETONATION IS	7.0 NM FROM CENTRIGU, LETHAL AREA =	60.22 SQUARE NM
WHEN DETONATION IS	8.0 NM FROM CENTRIGU, LETHAL AREA =	66.12 SQUARE NM
WHEN DETONATION IS	9.0 NM FROM CENTRIGU, LETHAL AREA =	71.07 SQUARE NM
WHEN DETONATION IS	10.0 NM FROM CENTRIGU, LETHAL AREA =	77.38 SQUARE NM
WHEN DETONATION IS	11.0 NM FROM CENTRIGU, LETHAL AREA =	84.67 SQUARE NM
WHEN DETONATION IS	12.0 NM FROM CENTRIGU, LETHAL AREA =	91.23 SQUARE NM
WHEN DETONATION IS	13.0 NM FROM CENTRIGU, LETHAL AREA =	104.46 SQUARE NM
WHEN DETONATION IS	14.0 NM FROM CENTRIGU, LETHAL AREA =	116.72 SQUARE NM
WHEN DETONATION IS	15.0 NM FROM CENTRIGU, LETHAL AREA =	127.13 SQUARE NM
WHEN DETONATION IS	16.0 NM FROM CENTRIGU, LETHAL AREA =	136.62 SQUARE NM
WHEN DETONATION IS	17.0 NM FROM CENTRIGU, LETHAL AREA =	150.52 SQUARE NM
WHEN DETONATION IS	18.0 NM FROM CENTRIGU, LETHAL AREA =	139.42 SQUARE NM
WHEN DETONATION IS	19.0 NM FROM CENTRIGU, LETHAL AREA =	141.68 SQUARE NM
WHEN DETONATION IS	20.0 NM FROM CENTRIGU, LETHAL AREA =	143.48 SQUARE NM
WHEN DETONATION IS	25.0 NM FROM CENTRIGU, LETHAL AREA =	144.95 SQUARE NM
WHEN DETONATION IS	30.0 NM FROM CENTRIGU, LETHAL AREA =	146.17 SQUARE NM
WHEN DETONATION IS	35.0 NM FROM CENTRIGU, LETHAL AREA =	147.21 SQUARE NM
WHEN DETONATION IS	40.0 NM FROM CENTRIGU, LETHAL AREA =	148.09 SQUARE NM
WHEN DETONATION IS	45.0 NM FROM CENTRIGU, LETHAL AREA =	148.86 SQUARE NM
WHEN DETONATION IS	50.0 NM FROM CENTRIGU, LETHAL AREA =	149.53 SQUARE NM
WHEN DETONATION IS	55.0 NM FROM CENTRIGU, LETHAL AREA =	150.12 SQUARE NM
WHEN DETONATION IS	60.0 NM FROM CENTRIGU, LETHAL AREA =	150.65 SQUARE NM
WHEN DETONATION IS	65.0 NM FROM CENTRIGU, LETHAL AREA =	151.12 SQUARE NM

WHEN DETONATION IS	0.0 NM FROM SHAK RELEASE, KILL LINE IS	0.0 PLUS	3.0 NM
WHEN DETONATION IS	1.0 NM FROM SHAK RELEASE, KILL LINE IS	1.0 PLUS	3.4 NM
WHEN DETONATION IS	2.0 NM FROM SHAK RELEASE, KILL LINE IS	2.0 PLUS	3.3 NM
WHEN DETONATION IS	3.0 NM FROM SHAK RELEASE, KILL LINE IS	3.0 PLUS	3.2 NM
WHEN DETONATION IS	4.0 NM FROM SHAK RELEASE, KILL LINE IS	4.0 PLUS	3.0 NM
WHEN DETONATION IS	5.0 NM FROM SHAK RELEASE, KILL LINE IS	5.0 PLUS	2.7 NM
WHEN DETONATION IS	6.0 NM FROM SHAK RELEASE, KILL LINE IS	6.0 PLUS	2.6 NM
WHEN DETONATION IS	7.0 NM FROM SHAK RELEASE, KILL LINE IS	7.0 PLUS	2.4 NM
WHEN DETONATION IS	8.0 NM FROM SHAK RELEASE, KILL LINE IS	8.0 PLUS	2.3 NM
WHEN DETONATION IS	9.0 NM FROM SHAK RELEASE, KILL LINE IS	8.9 PLUS	2.4 NM
WHEN DETONATION IS	10.0 NM FROM SHAK RELEASE, KILL LINE IS	9.5 PLUS	2.4 NM
WHEN DETONATION IS	11.0 NM FROM SHAK RELEASE, KILL LINE IS	10.1 PLUS	2.4 NM
WHEN DETONATION IS	12.0 NM FROM SHAK RELEASE, KILL LINE IS	10.5 PLUS	2.4 NM

\*\*\*\*\* AIRCRAFT TYPE C VS. MISSILE TYPE \*\*\*\*\*

WHEN DETONATION IS	0.0 NM FROM	CENTROID	LETHAL AREA =	40.51 SQUARE NM
WHEN DETONATION IS	1.0 NM FROM	CENTROID	LETHAL AREA =	39.71 SQUARE NM
WHEN DETONATION IS	2.0 NM FROM	CENTROID	LETHAL AREA =	37.25 SQUARE NM
WHEN DETONATION IS	3.0 NM FROM	CENTROID	LETHAL AREA =	36.88 SQUARE NM
WHEN DETONATION IS	4.0 NM FROM	CENTROID	LETHAL AREA =	44.55 SQUARE NM
WHEN DETONATION IS	5.0 NM FROM	CENTROID	LETHAL AREA =	48.01 SQUARE NM
WHEN DETONATION IS	6.0 NM FROM	CENTROID	LETHAL AREA =	50.80 SQUARE NM
WHEN DETONATION IS	7.0 NM FROM	CENTROID	LETHAL AREA =	54.09 SQUARE NM
WHEN DETONATION IS	8.0 NM FROM	CENTROID	LETHAL AREA =	59.27 SQUARE NM
WHEN DETONATION IS	9.0 NM FROM	CENTROID	LETHAL AREA =	64.19 SQUARE NM
WHEN DETONATION IS	10.0 NM FROM	CENTROID	LETHAL AREA =	70.43 SQUARE NM
WHEN DETONATION IS	11.0 NM FROM	CENTROID	LETHAL AREA =	76.80 SQUARE NM
WHEN DETONATION IS	12.0 NM FROM	CENTROID	LETHAL AREA =	81.02 SQUARE NM
WHEN DETONATION IS	13.0 NM FROM	CENTROID	LETHAL AREA =	91.02 SQUARE NM
WHEN DETONATION IS	14.0 NM FROM	CENTROID	LETHAL AREA =	101.59 SQUARE NM
WHEN DETONATION IS	15.0 NM FROM	CENTROID	LETHAL AREA =	107.84 SQUARE NM
WHEN DETONATION IS	16.0 NM FROM	CENTROID	LETHAL AREA =	111.94 SQUARE NM
WHEN DETONATION IS	17.0 NM FROM	CENTROID	LETHAL AREA =	114.05 SQUARE NM
WHEN DETONATION IS	18.0 NM FROM	CENTROID	LETHAL AREA =	117.02 SQUARE NM
WHEN DETONATION IS	19.0 NM FROM	CENTROID	LETHAL AREA =	118.71 SQUARE NM
WHEN DETONATION IS	20.0 NM FROM	CENTROID	LETHAL AREA =	120.06 SQUARE NM
WHEN DETONATION IS	21.0 NM FROM	CENTROID	LETHAL AREA =	121.16 SQUARE NM
WHEN DETONATION IS	22.0 NM FROM	CENTROID	LETHAL AREA =	122.07 SQUARE NM
WHEN DETONATION IS	23.0 NM FROM	CENTROID	LETHAL AREA =	122.85 SQUARE NM
WHEN DETONATION IS	24.0 NM FROM	CENTROID	LETHAL AREA =	123.51 SQUARE NM
WHEN DETONATION IS	25.0 NM FROM	CENTROID	LETHAL AREA =	124.08 SQUARE NM
WHEN DETONATION IS	26.0 NM FROM	CENTROID	LETHAL AREA =	124.59 SQUARE NM
WHEN DETONATION IS	27.0 NM FROM	CENTROID	LETHAL AREA =	125.03 SQUARE NM
WHEN DETONATION IS	28.0 NM FROM	CENTROID	LETHAL AREA =	125.42 SQUARE NM
WHEN DETONATION IS	29.0 NM FROM	CENTROID	LETHAL AREA =	125.76 SQUARE NM

WHEN DETONATION IS	0.0 NM FROM	BRAKE RELEASE	KILL LINE IS	0.0 PLUS	3.3 NM
WHEN DETONATION IS	1.0 NM FROM	BRAKE RELEASE	KILL LINE IS	1.0 PLUS	3.1 NM
WHEN DETONATION IS	2.0 NM FROM	BRAKE RELEASE	KILL LINE IS	2.0 PLUS	3.0 NM
WHEN DETONATION IS	3.0 NM FROM	BRAKE RELEASE	KILL LINE IS	3.0 PLUS	3.0 NM
WHEN DETONATION IS	4.0 NM FROM	BRAKE RELEASE	KILL LINE IS	4.0 PLUS	2.9 NM
WHEN DETONATION IS	5.0 NM FROM	BRAKE RELEASE	KILL LINE IS	5.0 PLUS	2.6 NM
WHEN DETONATION IS	6.0 NM FROM	BRAKE RELEASE	KILL LINE IS	6.0 PLUS	2.4 NM
WHEN DETONATION IS	7.0 NM FROM	BRAKE RELEASE	KILL LINE IS	7.0 PLUS	2.3 NM
WHEN DETONATION IS	8.0 NM FROM	BRAKE RELEASE	KILL LINE IS	8.0 PLUS	2.1 NM
WHEN DETONATION IS	9.0 NM FROM	BRAKE RELEASE	KILL LINE IS	9.0 PLUS	2.1 NM
WHEN DETONATION IS	10.0 NM FROM	BRAKE RELEASE	KILL LINE IS	9.5 PLUS	2.2 NM
WHEN DETONATION IS	11.0 NM FROM	BRAKE RELEASE	KILL LINE IS	9.5 PLUS	2.2 NM
WHEN DETONATION IS	12.0 NM FROM	BRAKE RELEASE	KILL LINE IS	9.5 PLUS	2.2 NM

PAGE 11

THE DISTANCE TO TARGET 1 FROM SUB 1 IS 4000000000  
THE AVERAGE DISTANCE TO THE TURN POINT IS 4017 NM

THE DISTANCE TO TARGET 1 FROM SUB 2 IS 2994000000  
THE AVERAGE DISTANCE TO THE TURN POINT IS 4017 NM

THE DISTANCE TO TARGET 1 FROM SUB 3 IS 2151000000  
THE AVERAGE DISTANCE TO THE TURN POINT IS 4017 NM

THE DISTANCE TO TARGET 2 FROM SUB 1 IS 3370000000  
THE AVERAGE DISTANCE TO THE TURN POINT IS 3000 NM

AFTER 4000000000 MINUTES, WHEN REAPPEAR, 1 ARRIVES, THE RANGES(NM) OF AIRCRAFT ARE  
1000000 000000

THE DISTANCE TO TARGET 2 FROM SUB 2 IS 1547000000  
THE AVERAGE DISTANCE TO THE TURN POINT IS 5000 NM

AFTER 4000000000 MINUTES, WHEN REAPPEAR, 2 ARRIVES, THE RANGES(NM) OF AIRCRAFT ARE  
470000 440000 397000 351000

THE DISTANCE TO TARGET 2 FROM SUB 3 IS 2360000000  
THE AVERAGE DISTANCE TO THE TURN POINT IS 5000 NM

THE DISTANCE TO TARGET 3 FROM SUB 1 IS 3400000000  
THE AVERAGE DISTANCE TO THE TURN POINT IS 4001 NM

AFTER 4000000000 MINUTES, WHEN REAPPEAR, 1 ARRIVES, THE RANGES(NM) OF AIRCRAFT ARE  
1000000 1000000 1000000 000000 000000 000000

THE DISTANCE TO TARGET 3 FROM SUB 2 IS 5790000000  
THE AVERAGE DISTANCE TO THE TURN POINT IS 4001 NM

THE DISTANCE TO TARGET 3 FROM SUB 3 IS 2015000000  
THE AVERAGE DISTANCE TO THE TURN POINT IS 4001 NM

THE DISTANCE TO TARGET 4 FROM SUB 1 IS 1874000000  
THE AVERAGE DISTANCE TO THE TURN POINT IS 3000 NM

AFTER 4000000000 MINUTES, WHEN REAPPEAR, 1 ARRIVES, THE RANGES(NM) OF AIRCRAFT ARE  
310000 290000 250000 240000

THE DISTANCE TO TARGET 4 FROM SUB 2 IS 1017000000  
THE AVERAGE DISTANCE TO THE TURN POINT IS 3000 NM

AFTER 4000000000 MINUTES, WHEN REAPPEAR, 2 ARRIVES, THE RANGES(NM) OF AIRCRAFT ARE  
140000 100000 150000 120000

THE DISTANCE TO TARGET 4 FROM SUB 3 IS 973000000  
THE AVERAGE DISTANCE TO THE TURN POINT IS 3000 NM

AFTER 4000000000 MINUTES, WHEN REAPPEAR, 3 ARRIVES, THE RANGES(NM) OF AIRCRAFT ARE  
160000 150000 130000 100000

PAGE 12

[illegible][illegible]

$\frac{d}{dt} \left( \frac{1}{r^2} \right) = -\frac{2}{r^3} \frac{dr}{dt}$



PAGE 13

ITERATION 34  
THE MULTIPLE MATRIX HAS CONVERGED USING EPSILON = .1000 THE MAXIMUM DELTA LAMBDA FOUND: .092267

ITERATION 35  
THE MULTIPLE MATRIX HAS CONVERGED USING EPSILON = .0100 THE MAXIMUM DELTA LAMBDA FOUND: .006631

ITERATION 36  
MULTIPLE MATRIX CONVERGED WITHIN TOLERANCE OF .010000

\*\*\*\*\*OVERPRINTOUT OF THE OPTIMUM ALLOCATION OF MISSILES\*\*\*\*\*

TARGET	1	VS. SUB LOCATION	BASE	ROUTE	TURN PT	
TARGET 2	VS. SUB LOCATION	BASE	ROUTE	TURN PT		
	1 ( 2 SUBS)	1.0	1.0	0.0 FROM SALVO	4 (WEAPON GROUP	4 )
	1 ( 2 SUBS)	0.0	1.0	0.0 FROM SALVO	7 (WEAPON GROUP	7 )
TARGET 3	VS. SUB LOCATION	BASE	ROUTE	TURN PT		
	1 ( 2 SUBS)	0.0	1.0	0.0 FROM SALVO	2 (WEAPON GROUP	2 )
	1 ( 2 SUBS)	0.0	1.0	0.0 FROM SALVO	5 (WEAPON GROUP	5 )
	1 ( 2 SUBS)	0.0	1.0	0.0 FROM SALVO	6 (WEAPON GROUP	6 )
	1 ( 2 SUBS)	0.0	1.0	0.0 FROM SALVO	7 (WEAPON GROUP	7 )
TARGET 4	VS. SUB LOCATION	BASE	ROUTE	TURN PT		
	1 ( 2 SUBS)	1.0	0.0	0.0 FROM SALVO	1 (WEAPON GROUP	1 )
	1 ( 2 SUBS)	1.0	0.0	0.0 FROM SALVO	2 (WEAPON GROUP	2 )
	2 ( 3 SUBS)	0.0	0.0	0.0 FROM SALVO	1 (WEAPON GROUP	1 )
	3 ( 2 SUBS)	0.0	0.0	0.0 FROM SALVO	1 (WEAPON GROUP	31 )

SUB LOCATION 1 ( 2 SUBS)

1.0 MISSILES FROM SALVO	1 TO TARGET	4 ( 1.0 TO BASE)
1.0 MISSILES FROM SALVO	2 TO TARGET	3 ( 0.0 TO BASE)
1.0 MISSILES FROM SALVO	2 TO TARGET	4 ( 1.0 TO BASE)
2.0 MISSILES FROM SALVO	4 TO TARGET	2 ( 1.0 TO BASE)
1.0 MISSILES FROM SALVO	5 TO TARGET	3 ( 0.0 TO BASE)
1.0 MISSILES FROM SALVO	6 TO TARGET	3 ( 0.0 TO BASE)
1.0 MISSILES FROM SALVO	7 TO TARGET	2 ( 0.0 TO BASE)
1.0 MISSILES FROM SALVO	7 TO TARGET	3 ( 0.0 TO BASE)

SUB LOCATION 2 ( 3 SUBS)

2.0 MISSILES FROM SALVO	1 TO TARGET	4 ( 0.0 TO BASE)
-------------------------	-------------	------------------

SUB LOCATION 3 ( 2 SUBS)

2.0 MISSILES FROM SALVO	1 TO TARGET	4 ( 0.0 TO BASE)
-------------------------	-------------	------------------

PAGE 10

THIS IS THE NUMBER 1 REMAIN KILL. CUF = .50000

TARGET NUMBER	NUMBER OF THE BASE	REMPONS NUMBER	ALLOCAED TO TURN PI	BASE VALUE	PROB. OF KILL	AIRCRAFT TYPE	AIRCRAFT VALUE	KILL VALUE	PROB. OF KILL
1	0.0	0.0	0.0	15.0000	0.0000	1	2.5000	0.0000	0.0000
						1	2.5000	0.0000	0.0000
						2	1.0000	0.0000	0.0000
TARGET 1 HAS A TOTAL KILL OF 0.0000									
2	1.0	2.0	0.0	2.0000	.9600	1	2.5000	2.2529	.9132
						2	1.0000	.8455	.8455
						2	1.0000	.8455	.8455
						2	1.0000	.8455	.8455
TARGET 2 HAS A TOTAL KILL OF 0.0194									
3	0.0	4.0	0.0	0.0000	0.0000	1	2.5000	2.4888	.9447
						1	2.5000	2.4888	.9447
						1	2.5000	2.4888	.9447
						2	1.0000	.9775	.9775
						2	1.0000	.9775	.9775
						2	1.0000	.9775	.9775
						2	1.0000	.9775	.9775
						2	1.0000	.9775	.9775
TARGET 3 HAS A TOTAL KILL OF 14.0351									
4	2.0	0.0	4.0	10.0000	.9900	1	2.5000	2.2630	.9032
						1	2.5000	2.2630	.9032
						1	2.5000	2.2630	.9032
						1	2.5000	2.2630	.9032
TARGET 4 HAS A TOTAL KILL OF 10.9522									
***** TOTALS *****						1	2.5000	21.2821	8.5128
						2	9.0000	7.4246	7.4246

EXPECTED VALUE KILLED = 40.4068

NUMBER OF REMPONS NOT ALLOCATED = 71